



Air-Conditioning, Heating, and Refrigeration
Institute (AHRI) Low-GWP Alternative Refrigerants
Evaluation Program (Low-GWP AREP)

TEST REPORT #59

Compressor Calorimeter Test of Refrigerants L41-1, DR-5A, ARM-71a, D2Y-60 and R-32 in a R-410A Reciprocating Piston Compressor

James R. Lenz
Bristol Compressor International, Inc.
15185 Industrial Park Rd., Bristol, VA 24202

And

Som Shrestha
Oak Ridge National Laboratory
Oak Ridge, TN 37831

January 18, 2016

This report has been made available to the public
as part of the author company's participation in the
AHRI's Low-GWP AREP.



we make life better®

List of Tested Refrigerants' Composition (Mass %)

R-410A	R-32/R-125 (50/50)
L41-1	R-32/R-1234ze/R-600 (68/29/3)
DR-5A	R-32/R-1234yf (68.9/31.1)
ARM-71a	R-32/R-1234yf/R1234ze (68/26/6)
D2Y-60	R-32/R-1234yf (40/60)
R-32	R-32 (100)

1. Introduction

As a contribution to Phase II of the AHRI Low-GWP Alternative Refrigerants Evaluation Program (AREP), this report presents the results of performance tests of five Low-GWP refrigerants L41-1, DR-5A, ARM-71a, D2Y-60 and R-32, and compares the results with R-410A. Tests conditions spanned the air conditioning application envelope. Suction pressures ranged from a dew point of -10°F to 55°F. Discharge pressures ranged from a dew point of 80°F to 150°F. All tests were performed with 20°F superheat and 15°F subcooling.

It should be noted that the test compressor used is a production compressor specifically designed for R-410A. The new refrigerants may give slightly better performance with compressors optimized for them. Also, the lubricant was changed from a standard 32 cSt POE to a 64 cSt POE specifically formulated for R32 and refrigerant blends with high concentrations of R32. Therefore the change in performance may be due in part to the different lubricant.

2. Test Setup:

a. Description of Test Refrigerants

The composition of the baseline R-410A and five Low-GWP refrigerants tested are shown in Table 1. Glide is for a 45 °F evaporator. GWP values use a 100 year integration time horizon and data from IPPC AR4.

Table 1: All Refrigerants Tested

	Composition (Mass %)	GWP	Glide	Manufacturer
R-410A	R-32/R-125 (50/50)	2088	0.2 °F	various
L41-1	R-32/R-1234ze/R-600 (68/29/3)	461	8.4 °F	Honeywell
DR-5A	R-32/R-1234yf (68.9/31.1)	466	2.9 °F	Chemours
ARM-71a	R-32/R-1234yf/R1234ze (68/26/6)	482	3.5 °F	Arkema
D2Y-60	R-32/R-1234yf (40/60)	272	8.6 °F	Daikin
R-32	R-32 (100)	675	0 °F	various

b. Description of Lubricants

The lubricant used for the R-410A testing is 32BCE, an ISO 32 Polyolester oil (POE). This is the original lubricant shipped with the production compressor. The compressor was charged with 30 oz. of oil.

The Low-GWP refrigerants were tested with HXL-8849, a special ISO 64 POE made by Chemtura for use with R32 and refrigerant blends with high R-32 concentrations. The compressor was charged with 30 oz. of this oil.

c. Description of Compressor

The compressor used for this test was a high-efficiency reciprocating piston compressor made by Bristol Compressors International, Inc. The compressor specification are presented in Table 2.

Table 2: Test Compressor Specification

Model No.	H84B223ABC
Capacity	22,220 BTU/hr @ AHRI 45/130 Rating Point
Motor Input	2150 watts
EER	10.3 BTU/W-hr
RLA	9.5 amps
Displacement	1.862 cu.in/rev
Voltage	230/208-1-60hz

No modifications were made to the compressor other than to change oil from the standard POE after baseline testing with R-410A to the special POE used for the Low-GWP blends. The compressor was “run-in” for 72 hours on R-410A before testing.

d. Description of Calorimeter Test Facilities

The performance testing was done on the 36,000 BTU/hr calorimeter located at the Heat Exchanger Advanced Testing Facility at Oak Ridge National Laboratory. These tests were conducted from April through June of 2015.

The calorimeter test loop consists of a compressor, a condenser, a sub-cooler, three electronic expansion valves, and an evaporator. Suction pressure, suction temperature, liquid temperature, compressor chamber air temperature, and discharge pressure are controlled independently by controlling the electronic expansion valve, evaporator heater, secondary glycol temperature, heating or cooling the air within the compressor chamber, and temperature of the condenser, respectively.

The compressor chamber air temperature was maintained between 94°F and 96°F. The compressor was uninsulated and airflow over the compressor was provided by two small fans with a total airflow rate of 750 CFM.

Figure 1 shows the schematic of the test loop and location of various sensors. Table 3 lists the accuracy of the test instruments used in the calorimeter.

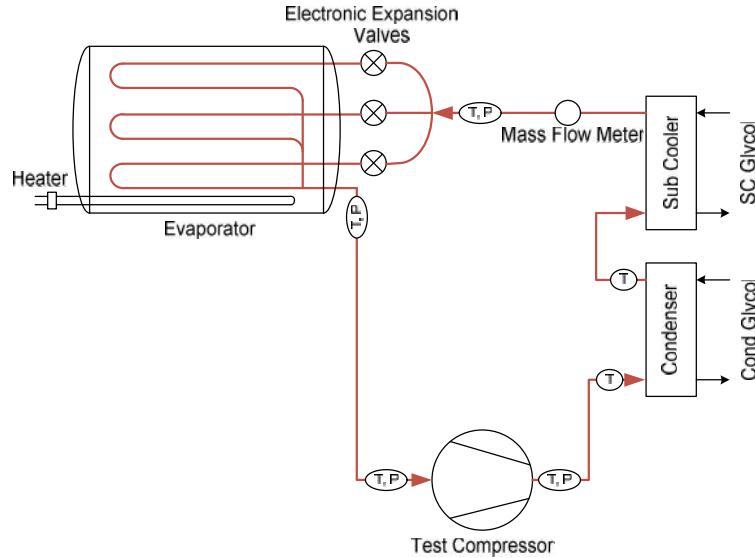


Figure 1: Location of various sensors in the test loop.

Table 3: Accuracy of test instruments

Instrument	Measured Parameter	Measurement Range	Accuracy
RTDs (tolerance class A)	Temperature	-58 °F to 572 °F	±0.40 °F
Micro Motion Elite CMF025 Coriolis mass flow meter	Refrigerant mass flow rate	25 lbm/min	0.10%
Honeywell Pressure Transmitter 060-F444-02	High side refrigerant pressure	750 psia	0.25% F.S.
Omega Pressure Transmitter PX409-250-AI	Low side refrigerant pressure	250 psia	0.08% B.S.L
Yokogawa Power and Energy Meter PR300	Compressor power	26000 watts	0.50% F.S.
Yokogawa Power and Energy Meter PR300	Compressor capacity	7500 watts	0.50% F. S.

3. Results

All compressor tests are performed at a refrigerant's dew point temperature for suction and discharge pressure conditions, per AHRI Standard 540 requirements. This does not have an impact on comparing compressor performance between two or more refrigerants that do not exhibit temperature glide. However, when refrigerants exhibit temperature glide, it is important to note that actual systems operate closer to the mid-point condition.

When comparing compressor performance of one refrigerant with glide to another refrigerant without glide, or comparing two refrigerants with significantly different glides, comparison at pressures corresponding to the mid-point of the temperature glide rather than the dew point will yield results that are more representative of actual operation in a system. The typical temperature glides of the tested refrigerants are listed in Table 1.

Test results and the coefficients for the AHRI 10-Coefficient Polynomial Equation are presented in the Appendices. The polynomial equation is of the form:

$$X = C_1 + C_2S + C_3D + C_4S^2 + C_5SD + C_6D^2 + C_7S^3 + C_8S^2D + C_9SD^2 + C_{10}D^3$$

Where:

C_N = Equation coefficient

S = Suction dew point temperature, °F

D = Discharge dew point temperature, °F

X can represent any of the following variables:

- Compressor Capacity, BTU/hr
- Power Input, W
- Current, A
- Mass flow rate, lbm/hr
- Isentropic efficiency, dimensionless
- Discharge Gas Temperature, °F

The following sections compare the performance of the Low-GWP blends with R-410A. In the following discussion, the 50 °F Evaporator / 110 °F Condenser condition (50/110) is chosen to represent a typical high efficiency air conditioning operating point

a. Honeywell L41-1

Figure 2 shows compressor capacity ratios with L41-1 relative to R-410A. At 50/110, the capacity ratio of L41-1 over R-410A is 0.84.

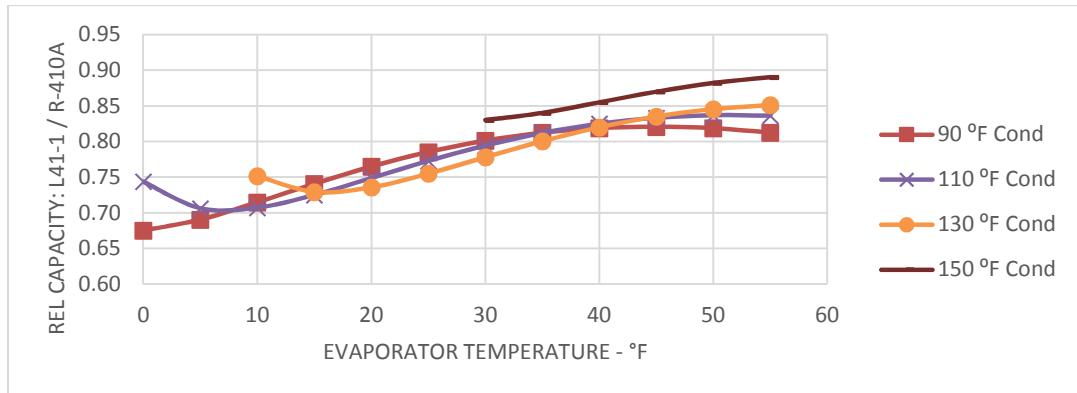


Figure 2: Compressor capacity ratios with L41-1 relative to R-410A

Figure 3 shows compressor energy efficiency ratios (EER) with L41-1 relative to R-410A. At 50/110 the EER ratio of L41-1 over R-410A is 0.97.

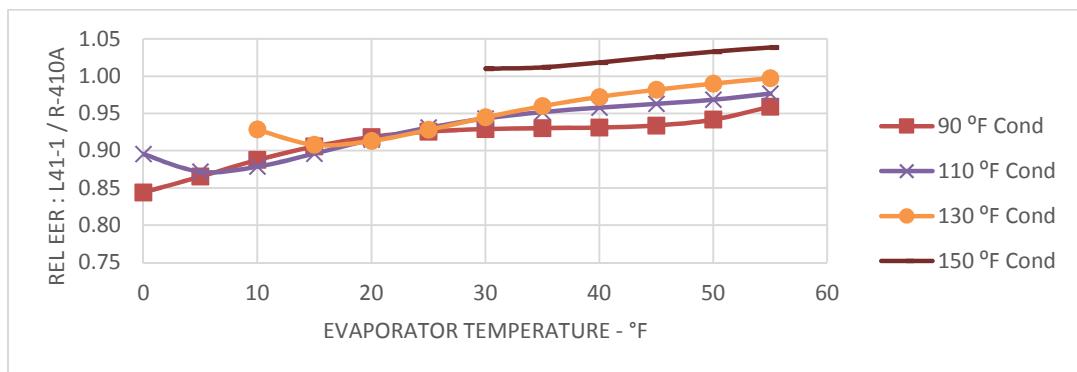


Figure 3: Compressor EER's with L41-1 relative to R-410A

Figure 4 shows compressor discharge gas temperatures with L41-1 relative to R-410A. At 50/110 the discharge gas with L41-1 is about 11 °F hotter than with R-410A.

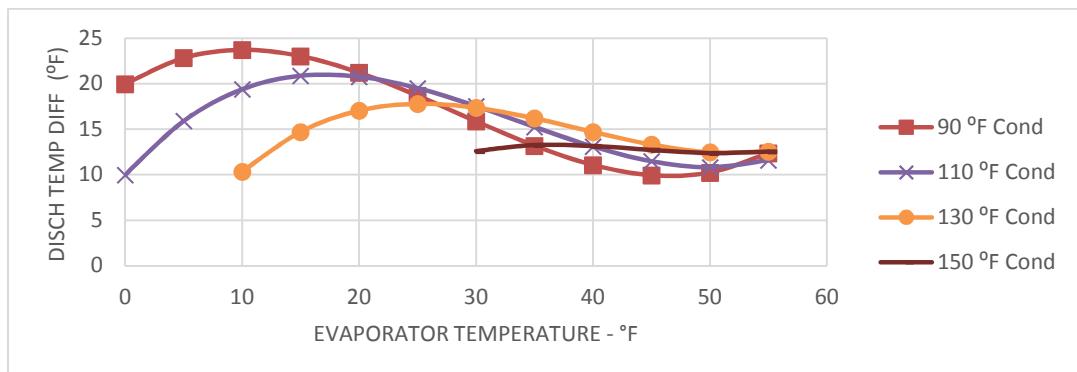


Figure 4: Compressor discharge gas temperatures with L41-1 relative to R-410A

b. Chemours DR-5A

Figure 5 shows compressor capacity ratios with DR-5A relative to R-410A. At 50/110 the capacity ratio of DR-5A over R-410A is 0.93.

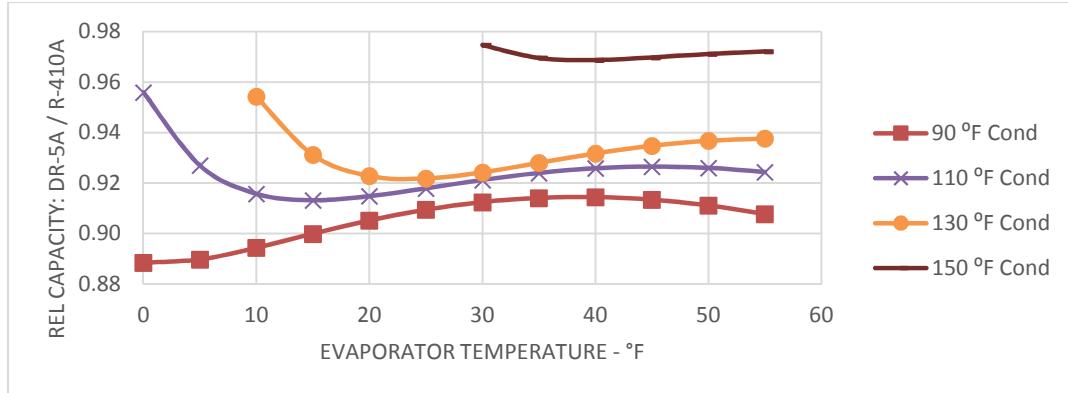


Figure 5: Compressor capacity ratios with DR-5A relative to R-410A

Figure 6 shows compressor energy efficiency ratios (EER) with DR-5A relative to R-410A. At 50/110 the EER ratio of DR-5A over R-410A is 0.98.

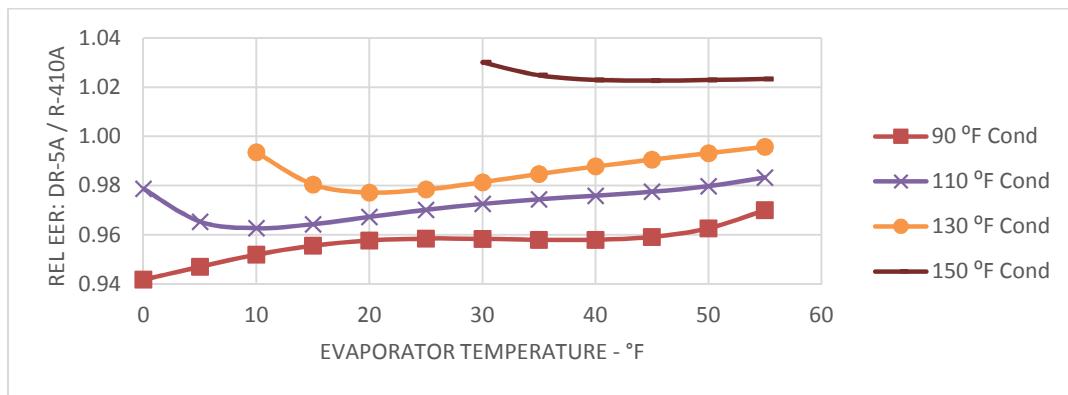


Figure 6: Compressor EER's with DR-5A relative to R-410A

Figure 7 shows discharge gas temperatures with DR-5A relative to R-410A. At 50/110 the discharge gas with DR-5A is about 8 °F hotter than with R-410A.

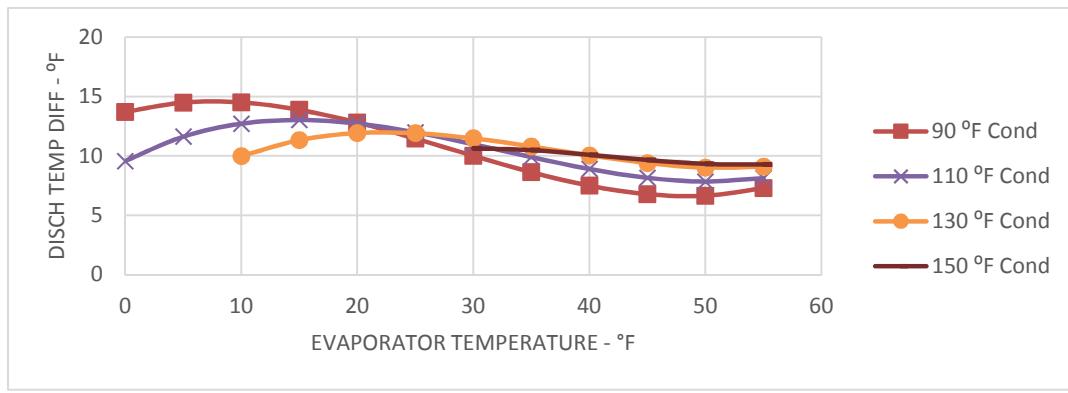


Figure 7: Compressor discharge gas temperatures with DR-5A relative to R-410A

c. Arkema ARM-71a

Figure 8 shows compressor capacity ratios with ARM-71a relative to R-410A. At 50/110 the capacity ratio of ARM-71a over R-410A is 0.91.

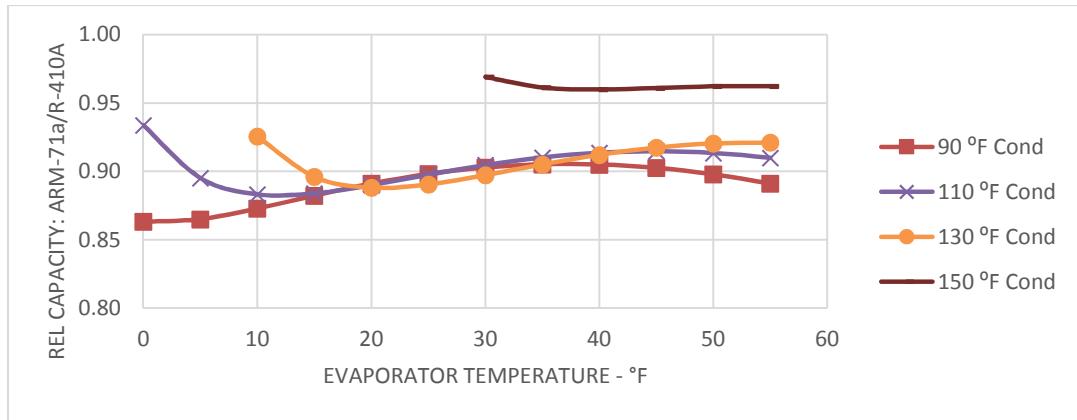


Figure 8: Compressor capacity ratios with ARM-71a relative to R-410A

Figure 9 shows compressor energy efficiency ratios (EER) with ARM-71a relative to R-410A. At 50/110 the EER ratio of ARM-71a over R-410A is 0.99.

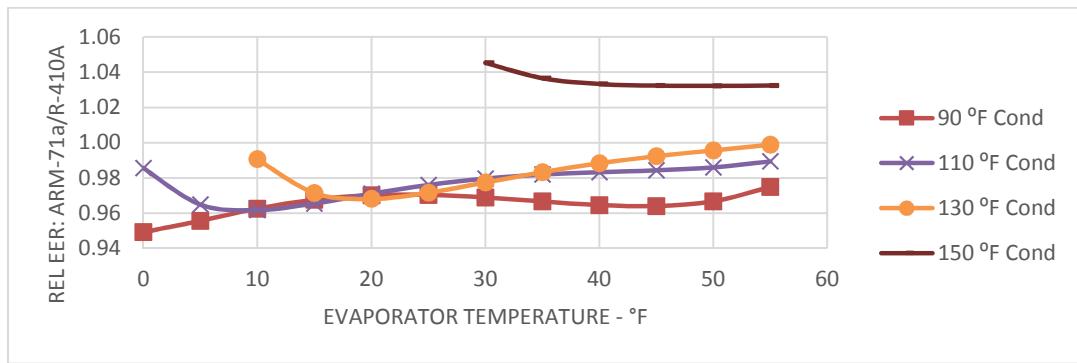


Figure 9: Compressor EER's with ARM-71a relative to R-410A

Figure 10 shows compressor discharge gas temperatures with ARM-71a relative to R-410A. At 50/110 the discharge gas with ARM-71a is about 8 °F hotter than with R-410A.

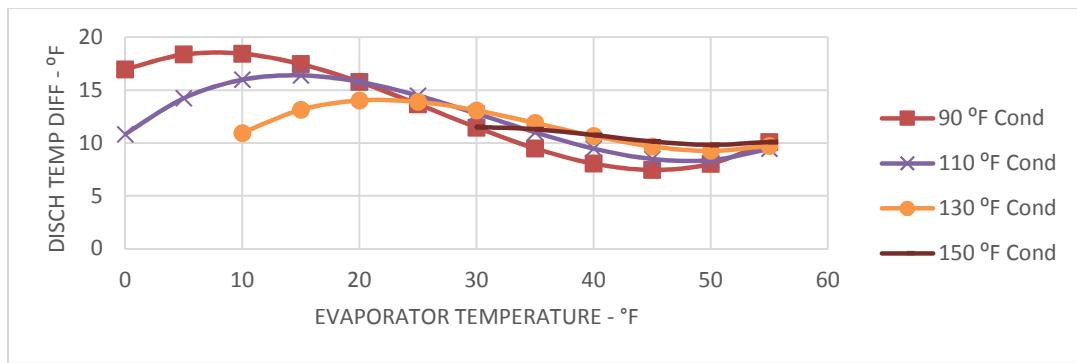


Figure 10: Compressor discharge gas temperatures with ARM-71a relative to R-410A

d. Daikin D2Y-60

Figure 11 shows compressor capacity ratios with D2Y-60 relative to R-410A. At 50/110 the capacity ratio with D2Y-60 is about 0.76.

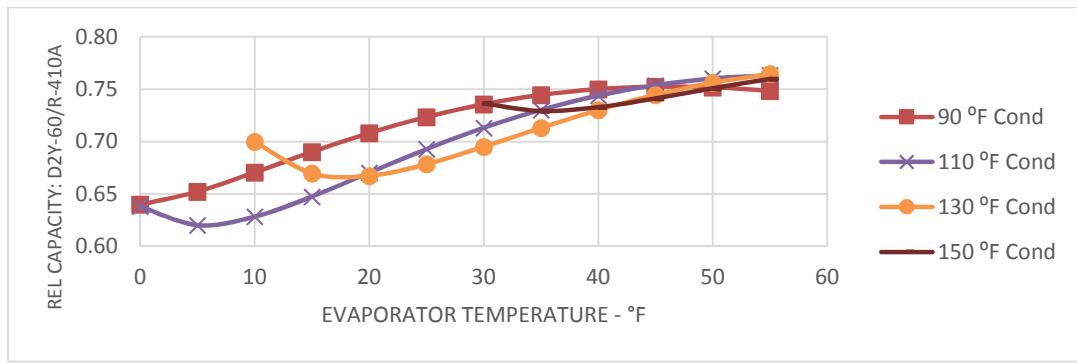


Figure 11: Compressor capacity ratios with D2Y-60 relative to R-410A

Figure 12 shows compressor energy efficiency ratios (EER) with D2Y-60 relative to R-410A. At 50/110 the EER ratio with D2Y-60 is about 0.98.

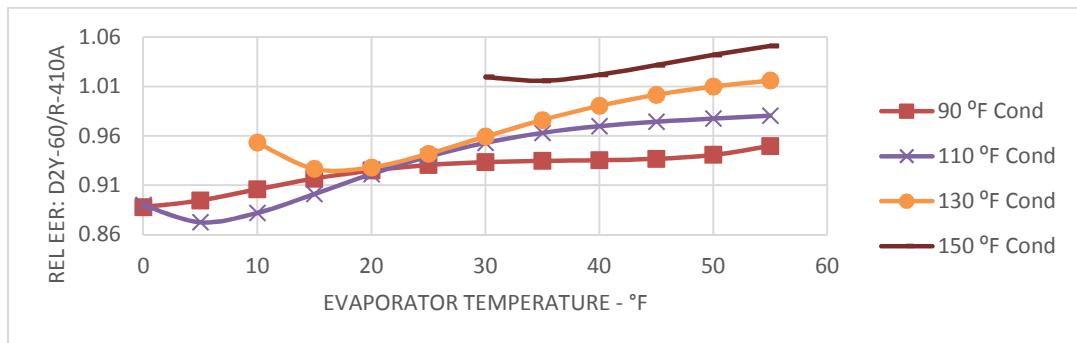


Figure 12: Compressor EER's with D2Y-60 relative to R-410A

Figure 13 shows compressor discharge gas temperatures with D2Y-60 relative to R-410A. At 50/110 the discharge gas with D2Y-60 is about 6 °F cooler than with R-410A.

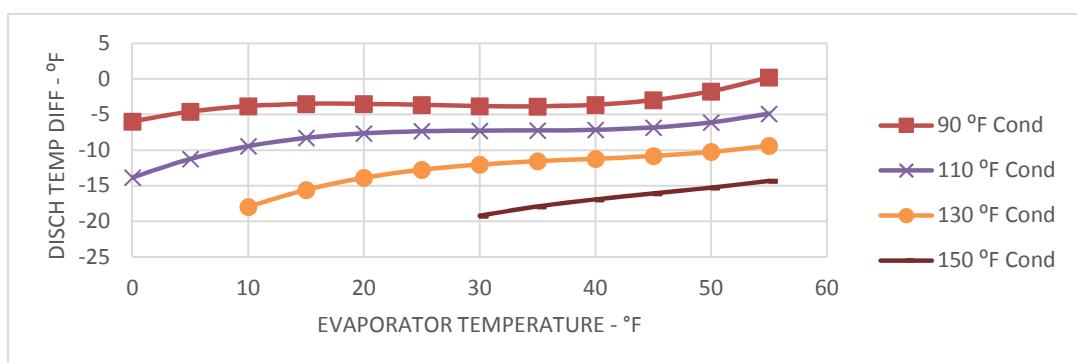


Figure 13: Compressor discharge gas temperatures with D2Y-60 relative to R-410A

e. R-32

Figure 14 shows compressor capacity ratios with R-32 relative to R-410A. At 50/110 the capacity ratio with R-32 is about 1.1.

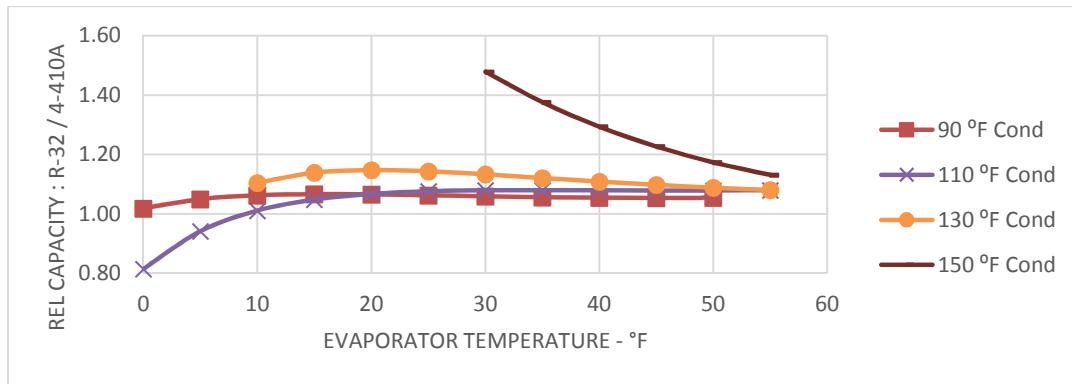


Figure 14: Compressor capacity ratios with R-32 relative to R-410A

Figure 15 shows compressor energy efficiency ratios (EER) with R-32 relative to R-410A. At 50/110 the EER ratio with R-32 is about 0.96.

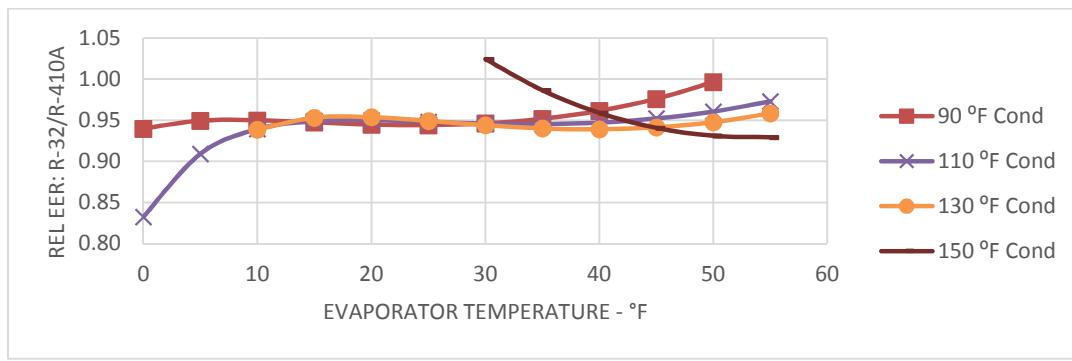


Figure 15: Compressor EER's with R-32 relative to R-410A

Figure 16 shows compressor discharge gas temperatures with R-32 relative to R-410A. At 50/110 the discharge gas with R-32 is about 27 °F hotter than with R-410A.

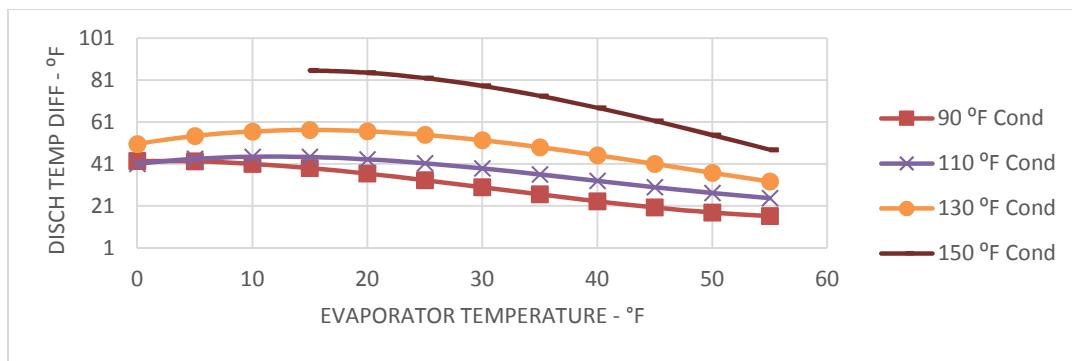


Figure 16: Compressor discharge gas temperatures with R-32 relative to R-410A

4. Conclusions

Calorimeter testing was done to establish ARI standard polynomial curve fits. The graphs in Section 3 above are taken from the resulting curves. Coefficients for the polynomial equations are presented in the appendix for each refrigerant. From the curve fit data we conclude that:

- All refrigerants tested slightly lower in EER than with R-410A, with a relative EER of 0.96 to 0.99 at 50/110 °F. R-32 tested lowest. ARM-71a tested highest.
- DR-5A gives the relative capacity that is closest to R-410A at 50/110 °F
- R-32 gives the highest relative capacity with value of 1.09 at 50/110 °F.
- Discharge temperature with R-32 were higher by 27 °F at 50/110 °F. Discharge temperatures with L41-1, DR-5A, and ARM-71a are 5 to 10°F higher than with R410A at 50/110 °F. Discharge temperatures were 6 °F lower with D2Y-60.

Note that the polynomial curves evaluated at 50/110 °F differ slightly from the experimental data at this point. The above conclusions are based on the curves, not the experimental data.

It should also be noted that an ISO 64 viscosity oil was used with R-32 and the Low-GWP blends, while an ISO 32 oil was used with R-410A. This is because R-32 dilutes POE oil more than R-410A, reducing the working viscosity of the oil-refrigerant mixture. The higher viscosity oil chosen for the Low-GWP refrigerants was an attempt to ensure, across the various operating conditions, that the working viscosity was not reduced. If a lower viscosity oil were to be used, the viscous friction losses would be expected to be reduced and EER might improve somewhat. However extensive testing would be required to ensure that bearing wear is not adversely effected.

Acknowledgements

The authors would like to thank Ed Hessell of Chemtura Corporation for his technical support in lubrication and selecting the lubricant used for the R32 blends tested in this work.

APPENDIX A
H84B223ABC at 60 Hz with R-410A

R-410A Calorimeter Data

Evaporator Dew Point (°F)	Condenser Dew Point (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
0	80	20.0	10525.2	1118.3	9.4	179.3	4.88	124.0
30	80	50.0	27077.6	1376.7	19.7	139.1	6.01	308.0
45	80	65.0	38647.7	1313.0	29.4	126.1	5.73	433.1
-10	90	10.0	5371.9	918.4	5.8	211.0	4.03	67.4
10	100	30.0	11273.7	1331.1	8.5	194.2	5.80	144.7
45	100	65.0	31620.0	1706.2	18.5	154.9	7.45	389.4
50	100	70.0	35356.1	1705.2	20.7	150.9	7.44	432.9
0	110	20.0	5993.7	1094.3	5.5	223.3	4.78	82.3
30	110	50.0	19245.2	1737.4	11.1	183.8	7.58	253.8
50	115	70.0	30199.0	1990.1	15.2	173.3	8.69	400.3
10	130	30.0	6786.6	1349.2	5.0	238.0	5.89	104.3
45	130	65.0	21922.5	2151.8	10.2	200.4	9.41	320.2
55	130	75.0	28275.3	2291.1	12.3	192.2	10.03	408.3
30	150	50.0	9405.1	1837.9	5.1	247.6	8.03	162.7
55	150	75.0	20766.7	2551.7	8.1	223.8	11.19	346.8

R-410A Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	3.98262E+04	1.59705E+03	7.27427E+00	4.53207E+02	9.86492E+01	4.28249E+01
C2	6.73112E+02	-1.04420E+01	-4.29370E-02	5.29081E+00	-3.85037E-01	-1.64740E+00
C3	-6.13930E+02	-1.98426E+01	-9.51098E-02	-7.58900E+00	-1.09876E+00	1.99877E+00
C4	5.56190E+00	-4.33685E-01	-1.89414E-03	3.69081E-02	-6.11332E-03	1.92469E-02
C5	-2.82264E+00	3.62324E-01	1.52440E-03	5.32846E-03	1.11781E-02	-4.23851E-03
C6	3.89156E+00	2.59366E-01	1.20854E-03	5.68501E-02	1.10514E-02	-4.57047E-03
C7	7.98980E-03	-1.13274E-03	-5.46298E-06	7.36835E-05	1.43876E-04	2.53057E-05
C8	-1.84008E-02	2.70266E-03	1.23588E-05	5.22869E-05	-1.14911E-04	-1.26519E-04
C9	-3.64562E-03	-3.31445E-04	-1.29636E-06	-1.35845E-04	5.23849E-06	5.27383E-05
C10	-9.95855E-03	-1.07994E-03	-4.92867E-06	-1.66813E-04	-4.42210E-05	1.17218E-05

APPENDIX B
H84B223ABC at 60 Hz with L41-1

L41-1 Calorimeter Data

Evaporator Dew Point (°F)	Condenser Dew Point (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
0	80	20.0	6827.5	871.2	7.8	203.2	3.83	62.5
30	80	50.0	21600.2	1201.2	18.0	153.9	5.24	191.9
45	80	65.0	31070.1	1150.0	27.0	136.2	5.02	272.2
-10	90	10.0	3947.7	778.7	5.1	217.4	3.42	38.1
10	100	30.0	8049.0	1069.5	7.5	216.2	4.68	79.1
45	100	65.0	26078.1	1482.5	17.6	166.2	6.48	246.9
50	100	70.0	29446.5	1477.5	19.9	161.2	6.45	277.6
0	110	20.0	4729.8	941.8	5.0	233.0	4.13	49.3
30	110	50.0	15145.6	1455.3	10.4	200.9	6.35	152.1
50	115	70.1	25308.7	1719.9	14.7	184.5	7.51	254.6
10	130	30.0	4830.7	1062.9	4.5	248.9	4.65	54.9
45	130	65.0	18396.1	1829.5	10.1	214.3	7.99	200.1
55	130	75.0	24207.0	1970.5	12.3	203.8	8.61	260.7
30	150	50.0	7962.9	1527.1	5.2	259.8	6.67	99.4
55	150	75.0	18342.2	2173.4	8.4	236.8	9.50	221.5

L41-1 Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	1.08976E+04	3.95520E+02	1.59095E+00	5.05537E+01	-1.26373E+02	1.05335E+02
C2	5.35249E+02	3.87105E-02	-2.62128E-03	2.66181E+00	1.27156E+00	-2.00404E+00
C3	5.93433E+01	7.39877E+00	3.72655E-02	2.02306E+00	4.09555E+00	9.79299E-01
C4	3.11738E+00	-3.98304E-01	-1.73602E-03	-6.37916E-03	2.19867E-02	1.07354E-02
C5	-2.57192E-01	2.53550E-01	1.13896E-03	4.62925E-02	-3.18594E-02	-7.55616E-03
C6	-2.18980E+00	-4.39018E-03	-7.02834E-05	-3.53967E-02	-2.80872E-02	6.66706E-03
C7	-4.43332E-02	-5.32245E-03	-2.28458E-05	-5.45149E-04	2.17180E-04	5.91888E-04
C8	4.45411E-02	6.05738E-03	2.63207E-05	8.42911E-04	-3.52766E-04	-5.67905E-04
C9	-2.92717E-02	-1.12826E-03	-5.04382E-06	-5.20874E-04	2.22191E-04	2.32496E-04
C10	1.02389E-02	-1.72810E-04	-5.85927E-07	1.51663E-04	5.43633E-05	-4.56391E-05

APPENDIX C
H84B223ABC at 60 Hz with DR-5A

DR-5A Calorimeter Data

Evaporator Dew Point (°F)	Condenser Dew Point (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
0	80	20.0	8985.65	1031.44	8.71	195.3	4.51	88.53
30	80	50.0	24472.85	1311.69	18.66	148.3	5.72	233.56
45	80	65.0	34765.60	1245.54	27.91	132.4	5.44	328.07
-10	90	10.0	4875.20	884.14	5.51	219.8	3.88	50.78
10	100	30.0	10223.18	1255.12	8.15	207.6	5.48	108.41
45	100	65.0	29040.24	1620.27	17.92	163.0	7.07	297.30
50	100	70.0	32667.22	1613.28	20.25	158.1	7.05	332.45
0	110	20.0	5956.80	1096.19	5.43	232.7	4.79	67.16
30	110	50.0	17583.84	1636.86	10.74	194.8	7.15	191.42
50	115	70.0	27963.08	1881.22	14.86	181.4	8.22	305.58
10	130	30.0	6288.86	1274.53	4.93	248.5	5.56	78.01
45	130	65.0	20646.20	2036.10	10.14	210.1	8.91	245.43
55	130	75.0	26544.19	2162.26	12.28	200.6	9.46	312.51
30	150	50.0	9252.49	1749.19	5.29	257.9	7.64	127.10
55	150	75.0	20103.45	2416.01	8.32	233.5	10.58	268.09

DR-5A Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	1.89666E+04	7.32874E+02	3.44567E+00	1.48559E+02	1.35335E+02	8.31969E+01
C2	6.30486E+02	2.54725E-01	2.44781E-03	4.07400E+00	1.32834E+00	-2.30010E+00
C3	-1.12821E+02	-3.16471E-01	-8.84466E-03	-3.55390E-01	-2.69215E+00	1.45295E+00
C4	3.86866E+00	-4.52039E-01	-1.90731E-03	1.03150E-02	-1.08098E-02	1.41277E-02
C5	-2.08811E+00	2.09683E-01	8.47864E-04	1.74904E-02	-1.47210E-02	3.18192E-03
C6	-3.93979E-01	9.67397E-02	4.99554E-04	-8.25075E-03	2.79656E-02	-2.04163E-04
C7	-9.62912E-03	-2.68460E-03	-1.20354E-05	-1.54018E-04	8.87571E-05	2.57124E-04
C8	9.49813E-03	4.27065E-03	1.83195E-05	3.94778E-04	2.79701E-05	-2.85826E-04
C9	-1.22974E-02	-2.73611E-04	-7.51698E-07	-2.72095E-04	5.42387E-05	8.20430E-05
C10	3.05629E-03	-5.85542E-04	-2.82281E-06	4.19043E-05	-9.18432E-05	-6.00897E-06

APPENDIX D
H84B223ABC at 60 Hz with ARM-71a

ARM-71a Calorimeter Data

Evaporator Dew Point (°F)	Condenser Dew Point (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
0	80	20.1	8671.47	992.67	8.74	198.5	4.36	84.46
30	80	50.0	24181.74	1288.07	18.77	149.5	5.63	227.97
45	80	64.7	34205.71	1227.08	27.88	133.3	5.37	319.63
-10	90	9.9	4897.10	866.04	5.65	219.8	3.82	50.35
10	100	30.1	9911.68	1211.70	8.18	212.1	5.31	103.53
45	100	65.0	28615.28	1588.99	18.01	163.7	6.94	289.98
50	100	70.0	32302.76	1582.25	20.42	158.7	6.91	324.41
0	110	20.0	5794.43	1059.30	5.47	233.5	4.64	64.57
30	110	50.0	17331.06	1598.74	10.84	195.8	6.98	186.46
50	115	70.0	27596.89	1843.42	14.97	182.0	8.06	298.22
10	130	30.0	6116.41	1242.34	4.92	249.6	5.44	74.80
45	130	65.0	20226.67	1991.56	10.16	210.7	8.69	237.40
55	130	75.0	26058.07	2119.66	12.29	201.1	9.28	302.92
30	150	50.0	9191.96	1713.31	5.37	258.7	7.49	124.40
55	150	75.0	19917.68	2371.20	8.40	234.3	10.38	261.78

ARM-71a Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	1.07249E+04	7.30363E+02	3.19532E+00	4.24926E+01	9.59292E+01	6.88821E+01
C2	5.97682E+02	3.47029E-01	2.70651E-03	3.43709E+00	2.90662E+00	-2.16024E+00
C3	1.25935E+02	-3.64231E-01	-8.90955E-04	2.83547E+00	-2.28510E+00	1.88803E+00
C4	3.28275E+00	-4.37716E-01	-1.93030E-03	1.47790E-05	1.06517E-02	1.25983E-02
C5	-1.06341E+00	2.24145E-01	9.46776E-04	3.61013E-02	-5.58159E-02	-2.42134E-03
C6	-2.78734E+00	8.46144E-02	3.62020E-04	-4.13207E-02	3.17968E-02	-2.85214E-03
C7	-2.35535E-02	-3.54449E-03	-1.50101E-05	-3.22208E-04	1.26556E-04	4.45227E-04
C8	2.52878E-02	4.86724E-03	2.12692E-05	6.15342E-04	-2.00663E-04	-4.23352E-04
C9	-2.12175E-02	-5.70170E-04	-2.34773E-06	-4.17934E-04	2.95349E-04	1.50186E-04
C10	1.11725E-02	-4.93935E-04	-2.13365E-06	1.56679E-04	-1.27657E-04	-6.19144E-06

APPENDIX E
H84B223ABC at 60 Hz with D2Y-60

D2Y-60 Calorimeter Data

Evaporator Dew Point (°F)	Condenser Dew Point (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
10	80	30.0	10662.7	974.4	10.9	161.5	4.27	124.9
30	80	50.0	20118.4	1114.9	18.0	137.2	4.87	228.6
45	80	65.0	28798.9	1070.2	26.9	125.2	4.68	321.0
0	90	20.0	5580.4	808.1	6.9	189.1	3.55	69.7
10	100	30.0	7193.7	950.1	7.6	188.5	4.17	92.6
45	100	65.0	23788.5	1344.2	17.7	150.3	5.88	290.2
50	100	70.0	26866.5	1342.3	20.0	146.7	5.88	324.8
0	110	20.0	4053.3	816.2	5.0	207.9	3.60	56.2
30	110	50.0	13706.6	1301.3	10.5	176.4	5.68	180.0
50	115	70.0	22893.0	1537.5	14.9	166.3	6.73	299.4
10	130	30.0	4569.2	970.1	4.7	221.1	4.25	70.1
45	130	65.0	16357.8	1596.8	10.2	189.5	6.99	234.6
55	130	75.0	21705.0	1732.7	12.5	182.6	7.59	306.9
30	150	50.0	7016.5	1337.5	5.2	228.0	5.84	120.1
55	150	75.0	15701.6	1838.0	8.5	209.8	8.04	255.7
0	100	20.0	4546.8	787.4	5.8	199.6	3.46	59.6
10	90	30.0	8863.3	969.8	9.1	174.5	4.24	108.9

D2Y-60 Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	3.16414E+04	1.72117E+03	7.50528E+00	2.87557E+02	7.92238E+01	5.59285E+01
C2	2.75625E+02	-2.02426E+01	-9.07118E-02	-9.39471E-01	8.94477E-01	-1.53167E+00
C3	-4.32196E+02	-2.11181E+01	-9.12925E-02	-2.23774E+00	-1.51525E+00	1.71245E+00
C4	2.26181E+00	-5.33215E-01	-2.29977E-03	-2.54038E-02	2.96180E-02	2.18856E-02
C5	4.03922E+00	7.12435E-01	3.12678E-03	1.36608E-01	-2.99449E-02	-1.04884E-02
C6	1.39755E+00	1.51004E-01	6.50720E-04	-1.55503E-02	2.21893E-02	-1.70786E-03
C7	-2.87529E-02	-3.22384E-03	-1.41770E-05	-5.31116E-04	1.33858E-04	2.20493E-04
C8	3.83108E-02	5.94698E-03	2.60763E-05	1.06938E-03	-3.75398E-04	-3.21926E-04
C9	-4.67049E-02	-3.51315E-03	-1.54575E-05	-1.00667E-03	2.31795E-04	1.50366E-04
C10	2.17919E-03	-3.19654E-04	-1.36346E-06	1.49273E-04	-9.42617E-05	-1.08842E-05

APPENDIX F
H84B223ABC at 60 Hz with R-32

R-32 Calorimeter Data

Evaporator Temp (°F)	Condenser Temp (°F)	Return Gas Temp (°F)	Cooling Capacity (BTU/hr)	Input Power (watts)	Cooling EER (BTU/W-hr)	Discharge Temp (°F)	Input Current (amps)	Mass Flow Rate (lbm/hr)
0	80	20.0	11180.7	1257.3	8.9	224.9	5.50	89.7
30	80	50.0	28259.2	1502.6	18.8	164.7	6.57	222.5
-10	90	9.8	4666.9	946.3	4.9	250.0	4.15	39.2
10	100	30.0	12238.3	1513.0	8.1	238.1	6.62	105.1
45	100	65.0	33681.9	1892.0	17.8	180.0	8.28	283.2
50	100	70.0	37863.9	1874.5	20.2	173.1	8.19	317.6
0	110	20.0	4413.3	1023.2	4.3	262.1	4.48	39.9
30	110	50.0	20491.5	1958.3	10.5	223.1	8.56	181.2
50	115	70.0	32570.9	2239.9	14.5	201.9	9.80	291.1
10	130	30.0	7604.9	1592.8	4.8	295.7	6.97	74.8
45	130	65.0	24085.7	2499.7	9.6	240.5	10.96	231.0
55	130	75.0	30837.1	2629.8	11.7	225.5	11.53	294.8
55	150	75.0	23338.9	3082.7	7.6	271.4	13.57	248.1
10	80	30.0	16045.1	1397.5	11.5	201.1	6.12	127.9
10	90	30.0	14030.3	1466.2	9.6	220.0	6.41	116.2
20	120	40.0	12969.0	1816.6	7.1	258.6	7.94	120.5

R-32 Polynomial Coefficients

	Capacity	Power	Line Current	Mass Flow	Efficiency	Discharge T
C1	1.67054E+04	-1.60762E+03	-7.52909E+00	-8.51495E+00	8.22013E+01	1.07418E+01
C2	-1.48840E+02	-1.07185E+02	-4.68919E-01	-4.12413E+00	-4.03942E+00	-6.51966E+00
C3	3.05508E+02	1.04004E+02	4.70924E-01	6.44120E+00	8.59642E-01	5.18780E+00
C4	6.14355E+00	-4.31747E-01	-1.93741E-03	4.28250E-02	-1.89501E-02	2.40077E-02
C5	1.28606E+01	2.17736E+00	9.54155E-03	1.49438E-01	9.09065E-02	7.39904E-02
C6	-7.04845E+00	-1.18541E+00	-5.35421E-03	-9.29621E-02	-2.28527E-02	-4.57028E-02
C7	3.38215E-02	-9.74890E-04	-4.87420E-06	3.21310E-04	2.94168E-04	2.83908E-04
C8	-4.94973E-02	8.66847E-04	4.75769E-06	-3.73754E-04	-1.28180E-04	-4.51279E-04
C9	-6.58719E-02	-7.61564E-03	-3.35757E-05	-6.67872E-04	-3.65768E-04	-2.04395E-04
C10	3.00254E-02	4.20852E-03	1.89978E-05	3.52804E-04	1.03352E-04	1.76925E-04

