AHRI Standard 700-2024 (SI)

Specifications for Refrigerants



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Note:

This standard supersedes AHRI Standard 700-2019 (SI).

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Intent

This standard is intended for the guidance of the industry, including manufacturers, engineers, installers, contractors, and users.

Review and Amendment

This standard is subject to review and amendment as technology advances.

2024 Edition

This edition of AHRI Standard 700 (SI), *Specifications for Refrigerants*, was prepared by the Refrigerants/Refrigerant Recovery Standards Technical Committee. The standard was approved by the Standards Committee on 12 December 2024.

Origin and Development of AHRI Standard 700 (SI)

The initial publication was ARI Standard 700-1988 (SI), *Specifications for Fluorocarbon and Other Refrigerants*. Subsequent revisions were:

ARI Standard 700-1993 (SI), Specifications for Fluorocarbon and Other Refrigerants ARI Standard 700-1995 (SI), Specifications for Fluorocarbon and Other Refrigerants ARI Standard 700-1999 (SI), Specifications for Fluorocarbon and Other Refrigerants ARI Standard 700-2004 (SI), Specifications for Fluorocarbon and Other Refrigerants AHRI Standard 700-2006 (SI), Specifications for Fluorocarbon Refrigerants AHRI Standard 700-2006 (SI) (with Addenda 1 and 2), Specifications for Fluorocarbon Refrigerants AHRI Standard 700-2011 (SI), Specifications for Fluorocarbon Refrigerants AHRI Standard 700-2011 (SI) (with Addendum 1), Specifications for Fluorocarbon Refrigerants AHRI Standard 700-2012 (SI), Specifications for Fluorocarbon Refrigerants AHRI Standard 700-2014 (SI), Specifications for Refrigerants AHRI Standard 700-2014 (SI) (with Addendum 1), Specifications for Refrigerants AHRI Standard 700-2015 (SI), Specifications for Refrigerants AHRI Standard 700-2015 (SI) (with Addendum 1), Specifications for Refrigerants AHRI Standard 700-2016 (SI), Specifications for Refrigerants AHRI Standard 700-2016 (with Addendum 1) (SI), Specifications for Refrigerants AHRI Standard 700-2017 (SI), Specifications for Refrigerants AHRI Standard 700-2017 (SI) (with Addendum 1), Specifications for Refrigerants AHRI Standard 700-2019 (SI), Specifications for Refrigerants

Summary of Changes

AHRI Standard 700-2024 (SI) contains the following updates to the previous edition:

- Update Refrigerants and specifications within AHRI 700
- Update sampling and test procedures
- Propose portions of the standard that can be moved to a continuous maintenance process
- Update <u>Appendix C</u> and <u>Appendix D</u>

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Refrigerants/Refrigerant Recovery Standards Technical Committee (STC) Scope:

The Refrigerants/Refrigerant Recovery STC is responsible for the development and maintenance of AHRI standards and guidelines pertaining to refrigerants as defined in ASHRAE 34, and related refrigerant recovery equipment.

Out of scope for this STC are refrigerants not defined in ASHRAE 34.

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These lists represent the membership at the time the Standards Technical Committee and Standards Subcommittee were balloted on the final text of this edition. Since that time, changes in the membership may have occurred. Membership on these committees shall not in and of itself constitute an endorsement by the committee members or their employers of any document developed by the committee on which the member serves.

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1

SPECIFICATIONS FOR REFRIGERANTS

2 Section 1. Purpose 3 This standard establishes purity specifications to verify composition, and to specify the associated methods of testing for 4 acceptability of the refrigerants listed in Section 2 regardless of source (new, reclaimed, or repackaged, or all three) for use in 5 new and existing refrigeration and air-conditioning products within the scope of AHRI. 6 Section 2. Scope 7 This standard specifies levels of contaminants (purity requirements) for fluorocarbon, hydrocarbon, and carbon dioxide 8 refrigerants regardless of source and lists test methods. These refrigerants are as referenced in ASHRAE 34 and in ISO 817: 9 2.1 Single Component Fluorocarbon Refrigerants 10 R-11; R-12; R-13; R-22; R-23; R-32; R-113; R-114; R-115; R-116; R-123; R-124; R-125; R-134a; R-141b; R-142b; R-143a; R-152a; R-218; R-227ea; R-236fa; R-245fa; R-1224yd(Z); R-1233zd(E); R-1234yf; R-1234ze(E); 11 12 R-1336mzz(Z); and R-1336mzz(E).-13 2.2 Single Component Hydrocarbon Refrigerants 14 R-50; R-170; R-E170; R-290; R-600; R-600a; R-601; R-601a; R-610; R-1150; and R-1270. 15 2.3 **Carbon Dioxide Refrigerant** 16 **R-744** 17 2.4 **Zeotropic Blend Refrigerants** 18 R-401A; R-401B; R-402A; R-402B; R-403A; R-403B; R-404A; R-405A; R-406A; R-407A; R-407B; R-407C; R-407D; R-407E; R-407F; R-407G; R-407H; R-407I; R-408A; R-409A; R-409B; R-410A; R-410B; R-411A; 19 20 R-411B: R-412A: R-413A: R-414A: R-414B: R-415A: R-415B: R-416A: R-417A: R-417B: R-417C: R-418A: 21 R-419A; R-420A; R-421A; R-421B; R-422A; R-422B; R-422C; R-422D; R-422E; R-423A; R-424A; 22 R-425A; R-426A; R-427A; R-428A; R-429A; R-430A; R-431A; R-434A; R-435A; R-437A; R-438A; R-439A; 23 R-440A; R-442A; R-444A; R-444B; R-445A; R-446A; R-447A; R-447B; R-448A;; R-449A; R-449B; R-449C; 24 R-450A; R-451A; R-451B; R-452A; R-452B; R-452C; R-453A; R-454A; R-454B; R-454C; R-454D; R-455A; R-455B; R-455C; R-456A; R-457A; R-457B; R-457C; R-457D; R-459B; R-460A; R-460B; R-460C; R-461A; 25 R-462A; R-463A; R-464A; R-465A; R-466A; R-467A; R-468A; R-468B; R-468C; R-469A; R-470A; R-470B; 26 R-471A; R-472A; R-472B; R-473A; R-475A; R-476A; R-477A; R-477B; and R-478A. 27 28 2.5 Zeotropic Hydrocarbon Blend Refrigerants 29 R-432A; R-433A; R-433B; R-433C; R-436A; R-436B; R-441A; and R-443A. 30 2.6 **Azeotropic Blend Refrigerants** 31 R-500; R-502; R-503; R-507A; R-508A; R-508B; R-509A; R-510A; R-511A; R-512A; R-513A; R-513B; R-514A; 32 R-515A; R-515B; and R-516A. Section 3. Definitions 33 34 All terms in this document follow the standard industry definitions in the ASHRAE Terminology website unless otherwise 35 defined in Section 3.2. These standard-specific defined terms are italicized throughout the standard. 36 3.1 **Expression of Provisions** 37 Terms that provide clear distinctions between requirements, recommendations, permissions, options, and capabilities. "Can" or "cannot" 38 3.1.1 39 Express an option or capability.

40		3.1.2	"May"		
41			Signifies a permission expressed by the document.		
42		3.1.3	"Must"		
43 44			Indication of unavoidable situations and does not mean that an external constraint referred to is a requirement of the document.		
45		3.1.4	"Shall" or "shall not"		
46			Indication of mandatory requirements to strictly conform to the standard and where deviation is not permitted.		
47		3.1.5	"Should" or "should not"		
48 49			Indication of recommendations rather than requirements. In the negative form, a recommendation is the expression of potential choices or courses of action that is not preferred but not prohibited.		
50	3.2	Standa	ard-specific Definitions		
51		3.2.1	Boiling Point		
52 53			Temperature at which the vapor pressure of a liquid equals the absolute external pressure at the liquid vapor interface.		
54		3.2.2	Boiling Point Range		
55			The temperature range involved in the distillation of oil, from the start to the time when the oil evaporates.		
56		3.2.3	Bubble Point		
57			Refrigerant liquid saturation temperature at a specified pressure.		
58		3.2.4	Critical Temperatures		
59 60			The temperature at and above where vapor of the substance cannot be liquefied, no matter how much pressure is applied.		
61		3.2.5	Dew Point		
62			Refrigerant vapor saturation temperature at a specified pressure.		
63		3.2.6	Effective Carbon Number (ECN)		
64 65			The instrumental response factor calculated based on functional groups (or descriptors) present in molecular structure of a volatile organic compound.		
66		3.2.7	Effective Carbon Number Method (ECN Method)		
67			Method to external calibration method by applying ECN for quantitative analysis of compounds.		
68		3.2.8	High Boiling Residue (HBR)		
69			Non-volatile material remaining in the Goetz bulb upon completion of the analysis.		
70			Note: Can be called non-volatile residue.		
71		3.2.9	Non-condensable Gas (NCG)		
72			Any gas that does not condense to liquid phase in a system.		
73			Section 4. Test Requirements		
74	4.1	Refere	Referee Test		
75			ed test procedures are included in <u>Appendix C</u> . If alternative test methods are employed, the user shall be able		
76		to demonstrate that the results are at least equal to the specified referee test method.			

77 4.2 Refrigerant Sampling

4.2.1 Sampling Precautions

Representative samples shall be obtained for analysis. Sampling shall be done by qualified personnel following accepted sampling and safety procedures. Refrigerants with *critical temperatures* at or less than the ambient temperature cannot be reliably sampled for both a liquid phase and a vapor phase without special handling. Refrigerants that are ASHRAE 34 Class 2L, Class 2, or Class 3 are flammable.

4.2.2 Cylinder Preparation

Place a clean, empty sample cylinder with the valve open in an oven at 110°C for one hour. Remove the sample cylinder from the oven while hot, immediately connect the sample cylinder to an evacuation system, and evacuate the cylinder to less than 56 kPa. Close the valve and let the cylinder cool. Weigh the empty cylinder.

4.2.3 Vapor Phase Sampling

A vapor phase sample shall be obtained for determining the non-condensables. The source temperature shall be measured and recorded at the time the sample is taken.

4.2.3.1 Special Handling for Low Critical Temperature Refrigerant

A vapor phase sample is required to determine non-condensables and volatile impurities, including other refrigerants. The vapor phase sample is obtained by regulating the sample container temperature to 5K or more above the refrigerant *critical temperature*.

4.2.3.2 Handling for Liquid Refrigerants with Boiling Points At or Above Room Temperature

Since R-11, R-113, R-123, R-141b, R-245fa, R-514A, R-1233zd(E), R-1336mzz(Z), and R-1336mzz(E) have *boiling points* at or above room temperature, non-condensable determination is not required for these refrigerants.

Note: If present, *NCG* concentrate in the vapor phase of the refrigerant. The introduction of either air or liquid phase refrigerant during the sample transfer should be eliminated.

4.2.4 Liquid Phase Sampling

A liquid phase sample shall be used for all tests listed in this standard except the test for non-condensables.

4.2.4.1 Liquid Sampling

The sample cylinder, at ambient temperature, shall be filled to at least 60% by volume but not greater than 80%. This can be accomplished by weighing the empty cylinder and then the cylinder with refrigerant. When the required amount of refrigerant is collected, close the valve(s) and immediately disconnect the sample cylinder.

For low pressure refrigerants not requiring *NCG*, submitted samples shall be in either metal cylinders or in glass or plastic bottles such that the containers are at least 80% liquid full.

- Note: All connections and transfer lines should be dry and evacuated to prevent contaminating the sample.
 - Note: Low *critical temperature* refrigerants can have extremely high pressure at the sampling vessel.
 - Note: Expansion of refrigerant under transportation conditions should be considered.

All connections and transfer lines shall be designed to handle high pressures.

4.2.4.2 Special Handling for Low Critical Temperature Refrigerant

A liquid phase sample shall be used for all testing except volatile impurities, including other refrigerants. The liquid phase sample is obtained by regulating the sample cylinder temperature to $2^{\circ}C$ less than the *critical temperature* of the refrigerant.

Note: If free water is present in the sample, cooling to less than 0°C can result in the formation of ice. Clathrates can form at temperatures greater than 0°C with fluorocarbon refrigerants.

124 Check the sample cylinder for leaks and record the gross weight. 125 4.3 Refrigerant Identification 126 The require method shall be gas chromatography as described in <u>Appendix C</u> with the corresponding gas chromatogram figures as illustrated in <u>Appendix D</u> . The chromatogram of the sample shall be compared to known standards. 129 4.4 Water Content 130 4.1.1 Method 131 The coulometric Karl Fischer (KF) titration, as described in <u>Appendix C</u> , shall be used for determining the water content of refigerants, this method can be used for refigerants that are either a liquid or age sat room temperature. For all refrigerants, the sample for water analysis shall be taken from the liquid phase of the container to be tested. 135 4.2.2 Limits 136 The value for water content shall be expressed in parts per million (ppm) by weight and shall not exceed the maximum specific day in Table 1 through Table 23. 139 4.5 Conductivity (Alternative to Chloride and Acidly Tests) 141 A refrigerant can be tested for conductivity as an indication of the presence of acids, metal chlorides, and any compound that ionizzes in water. This alternative procedure is intended for use with new or reclaimed refrigerants, the value for conductivity is greater than this amount, then the chloride and acidity tests shall be converted to and expressed in pun by weight calculated as hydrochloric acid (HCI) and shall be compared with the maximum acidity vatue specified (see in Table 1 through Table 23	123			4.2.4.3	Record Weight
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127 chromatogram figures as illustrated in Appendix D. The chromatogram of the sample shall be compared to known standards. 128 4.4 Water Content 139 4.1 Method 131 The conlometric Karl Fischer (KF) thration, as described in Appendix C, shall be used for determining the water content of refrigerants. This method can be used for refrigerants that are cither a liquid or a gas at room temperature. For all refrigerants, the sample for water analysis shall be taken from the liquid phase of the container to be tested. 136 4.2 Limits 137 The value for water content shall be expressed in parts per million (ppm) by weight and shall not exceed the maximum specified in Table 1 through Table 23. When considering compliance, uncertainty has been taken into account with Table 1 through Table 23. When considering compliance, uncertainty has been taken into account with Table 1 through Table 23. 140 A refrigerant can be tested for conductivity as an indication of the presence of acids, metal chlorides, and any compound that ionizes in water. This alternative procedure is intended for use with new or reclaimed refrigerants; however, oil can interfere with the test results. 144 4.5 Limits 145 Hourdot in the conductivity is not greater than this amount, then the chloride and acidity tests shall be conducted. If the conductivity is not greater than this amount, then the chloride and acidity tests. 146 A.6 Method 151 4.6	125	4.3	Refrige	rant Identi	fication
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152The refrigerant shall be tested for chloride as an indication of the presence of hydrochloric acid or metal chlorides, or both. The referee procedure is intended for use with new or reclaimed halogenated refrigerants; however, <i>HBR</i> greater than the amounts in Table 1 through Table 23 can interfere with the test results.155The test method shall be that as described in Appendix C. The test shall show turbidity at chloride levels of 3 ppm or greater by weight.157 4.6.2 Limits158The results of the test shall not exhibit any sign of turbidity. Record the results as either "Pass" or "Fail."159 4.7 Acidity160 4.7.1 Method161The acidity test uses the titration principle to detect any compound that is soluble in water and ionizes as an acid. The test method shall be that as described in Appendix C. This test shall not be used for determination of high molecular weight organic acids. However, these acids are found in the <i>HBR</i> test outlined in Section <u>4.8</u> . The test shall have a fifty-gram to sixty-gram sample and a detection limit (DL) of 0.1 ppm by	150	4.6	Chlorid	le	
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	162 163 164			acid. The t of high m Section <u>4.8</u>	est method shall be that as described in <u>Appendix C</u> . This test shall not be used for determination olecular weight organic acids. However, these acids are found in the <i>HBR</i> test outlined in <u>B</u> . The test shall have a fifty-gram to sixty-gram sample and a detection limit (DL) of 0.1 ppm by

166		4.7.2	Limits	
167 168				Table 1 and Table 6 through Table 23. The formula $\frac{1}{1000}$ and $\frac{1}{1000}$ and $\frac{1}{1000}$ and $\frac{1}{1000}$ and $\frac{1}{1000}$ and $\frac{1}{10000}$ and $\frac{1}{10000000000000000000000000000000000$
169	4.8	High B	oiling Residu	e
170		4.8.1	Method	
171 172 173			standard vol	be determined by either volume or weight. The volume method measures the residue from a ume of refrigerant after evaporation. The gravimetric method is described in <u>Appendix C</u> . Oils cids, or both shall be captured by these methods.
174		4.8.2	Limits	
175 176				r <i>HBR</i> shall be expressed as a percentage by volume or weight and shall not exceed the maximum ified in <u>Table 1</u> through Table 23.
177	4.9	Particu	lates and Sol	ids
178		4.9.1	Method	
179 180 181			The particula	ed amount of sample shall be placed in a Goetz bulb under controlled temperature conditions. ates/solids shall be determined by visual examination of the Goetz bulb prior to the evaporation t. For details of this test method, refer to Section $\underline{C.3}$.
182 183 184			solid R-744	Illy sublimates when measuring a known amount of liquid sample into the Goetz bulb and the interferes with the visual examination of particulates/solids. Determining the particulates/solids pleted by visual examination of the Goetz bulb after the evaporation of the refrigerant.
185		4.9.2	Limits	
186			Visual prese	nce of dirt, rust or other particulate contamination is a failed test.
187	4.10	Non-co	ndensables	
188		4.10.1	Method	
189 190 191 192			accumulated extremely lo	is e sample shall be used for determination of non-condensables. <i>NCGs</i> consist primarily of air in the vapor phase of refrigerants where the solubility of air in the refrigerant liquid phase is w and air is extremely low as a liquid phase contaminant. The presence of <i>NCGs</i> can reflect poor of in transferring refrigerants to storage tanks and cylinders.
193 194			The test met <u>Appendix C</u>	thod shall be gas chromatography with a thermal conductivity detector (TCD) as described in
195		4.10.2	Limits	
196 197				m level of non-condensables in the vapor phase of a test sample shall not exceed the maximum shown in <u>Table 1</u> through Table 23.
198	4.11	All Oth	er Volatile Iı	npurities and Other Refrigerants
199		4.11.1	Method	
200 201				of volatile impurities including other refrigerants in the subject refrigerant shall be determined natography as described in <u>Appendix C</u> .
202		4.11.2	Limits	
203 204			The test sam and unsatura	ple shall not contain more than 0.5% by weight of volatile impurities including other refrigerants tes.
205			4.11.2.1	Individual Listed Volatile Impurities
206 207				<u>Table 1</u> through Table 23 list specific volatile impurities and their maximum allowable concentrations in percent (%) by weight.
208			4.11.2.2	R-40 Impurities
				Refrigerant shall not contain more than 300 ppm of R-40.

210	4.12	Total C	C3, C4, and C5 Polyolefins in Hydrocarbon Refrigerants
211		4.12.1	Method
212 213			The amount of polyolefin impurities in the hydrocarbon shall be determined by gas chromatography as described in GPA 2177.
214		4.12.2	Limits
215 216			The test sample shall not contain more than 0.05 % by weight in the hydrocarbon sample as shown in <u>Table 4</u> and <u>Table 21</u> . Record the results as either "Pass" or "Fail."
217	4.13	Sulfur	Odor in Hydrocarbon Refrigerants
218		4.13.1	Method
219 220			The amount of sulfur-containing compounds or other compounds with an odor shall be determined in accordance with ASTM D1296.
221		4.13.2	Limits
222			The test sample paper shall not emit a residual sulfur odor as shown in <u>Table 4</u> and <u>Table 21</u> .
223			Section 5. Rating Requirements
224	This st	andard do	es not have any applicable rating requirements.
225			Section 6. Minimum Data Requirements for Published Ratings
226	This st	andard do	es not establish requirements for published ratings.
227			Section 7. Conformance Conditions
228 229 230	within	the standa	nce with this standard is voluntary, conformance shall not be claimed or implied for products or equipment ard's <u>Purpose</u> (Section 1) and Scope (Section 2) unless such product claims meet all of the requirements of the of the testing and rating requirements are in complete compliance with the standard. Any product that has not

standard and an or the testing and rating requirements are in complete compliance with the standard. Any product that has not met all the requirements of the standard cannot reference, state, or acknowledge conformance to the standard in any written, oral, or electronic communication.

231 232

	- cabie					ough R-116						
	Reporting Units	Reference Section	R-11	R-12	R-13	R-22	R-23	R-32	R-113	R-114	R-115	R-116
					Character	ristics						
Boiling Point ¹	°C at 101.3 kPa	N/A	23.7	-29.8	-81.5	-40.8	-82	-51.7	47.6	3.6	-38.9	-78.2
Boiling Point Range ¹	K	N/A	± 0.3	± 0.3	± 0.5	± 0.3	± 0.5	± 0.3	± 0.3	± 0.3	± 0.3	± 0.3
Critical Temperature ¹	°C	N/A	198	112	28.9	96.2	26.1	78.1	214.1	145.7	80	19.9
Isomer(s)		N/A	N/A	N/A	N/A	N/A	N/A	N/A	R-113a	R-114a	N/A	N/A
Quantity of Isomer(s)	% by weight	N/A	N/A	N/A	N/A	N/A	N/A	N/A	0-1	0-30	N/A	N/A
				Vap	or Phase Co	ontaminants	5					
Air and Other Non- condensables, Maximum	% by volume at 25.0°C	4.10	N/A ²	1.5	1.5	1.5	1.5	1.5	N/A ²	1.5	1.5	1.5
				Liqu	id Phase Co	ontaminants	5					
Water, Maximum	ppm by weight	4.4	20	10	10	10	10	10	20	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01

 Table 1 Single Component Fluorocarbon Refrigerants Characteristics and Allowable Levels of Contaminants (R-11 through R-116)

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	Reporting Units	Reference Section	R-11	R-12	R-13	R-22	R-23	R-32	R-113	R-114	R-115	R-116
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1	1	1
Chloride ³	Pass or Fail	4.6	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	Visually clean	Visually clean

Notes:

1. Boiling points, boiling ranges, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Because R-11, R-113, R-123, R-141b, R-245fa, R-1233zd(E), R-1366mzz(E) and R-1336mzz(Z) have *boiling points* equal to or greater than the room temperature, testing for non-condensables is not required for these refrigerants.

3. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable; --- = Intentionally left blank

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Table 2 Single Component Fluorocarbon Refrigerants Characteristics and Allowable Levels of Contaminants (R-123 through R-227ea)

	Reporting Units	Reference Section	R-123	R-124	R-125	R-134a	R-141b	R-142b	R-143a	R-152a	R-218	R-227ea		
					Charac	teristics								
Boiling Point ¹	°C at 101.3 kPa	N/A	27.8	-12	-48.1	-26.1	32	-9.2	-47.2	-24	-36.8	-16.5		
Boiling Point Range ¹	К	N/A	±0.3	±0.3	±0.3	±0.3	±0.3	N/A	±0.3	±0.3	±0.3	N/A		
Critical Temperature ¹	°C	N/A	183.7	122.3	66	101.1	206.8	137.1	72.7	113.3	72	101.7		
Isomer(s)		N/A	R-123a R-123b	R-124a	N/A	R-134	R-141 R-141a	R-142 R-142a	R-143	N/A	N/A	N/A		
Quantity of Isomer	% by weight	N/A	0-8 of each	0-5	N/A	0-0.5	0-0.1 of each	0-0.1 of each	0-0.01	N/A	N/A	N/A		
	Vapor Phase Contaminants													
Air and Other Non- condensables, Maximum	% by volume at 25.0 °C	4.10	N/A ²	1.5	1.5	1.5	N/A ²	2	1.5	1.5	1.5	1.5		
				Lie	quid Phase	Contamina	nts			•				
Water, Maximum	ppm by weight	4.4	20	10	10	10	100	15	10	10	10	10		
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.9	0.5	0.5	0.5	0.5	0.5		
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01		
Particulates/ Solids	Pass or Fail	4.9	Visually clean											

	Reporting Units	Reference Section	R-123	R-124	R-125	R-134a	R-141b	R-142b	R-143a	R-152a	R-218	R-227ea
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	3	1	1	1	1
Chloride ³	Pass or Fail	4.6	No visible turbidity									

1. *Boiling points*, boiling ranges, and *critical temperatures*, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Because R-11, R-113, R-123, R-141b, R-245fa, R-1233zd(E), R-1336mzz(E) and R-1336mzz(Z) have *boiling points* at or above room temperature, non-condensable determinations are not required for these refrigerants.

3. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable; — = Intentionally left blank

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Table 3 Single Component Fluorocarbon Refrigerants Characteristics and Allowable Levels of Contaminants [R-236f through R-1336mzz(E)]

	Reporting Units	Reference Section	R-236fa	R-245fa	R-1224yd(Z)	R-1233zd(E)	R-1234yf	R-1234ze(E)	R-1336mzz(Z)	R-1336mzz(E)
					Characteristics	i -				
Boiling Point ¹	°C @ 101.3 kPa	N/A	-1.4	14.9	14.5	18.3	-29.4	-19	33.4	7.4
Boiling Point Range ¹	K	N/A	±0.3	±0.3	N/A	N/A	N/A	N/A	N/A	N/A
Critical Temperature ¹	°C	N/A	124.9	154.1	155.5	165.6	94.8	109.4	171.3	130.2
Isomer(s)		N/A	N/A	R-245ca, R-245cb, R-245ea, R-245eb	R-1224yd(E)	N/A	N/A	R-1234ze(Z)	R-1336mzz(E)	R-1336mzz(Z)
Quantity of Isomer	% by weight	N/A	N/A	0-0.1 of each	0-1.0	N/A	N/A	0-0.3	0-0.1	0-0.1
				Vapor	Phase Contam	inants				
Air and Other Non- condensables, Maximum	% by volume @ 25°C	4.10	1.5	N/A ²	N/A ²	N/A ²	1.5	1.5	N/A ²	N/A ²
				Liquid	Phase Contam	inants				
Water, Maximum	ppm by weight	4.4	10	20	20	20	10	10	20	20
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5

	Reporting Units	Reference Section	R-236fa	R-245fa	R-1224yd(Z)	R-1233zd(E)	R-1234yf	R-1234ze(E)	R-1336mzz(Z)	R-1336mzz(E)
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean							
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ³	Pass or Fail	4.6	No visible turbidity							

1. Boiling points, boiling ranges, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Because R-11, R-113, R-123, R-141b, R-245fa, R-1233zd(E), R-1336mzz(E), and R-1336mzz(Z) have *boiling points* at or above room temperature, non-condensable determinations are not required for these refrigerants.

3. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable; --- = Intentionally left blank

	Table 4	Single Com	ponent Hy	drocarbor	n Refrigera	nts Chara	cteristics	and Allowa	able Level	s of Conta	minants		
	Reporting Units	Reference Section	R-50	R-170	R-E170	R-290	R-600	R-600a	R-601	R-601a	R-610	R-1150	R-1270
					Ch	aracteristic	es						
Boiling Point ¹	°C at 101.3 kPa	N/A	-161.5	-88.6	-24.8	-42.1	-0.5	-11.8	36.1	27.8	34.6	-103.8	-47.6
Boiling Point Range ¹	К	N/A	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5	±0.5
Minimum Nominal Composition	% weight	N/A	99.5	99.5	99.5	99.5	99.5	99.5	99.5	99.5	99.5	99.5	99.5
Allowable Impurities		N/A	N/A	N/A	N/A	N/A	N/A	N/A	R-601a	R-601	N/A	N/A	R-290
Allowable Impurity Quantity	% weight	N/A	N/A	N/A	N/A	2 ²	2 ²	2 ²	0-1	0-1	N/A	N/A	0-1
					Vapor Ph	ase Contan	ninants ³						
Air and Other Non- condensables, Maximum	% by volume at 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
					Liquid Pl	nase Contar	ninants ⁴				•	•	1
Sulphur Odor	Pass or Fail	4.13	No sulfur odor	No sulfur odor									
HBR, Maximum	% weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1	1	1	1
Water, Maximum	mg/kg	4.4	10	10	10	10	10	10	10	10	10	10	10

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	Reporting Units	Reference Section	R-50	R-170	R-E170	R-290	R-600	R-600a	R-601	R-601 a	R-610	R-1150	R-1270
All Other Volatile Impurities, Maximum	% weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Total C ₃ , C ₄ , and C ₅ Polyolefins, Maximum	% weight	4.12	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05

Notes:

1. Boiling points and boiling point ranges are provided for informational purposes.

2. Two percent of other C3 and C4 saturated hydrocarbons can be used.

3. Taken from vapor phase.

4. Vaporized from liquid phase.

N/A = Not applicable; — = Intentionally left blank

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Table 5 Carbon Dioxide Refrigerant Characteristics and Allowable Levels of Contaminants

	Reporting Units	R-744
	Characteristics	
Sublimation Point ¹	°C at 101 kPa	-78.4
Sublimation Point Range ¹	К	± 0.3
	Vapor Phase Contaminants ²	
Air and Other Non- condensables, Maximum	% by volume at 10°C less than the <i>critical temperature</i> and measure non-condensable directly	1.5
	Liquid Phase Contaminants ³	
Water, Maximum	ppm by weight	10
HBR, Maximum	% by weight	0.0005
Particulates/Solids	Pass or Fail	Visually clean
Minimum Purity	% by weight	99.9
Notes:		

1. Sublimation point and sublimation point range are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Sample taken from vapor phase.

3. Sample vaporized from liquid phase.

	Table 6 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-401A through R-405A)												
	Reporting Units	Reference Section	R-401A	R-401B	R-402A	R-402B	R-403A	R-403B	R-404A	R-405A			
					Characteri	stics							
Refrigerant Components	N/A	N/A	R-22/ 152a/ 124	R-22/ 152a/ 124	R-125/ 290/ 22	R-125/ 290/ 22	R-290/ 22/ 218	R-290/ 22/ 218	R-125/ 143a/ 134a	R-22/ 152a/ 142b/ C318			
Nominal Composition	% by weight	N/A	53.0/ 13.0/ 34.0	61.0/ 11.0/ 28.0	60.0/ 2.0/ 38.0	38.0/ 2.0/ 60.0	5.0/ 75.0/ 20.0	5.0/ 56.0/ 39.0	44.0/ 52.0/ 4.0	45.0/ 7.0/ 5.5/ 42.5			
Allowable Composition	% by weight	N/A	51.0-55.0/ 11.5-13.5/ 33.0-35.0	59.0-63.0/ 9.5-11.5/ 27.0-29.0	58.0-62.0/ 1.0-2.1/ 36.0-40.0	36.0-40.0/ 1.0-2.1/ 58.0-62.0	3.0-5.2/ 73.0-77.0/ 18.0-22.0	3.0-5.2/ 54.0-58.0/ 37.0-41.0	42.0-46.0/ 51.0-53.0/ 2.0-6.0	43.0-47.0/ 6.0-8.0/ 4.5-6.5/ 40.5-44.5			
Bubble Point ¹	°C @ 101.3 kPa	N/A	-33.3	-34.9	-49	-47	-47.8	-49.2	-46.2	-32.9			
Dew Point ¹	°C @ 101.3 kPa	N/A	-26.4	-28.8	-46.9	-44.7	-44.3	-46.8	-45.5	-24.5			
Critical Temperature	°C	N/A	105.3	103.5	76	83	87	79.7	72.1	106			
				Vaj	por Phase Cor	ntaminants	·	·	·				
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5			

	Reporting Units	Reference Section	R-401A	R-401B	R-402A	R-402B	R-403A	R-403B	R-404A	R-405A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean							
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

		(R-406A through R-407G)												
	Reporting Units	Reference Section	R-406A	R-407A	R-407B	R-407C	R-407D	R-407E	R-407 F	R-407G				
					Characteri	stics								
Refrigerant Components	N/A	N/A	R-22/ 600a/ 142b	R-32/ 125/ 134a	R-32/ 125/ 134a	R-32/ 125/ 134a	R-32/ 125/ 134a	R-32/ 125/ 134a	R-32/ 125/ 134a	R-32/ 125/ 134a				
Nominal Composition	% by weight	N/A	55.0/ 4.0/ 41.0	20.0/ 40.0/ 40.0	10.0/ 70.0/ 20.0	23.0/ 25.0/ 52.0	15.0/ 15.0/ 70.0	25.0/ 15.0/ 60.0	30.0/ 30.0/ 40.0	2.5/ 2.5/ 95.0				
Allowable Composition	% by weight	N/A	53.0-57.0/ 3.0-5.0/ 40.0-42.0	18.0-22.0/ 38.0-42.0/ 38.0-42.0	8.0-12.0/ 68.0-72.0/ 18.0-22.0	21.0-25.0/ 23.0-27.0/ 50.0-54.0	13.0-17.0/ 13.0-17.0/ 68.0-72.0	23.0-27.0/ 13.0-17.0/ 58.0-62.0	28.0-32.0/ 28.0-32.0/ 38.0-42.0	2.0-3.0/ 2.0-3.0/ 94.0-96.0				
Bubble Point ¹	°C @ 101.3 kPa	N/A	-32.7	-45.3	-46.8	-43.6	-39.5	-42.9	-46.1	-29.2				
Dew Point ¹	°C @ 101.3 kPa	N/A	-23.5	-38.9	-42.5	-36.6	-32.9	-35.8	-39.7	-27.2				
Critical Temperature	°C	N/A	116.5	82.3	75	86	91.4	88.5	83	99.5				
				Vaj	oor Phase Cor	itaminants								
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5				

	Reporting Units	Reference Section	R-406A	R-407A	R-407B	R-407C	R-407D	R-407E	R-407F	R-407G
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	Table 8 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-407H through R-411A)												
	Reporting Units	Reference Section	R-407H	R-407I	R-408A	R-409A	R-409B	R-410A	R-410B	R-411A			
	I	Γ		Γ	Characteri	stics							
Refrigerant Components	N/A	N/A	R-32/ 125/ 134a	R-32/ 125/ 134a	R-125/ 143a/ 22	R-22/ 124/ 142b	R-22/ 124/ 142b	R-32/ 125	R-32/ 125	R-1270/ 22/ 152a			
Nominal Composition	% by weight	N/A	32.5/ 15.0/ 52.5	19.5/ 8.5/ 72.0	7.0/ 46.0/ 47.0	60.0/ 25.0/ 15.0	65.0/ 25.0/ 10.0	50.0/ 50.0	45.0/ 55.0	1.5/ 87.5/ 11.0			
Allowable Composition	% by weight	N/A	31.5-33.5/ 14.0-16.0/ 50.5-54.5	17.5-20.5/ 7.5-10.5/ 70.0-74.0	5.0-9.0/ 45.0-47.0/ 45.0-49.0	58.0-62.0/ 23.0-27.0/ 14.0-16.0	63.0-67.0/ 23.0-27.0/ 9.0-11.0	48.5-50.5/ 49.5-51.5	44.0-46.0/ 54.0-56.0	0.5-1.5/ 87.5-89.5/ 10.0-11.0			
Bubble Point ¹	°C @ 101.3 kPa	N/A	-44.6	-39.8	-44.6	-34.7	-35.6	-51.4	-51.3	-39.5			
Dew Point ¹	°C @ 101.3 kPa	N/A	-37.6	-33.0	-44.1	-26.4	-27.9	-51.4	-51.6	-36.6			
Critical Temperature	°C	N/A	86.5	92.0	83.1	106.9	106.9	71.4	70.8	99.1			
				Vaj	por Phase Cor	ntaminants							
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5			

	Reporting Units	Reference Section	R-407H	R-407I	R-408A	R-409A	R-409B	R-410A	R-410B	R-411A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean							
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

					(R-411B	through R-41	l6A)			
	Reporting Units	Reference Section	R-411B	R-412A	R-413A	R-414A	R-414B	R-415A	R-415B	R-416A
					Characteri	stics				
Refrigerant Components	N/A	N/A	R-1270/ 22/ 152a	R-22/ 218/ 142b	R-218/ 134a/ 600a	R-218/ 124/ 600a/ 142b	R-22/ 124/ 600a/ 142b	R-22/ 152a	R-22/ 152a	R-134a/ 124/ 600
Nominal Composition	% by weight	N/A	3.0/ 94.0/ 3.0	70.0/ 5.0/ 25.0	9.0/ 88.0/ 3.0	51.0/ 28.5/ 4.0/ 16.5	50.0/ 39.0/ 1.5/ 9.5	82.0/ 18.0	25.0/ 75.0	59.0/ 39.5/ 1.5
Allowable Composition	% by weight	N/A	2.0-3.0/ 94.0-96.0/ 2.0-3.0	68.0-72.0/ 3.0-7.0/ 24.0-26.0	8.0-10.0/ 86.0-90.0/ 2.0-3.0	49.0-53.0/ 26.5-30.5/ 3.5-4.5/ 15.5-17.0	48.0-52.0/ 37.0-41.0/ 1.0-2.0/ 8.5-10.0	81.0-83.0/ 17.0-19.0	24.0-26.0/ 74.0-76.0	58.0-59.5/ 39.0-40.5/ 1.3-1.6
Bubble Point ¹	°C @ 101.3 kPa	N/A	-41.6	-38	-30.6	-34	-32.9	-37.5	-27.7	-23.4
Dew Point ¹	°C @ 101.3 kPa	N/A	-40	-28.7	-27.9	-25.8	-24.3	-34.7	-26.2	-21.8
Critical Temperature	°C	N/A	96	107.2	98.5	110.7	111	100	111.3	108.2
				Vaj	por Phase Cor	ntaminants				
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

Table 9 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-411B through R-416A)

	Reporting Units	Reference Section	R-411B	R-412A	R-413A	R-414A	R-414B	R-415A	R-415B	R-416A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	Table 10 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-417A through R-421A)												
	Reporting Units	Reference Section	R-417A	R-417B	R-417C	R-418A	R-419A	R-419B	R-420A	R-421A			
					Characteri	stics							
Refrigerant Components	N/A	N/A	R-125/ 134a/ 600	R-125/ 134a/ 600	R-125/ 134a/ 600	R-290/ 22/ 152a	R-125/ 134a/ E170	R-125/ 134a/ E170	R-134a/ 142b	R-125/ 134a			
Nominal Composition	% by weight	N/A	46.6/ 50.0/ 3.4	79.0/ 18.3/ 2.7	19.5/ 78.8/ 1.7	1.5/ 96.0/ 2.5	77.0/ 19.0/ 4.0	48.5/ 48.0/ 3.5	88.0/ 12.0	58.0/ 42.0			
Allowable Composition	% by weight	N/A	45.5-47.7/ 49.0-51.0/ 3.0-3.5	78.0-80.0/ 17.3-19.3/ 2.2-2.8	18.5-20.5/ 77.8-79.8/ 1.2-1.8	1.0-2.0/ 95.0-97.0/ 2.0-3.0	76.0-78.0/ 18.0-20.0/ 3.0-5.0	47.5-49.5/ 47.0-49.0/ 3.0-4.0	88.0-89.0/ 11.0-12.0	57.0-59.0/ 41.0-43.0			
Bubble Point ¹	°C @ 101.3 kPa	N/A	-38	-44	-32.7	-41.2	-42.6	-37.4	-25	-40.8			
Dew Point ¹	°C @ 101.3 kPa	N/A	-32.9	-41.5	-29.2	-40.1	-36	-31.5	-24.2	-35.5			
Critical Temperature	°C	N/A	89.9	75.2	95.4	96.7	79.1	90.4	105.4	78.5			
				Vap	oor Phase Con	taminants:							
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5			

	Reporting Units	Reference Section	R-417A	R-417B	R-417C	R-418A	R-419A	R-419B	R-420A	R-421A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	20	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

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Table 11 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-421B through R-424A)

	Reporting Units	Reference Section	R-421B	R-422A	R-422B	R-422C	R-422D	R-422E	R-423A	R-424A
					Characteri	stics				
Refrigerant Components	N/A	N/A	R-125/ 134a	R-125/ 134a/ 600a	R-125/ 134a/ 600a	R-125/ 134a/ 600a	R-125/ 134a/ 600a	R-125/ 134a/ 600a	R-134a/ 227ea	R-125/ 134a/ 600a/ 600/ 601a
Nominal Composition	% by weight	N/A	85.0/ 15.0	85.1/ 11.5/ 3.4	55.0/ 42.0/ 3.0	82.0/ 15.0/ 3.0	65.1/ 30.5/ 3.4	58.0/ 39.3/ 2.7	52.5/ 47.5	50.5/ 47.0/ 0.9/ 1.0/ 0.6
Allowable Composition	% by weight	N/A	84.0-86.0/ 14.0-16.0	84.1-86.1/ 10.5-12.5/ 3.0-3.5	54.0-56.0/ 41.0-43.0/ 2.5-3.1	81.0-83.0/ 14.0-16.0/ 2.5-3.1	64.0-66.0/ 30.5-32.5/ 3.0-3.5	57.0-59.0/ 38.0-41.0/ 2.5-3.0	51.5-53.5/ 46.5-48.5	49.5-51.5/ 46.0-48.0/ 0.7-1.0/ 0.8-1.1/ 0.4-0.7
Bubble Point ¹	°C @ 101.3 kPa	N/A	-45.7	-46.5	-40.5	-45.3	-43.2	-41.8	-24.2	-39.1
Dew Point ¹	°C @ 101.3 kPa	N/A	-42.6	-44.1	-35.6	-42.3	-38.4	-36.4	-23.5	-33.3
Critical Temperature	°C	N/A	69	71.7	85.7	76.1	79.6	82.2	99	87.5
				Vaj	por Phase Cor	ntaminants				
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

	Reporting Units	Reference Section	R-421B	R-422A	R-422B	R-422C	R-422D	R-422E	R-423A	R-424A			
	Liquid Phase Contaminants												
Water, Maximum	ppm by weight	4.4	10	10	10	20	10	10	10	10			
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5			
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01			
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean			
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1			
Chloride ²	Pass or Fail	4.6	No visible turbidity										

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	Та	ble 12 Zeotr	opic Blends	s (400 Serie		ts) Characteri through R-43	stics and Allov 1A)	wable Levels o	of Contami
	Reporting Units	Reference Section	R-425A	R-426A	R-427A	R-428A	R-429A	R-430A	R-431A
				Cha	racteristics				
Refrigerant Components	N/A	N/A	R-32/ 134a/ 227ea	R-125/ 134a/ 600/ 601a	R-32/ 125/ 143a/ 134a	R-125/ 143a/ 290/ 600a	R-E170/ 152a/ 600a	R-152a/ 600a	R290/ 152a
Nominal Composition	% by weight	N/A	18.5/ 69.5/ 12.0	5.1/ 93.0/ 1.3/ 0.6	15.0/ 25.0/ 10.0/ 50.0	77.5/ 20.0/ 0.6/ 1.9	60.0/ 10.0/ 30.0	76.0/ 24.0	71.0/29.0
Allowable Composition	% by weight	N/A	18.0-19.0/ 69.0-70.0/ 11.5-12.5	4.1-6.1/ 92.0-94.0/ 1.1-1.4/ 0.4-0.7	13.0-17.0/ 23.0-27.0/ 8.0-12.0/ 48.0-52.0	76.5-78.5/ 19.0-21.0/ 0.4-0.7/ 1.7-2.0	59.0-61.0/ 9.0-11.0/ 29.0-31.0	75.0-77.0/ 23.0-25.0	70.0-72.0/ 28.0-30.0
Bubble Point ¹	°C @ 101.3 kPa	N/A	-38.1	-28.5	-43	-48.3	-25.5	-27.6	-43.2
Dew Point ¹	°C @ 101.3 kPa	N/A	-31.3	-26.7	-36.3	-47.5	-24.9	-27.4	-43.2
Critical Temperature	°C	N/A	93.9	100.2	85.3	69	123.5	107	100.3
				Vapor Ph	ase Contamin	ants			
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5

	Reporting Units	Reference Section	R-425A	R-426A	R-427A	R-428A	R-429A	R-430A	R-431A
				Liquid Ph	ase Contamin	ants			
Water, Maximum	ppm by weight	4.4	10	10	10	10	20	20	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity						
comp	<i>le points, dew</i> biled from REF	FPROP 10.0.	ŕ		ugh not requir	ed, are provided	l for information	nal purposes. Re	frigerant data

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

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Table 13 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants
(R-434A through R-442A)

	Reporting Units	Reference Section	R-434A	R-435A	R-437A	R-438A	R-439A	R-440A	R-442A		
				Cha	racteristics						
Refrigerant Components	N/A	N/A	R-125/ 143a/ 134a/ 600a	R-E170/ 152a	R-125/ 134a/ 600/ 601	R-32/ 125/ 134a/ 600/ 601a	R-32/ 125/ 600a	R-290/ 134a/ 152a	R-32/ 125/ 134a/ 152a/ 227ea		
Nominal Composition	% by weight	N/A	63.2/18.0/ 16.0/2.8	80.0/20.0	19.5/ 78.5/ 1.4/0.6	8.5/ 45.0/ 44.2/ 1.7/ 0.6	50.0/ 47.0/ 3.0	0.6/ 1.6/ 97.8	31.0/ 31.0/ 30.0/ 3.0/ 5.0		
Allowable Composition	% by weight	N/A	62.2-64.2/ 17.0-19.0/ 15.0-17.0/ 2.6-2.9	79.0-81.0/ 19.0-21.0	17.7-20.0/ 77.8-80.0/ 1.2-1.5/ 0.4-0.7	7.0-9.0/ 43.5-46.5/ 42.7-45.7/ 1.5-1.8/ 0.4-0.7	49.0-51.0/ 46.0-48.0/ 2.5-3.5	0.5-0.7/ 1.0-2.2/ 97.3-98.3	30.0-32.0/ 30.0-32.0/ 29.0-31.0/ 2.5-3.5/ 4.0-6.0		
Bubble Point ¹	°C @ 101.3 kPa	N/A	-45.1	-26	-32.9	-43	-52	-25.5	-46.5		
Dew Point ¹	°C @ 101.3 kPa	N/A	-42.4	-25.8	-29.2	-36.4	-51.7	-24.3	-39.9		
Critical Temperature	°C	N/A	75.6	125.2	95.3	84.2	72	112.9	82.4		
				Vapor Pha	ase Contamin	ants					
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5		

	Reporting Units	Reference Section	R-434A	R-435A	R-437A	R-438A	R-439A	R-440A	R-442A
				Liquid Ph	ase Contamin	ants			
Water, Maximum	ppm by weight	4.4	10	20	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity						
	le points, dew biled from REF		critical tempe	ratures, altho	ugh not requir	red, are provid	ed for informat	ional purposes. I	Refrigerant data

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

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Table 14 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-444A through R-449A)

	Reporting Units	Reference Section	R-444A	R-444B	R-445A	R-446A	R-447A	R-447B	R-448A	R-449A
					Characteri	stics				
Refrigerant Components	N/A	N/A	R-32/ 152a/ 1234ze(E)	R-32/ 152a/ 1234ze(E)	R-744/ 134a/ 1234ze(E)	R-32/ 1234ze(E)/ 600	R-32/ 125/ 1234ze(E)	R-32/ 125/ 1234ze(E)	R-32/ 125/ 1234yf/ 134a/ 1234ze(E)	R-32/ 125/ 1234yf/ 134a
Nominal Composition	% by weight	N/A	12.0/ 5.0/ 83.0	41.5/ 10.0/ 48.5	6.0/ 9.0/ 85.0	68.0/ 29.0/ 3.0	68.0/ 3.5/ 28.5	68.0/ 8.0/ 24.0	26.0/ 26.0/ 20.0/ 21.0/ 7.0	24.3/ 24.7/ 25.3/ 25.7
Allowable Composition	% by weight	N/A	11.0-13.0/ 4.0-6.0/ 81.0-85.0	40.5-42.5/ 9.0-11.0/ 47.5-49.5	5.0-7.0/ 8.0-10.0/ 83.0-87.0	67.0-68.5/ 28.4-31.0/ 2.0-3.1	67.5-69.5/ 3.0-5.0/ 27.5-29.5	66.0-69.0/ 7.0-10.0/ 22.0-25.0	24.0-26.5/ 25.5-28.0/ 18.0-20.5/ 20.0-23.0/ 5.0-7.5	23.3-24.5/ 24.5-25.7/ 24.3-25.5/ 25.5-26.7
Bubble Point ¹	°C @ 101.3 kPa	N/A	-34.3	-44.6	-50.3	-49.4	-49.3	-50.0	-45.9	-46
Dew Point ¹	°C @ 101.3 kPa	N/A	-24.3	-34.9	-23.5	-42.1	-44.2	-46.0	-39.8	-39.9
Critical Temperature	°C	N/A	103.2	91.5	98	84.2	82.6	83.6	81.6	81.5
				Vaj	oor Phase Cor	ntaminants				
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

	Reporting Units	Reference Section	R-444A	R-444B	R-445A	R-446A	R-447A	R-447B	R-448A	R-449A			
	Liquid Phase Contaminants												
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10			
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5			
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01			
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean			
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	N/A	1	1	1	1	1			
Chloride ²	Pass or Fail	4.6	No visible turbidity										

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	(R-449B through R-452C)													
	Reporting Units	Reference Section	R-449B	R-449C	R-450A	R-451A	R-451B	R-452A	R-452B	R-452C				
					Characteri	stics								
Refrigerant Components	N/A	N/A	R-32/ 125/ 1234yf/ 134a	R-32/ 125/ 1234yf/ 134a	R-134a/ 1234ze(E)	R-1234yf/ 134a	R-1234yf/ 134a	R-32/ 125/ 1234yf	R-32/ 125/ 1234yf	R-32/ 125/ 1234yf				
Nominal Composition	% by weight	N/A	25.2/2 4.3/ 23.2/ 27.3	20.0/ 20.0/ 31.0/ 29.0	42.0/ 58.0	89.8/ 10.2	88.8/ 11.2	11.0/ 59.0/ 30.0	67.0/ 7.0/ 26.0	12.5/ 61.0/ 26.5				
Allowable Composition	% by weight	N/A	23.7-25.5/ 24.0-25.8/ 21.7-23.5/ 27.0-28.8	18.5-20.5/ 19.5-21.5/ 29.5-31.5/ 28.5-30.5	40.0-44.0/ 56.0-60.0	89.6-90.0/ 10.0-10.4	88.6-89.0/ 11.0-11.4	9.3-12.7/ 57.2-60.8/ 29.0-30.1	65.0-69.0/ 5.5-8.5/ 24.0-28.0	11.0-13.0/ 60.0-62.0/ 25.0-27.0				
Bubble Point ¹	°C @ 101.3 kPa	N/A	-46.1	-44.6	-23.4	-30.8	-31	-47	-51.0	-47.5				
Dew Point ¹	°C @ 101.3 kPa	N/A	-40.2	-38.1	-22.8	-30.5	-30.6	-43.2	-50.3	-44.2				
Critical Temperature	°C	N/A	84.2	83.5	104.4	95.4	95.5	74.9	75.7	75.8				
				Vaj	por Phase Cor	ntaminants	·		·					
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5				

 Table 15 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-449B through R-452C)

	Reporting Units	Reference Section	R-449B	R-449C	R-450A	R-451A	R-451B	R-452A	R-452B	R-452C
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean							
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	(R-453A through R-455C)												
	Reporting Units	Reference Section	R-453A	R-454A	R-454B	R-454C	R-454D	R-455A	R-455B	R-455C			
					Characteri	stics							
Refrigerant Components	N/A	N/A	R-32/ 125/ 134a/ 227ea/ 600/601a	R-32/ 1234yf	R-32/ 1234yf	R-32/ 1234yf	R-32/ 1234yf	R-744/ 32/ 1234yf	R-744/ 32/ 1234yf	R-744/ 32/ 1234yf			
Nominal Composition	% by weight	N/A	20.0/20.0/ 53.8/5.0/ 0.6/0.6	35.0/ 65.0	68.9/ 31.1	21.5/ 78.5	43.0/ 57.0	3.0/ 21.5/ 75.5	6.0/ 42.0/ 52.0	7.5/ 78.0/ 54.0			
Allowable Composition	% by weight	N/A	19.0-21.0/ 19.0-21.0/ 52.8-54.8/ 4.5-5.5/ 0.4-0.7/ 0.4-0.7	33.0-37.0/ 63.0-67.0	67.9-69.9/ 30.1-32.1	19.5-23.5/ 76.5-80.5	41.0-45.0/ 55.0-59.0	2.0-5.0/ 19.5-22.5/ 73.5-77.5	5.5-6.5/ 41.0-43.0/ 51.0-53.0	2.0-3.5/ 41.0-45.0/ 52.0-56.0			
Bubble Point ¹	°C @ 101.3 kPa	N/A	-42.2	-48.4	-50.9	-46.0	-48.7	-51.6	-57.4	-53.4			
Dew Point ¹	°C @ 101.3 kPa	N/A	-35	-41.6	-50.0	-37.8	-44.5	-39.1	-46.7	-45.7			
Critical Temperature	°C	N/A	88	86.2	76.5	82.4	80.2	82.8	77.6	78.8			
				Vaj	por Phase Cor	ntaminants							
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5			

 Table 16 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-453A through R-455C)

	Reporting Units	Reference Section	R-453A	R-454A	R-454B	R-454C	R-454D	R-455A	R-455B	R-455C
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	N/A	N/A	N/A
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	Table 17 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-456A through R-460B)												
	Reporting Units	Reference Section	R-456A	R-457A	R-457B	R-457C	R-457D	R-459B	R-460A	R-460B			
					Characteri	stics							
Refrigerant Components	N/A	N/A	R-32/ 134a/ 1234ze(E)	R-32/ 1234yf/ 152a	R-32/ 1234yf/ 152a	R-32/ 1234yf/ 152a	R-32/ 1234yf/ 152a	R-32/ 1234yf/ 1234ze(E)	R-32/ 125/ 134a/ 1234ze(E)	R-32/ 125/ 134a/ 1234ze(E)			
Nominal Composition	% by weight	N/A	6.0/45.0/ 49.0	18.0/70.0/ 12.0	35.0/ 55.0/ 10.0	7.5/ 78.0/ 14.5	4.0/ 82.0/ 14.0	21.0/ 69.0/ 10.0	12.0/ 52.0/ 14.0/ 22.0	28.0/ 25.0/ 20.0/ 27.0			
Allowable Composition	% by weight	N/A	5.0-7.0/ 44.0-46.0/ 48.0-50.0	16.5-18.5/ 68.5-70.5/ 10.1-12.1	33.5-36.0/ 53.5-55.5/ 8.1-10.1	6.0-8.0/ 77.0-79.0/ 13.0-15.0	2.5-4.5/ 81.0-83.0/ 12.5-14.5	20.0-21.5/ 67.0-71.0/ 9.0-11.0	11.0-13.0/ 51.0-53.0/ 13.0-15.0/ 21.0-23.0	27.0-29.0/ 24.0-26.0/ 19.0-21.0/ 26.0-28.0			
Bubble Point ¹	°C @ 101.3 kPa	N/A	-30.4	-42.7	-46.4	-37.3	-34.5	-44.0	-44.6	-45.2			
Dew Point ¹	°C @ 101.3 kPa	N/A	-25.6	-35.5	-40.4	-32.1	-30.9	-36.1	-37.2	-37.1			
Critical Temperature	°C	N/A	102.4	92.6	85.3	94.1	95.3	89.8	81.6	85.7			
				Vaj	por Phase Cor	ntaminants							
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5			

	Reporting Units	Reference Section	R-456A	R-457A	R-457B	R-457C	R-457D	R-459B	R-460A	R-460B
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

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Reporting Reference R-464A R-460C R-467A R-461A R-462A R-463A R-465A **R-466A** Section Units **Characteristics** R-125/ R-32/ **R-744**/ R-32/ R-32/ R-32/125/ 143a/ 125/ R-32/ R-32/ Refrigerant 32/125/ 125/ 125/ 290/ N/A N/A 134a/ 134a/ 143a/ 125/ Components 134a/ 1234yf/ 1234ze(E)/ 1234ze(E) 227ea/ 134a/ 1234yf 13I1 134a 227ea 600a 600a 600 55.0/ 9.0/ 6.0/ 2.5/ 27.0/ 22.0/ 5.0/ 42.0/ 21.0/ 49.0/ 36.0/ Nominal 2.5/ 27.0/ 5.0/ % bv 7.9/ N/A 32.0/ 2.0/ 30.0/ 11.5/ Composition weight 46.0/ 40.0/ 72.4/ 5.0/ 44.0/ 71.1 39.5 14.0/ 49.0 6.0 0.6 14.0 3.0 3.0 54.0-56.0/ 8.0-10.5/ 5.0-8.0/ 2.0-3.0/ 26.0-28.0/ 21.5-22.1/ 40.0-44.0/ 34.0-38.0/ 19.5-21.5/ 47.0-49.5/ 4.5-5.5/ 4.5-5.5/ Allowable % by 2.0-3.0/ 26.0-28.0/ 7.0-8.0/ 11.0-13.5/ N/A 31.0-33.0/ 1.0-3.0/ 28.0-32.0/ weight 45.0-47.0/ 39.0-41.0/ 70.9-72.9/ Composition 4.5-5.5/ 42.0-46.0/ 12.0-16.0/ 70.1-72.1 39.0-41.5 48.0-50.0 5.5-6.5 0.5-0.7 2.6-3.1 2.0-4.0 12.0-16.0 °C @ Bubble N/A -29.2 -42 -58.4 -42.6 -46.5 -51.8 -51.7 -40.5 $Point^1$ 101.3 kPa °C @ Dew Point¹ N/A -26.0 -37 -36.6 -46.9 -36.9 -40.0 -51 -33.3 101.3 kPa Critical °C N/A 99.5 81.4 83.5 75.8 82.6 89.4 76.5 92 *Temperature*

Vapor Phase Contaminants

				, aj		tummunt,				
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

	Reporting Units	Reference Section	R-460C	R-461A	R-462A	R-463A	R-464A	R-465A	R-466A	R-467A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean							
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	N/A	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

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	Ta	ble 19 Zeotr	opic Blends	s (400 Serie		ts) Character through R-4		owable Levels	of Contamina	nts
	Reporting Units	Reference Section	R-468A	R-468B	R-468C	R-469A	R-470A	R-470B	R-471A	R-472A
					Characteri	stics				
Refrigerant Components	N/A	N/A	R-1132a/ 32/ 1234yf	R-1132a/ 32/ 1234yf	R-1132a/ 32/ 1234yf	R-744/ 32/ 125	R-744/ 32/ 125/ 134a/ 1234ze(E)/ 227ea	R-744/ 32/ 125/ 134a/ 1234ze(E)/ 227ea	R-1234ze(E)/ 227ea/ 1336mzz(E)	R-744/ 32/ 134a
Nominal Composition	% by weight	N/A	3.5/ 21.5/ 75.0	6.0/ 13.0/ 81.0	6.0/ 42.0/ 52.0	35.0/ 32.5/ 32.5	10.0/ 17.0/ 19.0/ 7.0/ 44.0/ 3.0	10.0/ 11.5/ 11.5/ 3.0/ 57.0/ 7.0	78.7/ 4.3/ 17.0	69.0/ 12.0/ 19.0
Allowable Composition	% by weight	N/A	2.0-3.7/ 19.5-23.5/ 73.0-77.0	5.0-6.5/ 12.0-13.5/ 80.0-83.0	5.0-6.5/ 41.0-42.5/ 50.0-54.0	32.0-37.0/ 30.5-34.5/ 30.5-34.5	9.0-11.0/ 16.0-18.0/ 18.0-20.0/ 6.5-7.5/ 42.0-46.0/ 2.5-3.5	9.0-11.0/ 10.5-12.5/ 10.5-12.5/ 2.5-3.5/ 55.0-59.0/ 6.5-7.5	77.2-79.1/ 3.9-5.8/ 16.6-18.5	68.0-70.0/ 11.0-13.0/ 18.0-20.0
Bubble Point ¹	°C @ 101.3 kPa	N/A	-51.3	-52.4	-56.6	-78.5	-62.7	-61.7	-16.9	-84.3
Dew Point ¹	°C @ 101.3 kPa	N/A	-39.0	-36.8	-46.2	-61.5	-35.6	-31.4	-13.8	-61.5
Critical Temperature	°C	N/A	83.9	85.0	76.8	57	94.3	94.3	111.8	50.2
				Vaj	por Phase Cor	ntaminants	·			
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

	Reporting Units	Reference Section	R-468A	R-468B	R-468C	R-469A	R-470A	R-470B	R-471A	R-472A
				Liq	uid Phase Co	ntaminants				
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean						
Acidity, Maximum	ppm by weight (as HCl)	4.7	1	1	1	N/A	N/A	N/A	1	N/A
Chloride ²	Pass or Fail	4.6	No visible turbidity							

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

	14		opie Biolia			through R-4			
	Reporting Units	Reference Section	R-472B	R-473A	R-475A	R-476A	R-477A	R-477B	R-478A
				Cha	aracteristics				
Refrigerant Components	N/A	N/A	R-744/ 32/ 134a	R-1132a/ 23/ 744/ 125	R-1234yf/ 134a/ 1234ze(E)	R-134a/ 1234ze(E)/ 1336mzz(E)	R-1270/ 600a	R-1270/ 600a	R-744/ 32/ 125/ 134a/ 152a/ 1234ze(E)/ 227ea
Nominal Composition	% by weight	N/A	58.0/ 10.0/ 32.0	20.0/ 10.0/ 60.0/ 10.0	45.0/ 43.0/ 12.0	10.0/ 78.0/ 12.0	84.0/ 16.0	38.0/ 62.0	7.0/ 26.0/ 15.0/ 15.0/ 3.0/ 30.0/ 4.0
Allowable Composition	% by weight	N/A	57.0-59.0/ 9.0-11.0/ 31.0-33.0	19.0-20.5/ 9.0-11.0/ 58.0-62.0/ 9.0-11.0	44.0-46.0/ 42.0-44.0/ 11.0-13.0	9.5-12.0/ 76.0-78.5/ 11.5-14.0	82.0-86.0/ 14.0-18.0	36.0-39.0/ 61.0-64.0	6.5-7.5/ 25.0-27.0/ 14.0-16.0/ 14.0-16.0/ 2.8-3.2/ 29.0-31.0/ 3.5-4.5
Bubble Point ¹	°C @ 101.3 kPa	N/A	-82.9	-87.6	-28.8	-19.1	-44.6	-31.5	-58.4
Dew Point ¹	°C @ 101.3 kPa	N/A	-54.8	-83	-28.3	-16.1	-37.2	-23.1	-37.4
Critical Temperature	°C	N/A	57.9	29.7	99.3	110.2	100.5	121.7	88

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Table 20 Zeotropic Blends (400 Series Refrigerants) Characteristics and Allowable Levels of Contaminants

Reporting Units	Reference Section	R-472B	R-473A	R-475A	R-476A	R-477A	R-477B	R-478A
			Vapor Ph	ase Contamin	ants			
% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5
			Liquid Ph	ase Contamin	ants			
ppm by weight	4.4	10	10	10	10	10	10	10
% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5
% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean
ppm by weight (as HCl)	4.7	N/A	1	1	1	1	1	N/A
Pass or Fail	4.6	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity
	Units% by volume @ 25.0°Cppm by weight% by weight% by weight% by volume or % by weightPass or Failppm by weight (as HCl)Pass or	UnitsSection% by volume @ 25.0°C4.10ppm by weight4.10% by weight4.4% by weight4.11% by volume or % by weight4.8Pass or Fail4.9ppm by weight (as HCl)4.7Pass or Pass or (as HCl)4.6	UnitsSectionR-472B% by volume @ 25.0°C4.101.5ppm by weight4.410% by weight4.410% by weight4.110.5% by weight4.80.01% by weight4.9Visually cleanPass or Fail4.9N/Appm by 	UnitsSectionK-4/2BK-4/3AWitsSectionVapor Pha% by volume @ 25.0°C4.101.51.5Ppm by weight4.401010% by weight4.41010% by weight4.110.50.5% by weight4.80.010.01% by weight4.9Visually cleanVisually cleanPass or Fail4.9No visibleNo visible	UnitsSectionR-472BR-473AR-473A $Vapor Phase Contamin\% byvolume @25.0°C4.101.51.51.5mathef{P$	UnitsSectionK-4/2BK-4/3AK-4/3AK-4/6A $Vapor Phase Contaminants\% byvolume @25.0°C4.101.51.51.51.5Liquid Phase Contaminantsppm byweight4.410101010\% byweight4.410101010\% byvolume or\% byweight4.80.010.050.50.5\% byvolume or\% byweight4.80.010.010.010.01Pass orFail4.9VisuallycleanVisuallycleanVisuallycleanVisuallycleanVisuallycleanppm byweight4.7N/A111Pass or(as HCl)4.6No visibleNo visibleNo visibleNo visible$	UnitsSectionK-4/2BK-4/3AK-4/3AK-4/0AK-4/0A $Vapor Phase Contaminants\% byvolume @25.0°C4.101.51.51.51.51.5Liquid Phase Contaminantsppm byweight4.41010101010\% byweight4.110.50.50.50.50.50.5\% byweight4.80.010.010.010.010.010.01\% byweight4.80.010.010.010.010.010.01Pass orweight4.7N/A1111Pass or(as HCl)4.6No visibleNo visibleNo visibleNo visibleNo visible$	Units Section R-4/2B R-4/3A R-4/3A R-4/3A R-4/7A R-4/7B Volume (0) 4.10 1.5

1. *Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes.* Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

		-			Sitteringeranta		ics and Allowa		oomannian		
	Reporting Units	Reference Section	R-432A	R-433A	R-433B	R-433C	R-436A	R-436B	R-436C	R-441A	R-443A
					Charact	eristics					
Refrigerant Components	N/A	N/A	R-1279/ E170	R-1270/ 290	R-1270/ 290	R-1270/ 290	R-290/ 600a	R-290/ 600a	R-290/ 600a	R-170/ 290/ 600a/ 600	R-1270/ 290/ 600a
Nominal Composition	% by weight	N/A	80.0/ 20.0	30.0/ 70.0	5.0/ 95.0	25.0/ 75.0	56.0/ 44.0	52.0/ 48.0	95.0/ 5.0	3.1/ 54.8/ 6.0/ 36.1	55.0/ 40.0/ 5.0
Allowable Composition	% by weight	N/A	79.0-81.0/ 19.0-21.0	29.0-31.0/ 69.0-71.0	4.0-6.0/ 94.0-96.0	24.0-26.0/ 74.0-76.0	55.0-57.0/ 43.0-45.0	51.0-53.0/ 47.0-49.0	93.8-96.5/ 3.8-6.2	2.8-2.4/ 52.8-56.8/ 5.4-6.6/ 34.1-38.1	53.0-57.0/ 38.0-42.0/ 3.8-6.2
Bubble Point ¹	°C @ 101.3 kPa	N/A	-45.2	-44.4	-42.5	-44.1	-34.3	-33.3	-41.5	-41.5	-45.2
Dew Point <mark>1</mark>	°C @ 101.3 kPa	N/A	-42.4	-44	-42.4	-43.7	-26.1	-25	-39.5	-20.3	-42.1
Critical Temperature ¹	°C	N/A	97.3	94.4	96.3	94.8	115.9	117.4	96.8	117.3	95.1
					Vapor Phase (Contaminants					
Air and Other Non- condensables, Maximum	% by volume @ 25.0°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

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	Reporting Units	Reference Section	R-432A	R-433A	R-433B	R-433C	R-436A	R-436B	R-436C	R-441A	R-443A
					Liquid Phase C	Contaminants ⁴					
Sulfur Odor ²	No odor to pass	4.13	Pass	Pass	Pass	Pass	Pass	Pass	Pass	Pass	Pass
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/ Solids	Pass or Fail	4.9	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean	Visually clean
Acidity, Maximum	ppm by weight	4.7	1	1	1	1	1	1	1	1	N/A
Water, Maximum	ppm by weight	4.4	20	10	10	10	10	10	10	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
Total C ₃ , C ₄ and C ₅ Polyolefins, Maximum	% by weight	4.12	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.05
Chloride ³	Pass or Fail	4.6	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	No visible turbidity	N/A	N/A

Notes:

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Including hydrogen sulfide and mercaptans.

3. Taken from vapor phase.

4. Vaporized from liquid phase.

N/A = Not applicable

Table 22 Azeotropic Blends (500 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-500 through R-512A)

	Reporting Units	Reference Section	R-500	R-502	R-503	R-507A	R-508A	R-508B	R-509A	R-510A	R-511A	R-512A
					Cha	racteristics						
Refrigerant Components	N/A	N/A	R-12/ 152a	R-22/ 115	R-23/ 13	R-125/ 143a	R-23/ 116	R-23/ 116	R-22/ 218	R-E170/ 600a	R-290/ E170	R-134a/ 152a
Nominal Composition	% by Weight	N/A	73.8/ 26.2	48.8/ 51.2	40.1/ 59.9	50.0/ 50.0	39.0/ 61.0	46.0/ 54.0	44.0/ 56.0	88.0/ 12.0	95.0/ 5.0	5.0/ 95.0
Allowable Composition	% by weight	N/A	72.8-74.8/ 25.2-27.2	44.8-52.8/ 47.2-55.2	39.0-41.0/ 59.0-61.0	49.5-51.5/ 48.5-50.5	37.0-41.0/ 59.0-63.0	44.0-48.0/ 52.0-56.0	42.0-46.0/ 56.0-60.0	87.5-88.5/ 11.5-12.5	94.0-96.0/ 4.0-6.0	4.0-6.0/ 94.0-96.0
Bubble Point ¹	°C @ 101.3 kPa	N/A	-33.6	-45.2	-87.8	-46.7	-87.4	-87	-49.8	-24.9	-42	-24
Dew Point ¹	°C @ 101.3 kPa	N/A	-33.6	-45	-87.8	-46.7	-87.4	-87	-48.1	-24.9	-42	-24
Critical Temperature ¹	°C	N/A	102.1	80.2	18.4	70.6	10.8	11.8	68.6	125.7	97	112.9
					Vapor Pha	se Contamina	ants					
Air and Other Non- condensables, Maximum	% by volume @ 25°C	4.10	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5

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	Reporting Units	Reference Section	R-500	R-502	R-503	R-507A	R-508A	R-508B	R-509A	R-510A	R-511A	R-512A
					Liquid Pha	ase Contamin	ants					
Water, Maximum	ppm by weight	4.4	10	10	10	10	10	10	10	20	20	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
<i>HBR</i> , Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01
Particulates/Solids	Pass/Fail	4.9	Visually clean									
Acidity, Maximum	ppm by weight	4.7	1	1	1	1	1	1	1	1	1	1
Chloride ²	Pass/Fail	4.6	No visible turbidity									

Notes:

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

Table 23 Azeotropic Blends (500 Series Refrigerants) Characteristics and Allowable Levels of Contaminants (R-513A through R-516A)

	Reporting Units	Reference Section	R-513A	R-513B	R-514A	R-515A	R-516A
		· ·	Chara	cteristics			
Refrigerant Components	N/A	N/A	R-1234yf/ 134a	R-1234yf/ 134a	R-1336mzz(Z)/ 1130(E)	R-1234ze(E)/ 227ea	R-1234yf/134a/ 152a
Nominal Composition	% by weight	N/A	56.0/ 44.0	58.5/ 41.5	74.7/ 25.3	88.0/ 12.0	77.5/ 8.5/ 14.0
Allowable Composition	% by weight	N/A	55.0-57.0/ 43.0-45.0	58.0-59.0/ 41.0-42.0	74.2-76.2/ 23.8-25.8	86.0-89.0/ 11.0-14.0	76.1-78.9/ 7.0-9.0/ 12.1-14.1
Bubble Point ¹	°C @ 101.3 kPa	N/A	-29.2	-29.2	29.0	-18.9	-29.4
Dew Point ¹	°C @ 101.3 kPa	N/A	-29.1	-29.1	29.0	-18.9	-29.4
Critical Temperature ¹	°C	N/A	96.5	95.5	178.1	108.4	99.3
			Vapor Phase	Contaminants			
Air and Other Non- condensables, Maximum	% by volume @ 25°C	4.10	1.5	1.5	N/A	1.5	1.5

AHRI Standard 700-2024 (SI)

	Reporting Units	Reference Section	R-513A	R-513B	R-514A	R-515A	R-516A
			Liquid Phase	Contaminants			
Water, Maximum	ppm by weight	4.4	10	10	20	10	10
All Other Volatile Impurities, Maximum	% by weight	4.11	0.5	0.5	0.5	0.5	0.5
HBR, Maximum	% by volume or % by weight	4.8	0.01	0.01	0.01	0.01	0.01
Particulates/Solids	Pass or Fail	4.9	Visually clean				
Acidity, Maximum	ppm by weight	4.7	1	1	1	1	1
Chloride ²	Pass or Fail	4.6	No visible turbidity				

Notes:

1. Bubble points, dew points, and critical temperatures, although not required, are provided for informational purposes. Refrigerant data compiled from REFPROP 10.0.

2. Recognized chloride level for pass/fail is 3 ppm.

N/A = Not applicable

324			Section 8. Characterization of Refrigerants and Contaminants
325	8.1	Single (Component Fluorocarbon and Zeotropic/Azeotropic Blend Refrigerants
326 327			erization of single component fluorocarbon (<u>Table 1</u> through <u>Table 3</u>) and zeotropic/azeotropic blend (<u>Table 6</u> Table 20, <u>Table 22</u> , and <u>Table 23</u>) refrigerants and contaminants are listed in the following classifications:
328		8.1.1	Isomer Content
329			See <u>Table 1</u> through <u>Table 3</u> .
330		8.1.2	Air and Other Non-condensables
331			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through Table 20, <u>Table 22</u> , and <u>Table 23</u> .
332		8.1.3	Water
333			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
334		8.1.4	All Other Volatile Impurities
335			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
336		8.1.5	High Boiling Residue
337			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
338		8.1.6	Particulates/Solids
339			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
340		8.1.7	Acidity
341			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
342		8.1.8	Chloride
343			See <u>Table 1</u> through <u>Table 3</u> , <u>Table 6</u> through <u>Table 20</u> , <u>Table 22</u> , and <u>Table 23</u> .
344	8.2	Hydroc	carbon Refrigerants
345 346		Charact classific	erization of hydrocarbon refrigerants (Table 4 and Table 21) and contaminants are listed in the following eations:
347		8.2.1	Nominal Composition
348			See <u>Table 4</u> and <u>Table 21</u> .
349		8.2.2	Other Allowable Impurities
350			See <u>Table 4</u> .
351		8.2.3	Air and Other Non-condensables
352			See <u>Table 4</u> and <u>Table 21</u> .
353		8.2.4	Sulfur Odor
354			See <u>Table 4</u> and Table 21.
355		8.2.5	High Boiling Residue
356			See <u>Table 4</u> and <u>Table 21</u> .
357		8.2.6	Particulates/Solids
358			See <u>Table 4</u> and Table 21.
359		8.2.7	Acidity
360			See <u>Table 4</u> and <u>Table 21</u> .
361		8.2.8	Water
362			See Table 4 and Table 21.

363		8.2.9	All other volatile impurities
364			See <u>Table 4</u> and Table 21.
365		8.2.10	Total C3, C4 and C5 polyolefins
366			See <u>Table 4</u> and Table 21.
367		8.2.11	Chloride
368			See Table 21.
369	8.3	Carbo	n Dioxide Refrigerants
370 371		Charact classific	erization of carbon dioxide and carbon dioxide's contaminants are shown in <u>Table 5</u> in the following cations:
372		•	Purity
373		•	Air and other non-condensables
374		•	Water
375		•	High boiling residue
376		•	Particulates/Solids
377			Section 9. Recording Procedure
378 379 380	be iden	tified by i	er manufacturer, reclaimer, or repackager, of the packaged refrigerant shall be identified. The refrigerant shall its accepted refrigerant number or the chemical name, or both. Maximum allowable levels of contaminants are through <u>Table 23</u> . Test results shall be tabulated in the same manner.

APPENDIX A. REFERENCES – NORMATIVE

- This appendix lists all standards, handbooks, and other publications essential to the development and implementation of the standard. All references in this appendix are part of the standard.
- A.1. AHRI Standard 740-2016 (SI), Performance Rating of Refrigerant Recovery Equipment and Recovery/Recycling
 Equipment, 2016 Air-Conditioning, Heating, and Refrigeration Institute, 2111 Wilson Blvd., Suite 500, Arlington,
 VA 22201, USA
- A.2. ANSI/ASHRAE Standard 34-2022, Designation and Safety Classification of Refrigerants, 2022, with Addenda,
 ASHRAE, 180 Technology Parkway NW, Peachtree Corners, Georgia 30092, USA.
- A.3. ASHRAE *Handbook Fundamentals*, 2021, ASHRAE, 180 Technology Parkway NW, Peachtree Corners, Georgia 30092, USA.
- A.4. ASHRAE *Terminology*. ASHRAE. Accessed August 9, 2024. <u>https://www.ashrae.org/technical-resources/free-resources/ashrae-terminology</u>
- A.5. ASTM Standard D1296-01-2012, *Standard Test Method for Odor of Volatile Solvents and Diluents*, 2012, ASTM International, 100 Barr Harbor Drive, West Conshohocken, PA 19428, USA.
- A.6. ISO 817:2014, *Refrigerants Designation and Safety Classification*, 2014, International Organization for Standardization, Chemin de Blandonnet 8 CP 401 1214 Vernier, Geneva, Switzerland.
- A.7. GPA 2177-20, Analysis of Natural Gas Liquid Mixtures by Gas Chromatography, 2020, GPA Midstream Association,
 6060 S American Plaza St E #700, Tulsa, OK 74135, USA.
- A.8. REFPROP Reference Fluid Thermodynamic and Transport Properties NIST Standard Reference Database 23
 Version 10.0, 2018, U.S. Department of Commerce, Technology Administration, National Institute of Standards and
 Technology, Standard Reference Data Program, Gaithersburg, MD 20899, USA.

403

382

APPENDIX B. REFERENCES – INFORMATIVE

406 This appendix lists standards, handbooks and other publications that can provide useful information and background but are 407 not essential for the use of this standard. All references in this appendix are not part of the standard.

- **B.1.** U.S. *Code of Federal Regulations*, Title 40, Part 82, 2024, Office of the Federal Register, National Archives and Records Administration, 800 North Capitol Street, NW, Washington, DC 20402, USA.

413 APPENDIX C. ANALYTICAL PROCEDURES – NORMATIVE

414	C.1.	Determ	ination of Acidity in New and Reclaimed Refrigerants by Titration
415		C.1.1.	Purpose
416			This test method determines the amount of acidity in new and reclaimed refrigerants.
417		C.1.2.	Scope
418			This test method is for use with low, medium, and high pressure fluorocarbon refrigerants.
419		C.1.3.	Definitions
420			Definitions for this section are identical to those in <u>Section 3</u> and AHRI 740.
421		C.1.4.	Principle
422 423 424 425			A known quantity of a liquid refrigerant sample is added to, or bubbled through, an extraction solvent that is a mixture of toluene, isopropanol and water to which bromothymol blue indicator has been added. The acidity imparted to the extraction solvent by the sample quantity is titrated with potassium hydroxide (KOH) to the indicator endpoint. The acidity is recorded in ppm as HCl.
426		C.1.5.	Applicability
427 428			This method is applicable to the routine quantitative determination of acidity in low, medium, and high pressure refrigerants.
429		C.1.6.	Limitations and Interferences
430 431 432			None of the refrigerants tested interfere with the acidity determination. The test shall be performed after the indicator solution is brought to its blue/green end point to prevent interferences from atmospheric carbon dioxide.
433		C.1.7.	Sensitivity, Precision and Accuracy
434			C.1.7.1. Sensitivity
435 436			The sensitivity of the acidity test using 50 g of sample in 100 g of extraction solvent is 0.1 ppm. Samples shall be handled to prevent cross contamination when performing this test.
437			C.1.7.2. Precision
438			Data is not provided.
439			C.1.7.3. Accuracy
440			Data is not provided.
441		C.1.8.	Special Apparatus and Reagents
442			1) Capillary tubing 1/16-in x 0.05-in stainless steel
443			2) Top loading balance, 1000 g with 0.1 g resolution
444			3) 1/16-in x 1/4-in stainless steel tube compression fitting reducing union
445			4) 1/4-in compression x 1/4-in flare AN female adaptor
446			5) 250 mL Erlenmeyer flask
447			6) Bromothymol blue sodium salt endpoint indicator
448			7) Reagent grade isopropanol
449			8) Reagent grade toluene
450 451			9) 0.1 N Potassium hydroxide in methanol10) 0.1 N Sulfuric acid
451 452			10) 0.1 N Sulfuric acid 11) Absolute methanol (anhydrous, reagent grade)
4 <i>32</i> 453			12) Stir plate/stir bar
+JJ			

454		13) Gl	ass distille	d water
455		14) Bu	ret (10 mL	with 0.05 mL graduation)
456	C.1.9.	Procedure		
457		C.1.9.1.	Capillary	y Tubing Connector
458			Take a	1/16-in x 0.05-in stainless steel tubing and make a compression fitting (swage)
459				on using a 1/16-in nut and ferrule. Connect this to a 1/16-in x 1/4-in compression-
460				ducing union and then connect this combination to the 1/4-in compression fitting x
461				are adaptor. The 1/4-in flare adaptor can then be connected to the 1/4-in flare fitting on
462				ble cylinder just before each acidity determination.
463		C.1.9.2.	Reagent	Preparation
464			C.1.9.2 .1	1. 0.01 N Potassium Hydroxide Solution
465 466				Pipet 100 mL of 0.1 N potassium hydroxide solution into a 1000 mL volumetric flask. Dilute to the mark with absolute methanol and mix thoroughly.
467			C.1.9.2.2	2. 0.01 N Sulfuric Acid Solution
468				Pipet 100 mL of 0.1 N sulfuric acid solution into a 1000 mL volumetric flask.
469				Dilute to the mark with distilled water and mix thoroughly.
470			C.1.9.2.3	3. Extraction Solvent
471 472				Add 495 mL of toluene to 495 mL of isopropanol. Add 10 mL of water to the toluene/isopropanol solution and mix thoroughly.
			C.1.9.2.4	
473 474			C.1.9.2.	Dissolve 1 g of bromothymol blue sodium salt in 100 mL of methanol. Mix
475				thoroughly and store in a dropper bottle.
476		C.1.9.3.	Sample A	Analysis
477			1)	Attach the 1/4-in stainless flare fitting to the vapor valve of the sample cylinder.
478			2)	Add 100 mL of the prepared extraction solvent to a 250 mL Erlenmeyer flask. Add a
479				clean magnetic stirring bar. Add six drops of the indicator solution to the extraction
480				solvent and initiate moderate stirring.
481			3)	If the extraction solvent/indicator solution is yellow, add 0.01 N potassium hydroxide
482				through the buret until a just-noticeable difference between yellow and light green is
483				seen in the extraction solvent. Half drops from the buret can be used to achieve the
484				real end point.
485			4)	If the extraction solvent/indicator solution is green or blue, add 0.01 N sulfuric acid
486				through the buret dropwise until the solution is yellow and then proceed as in
487				Section C.1.9.3(<u>3</u>).
488			5)	Attach the cleaned 0.05 in ID stainless steel capillary connector to the sample cylinder
489				and weigh the sample cylinder to the nearest 0.1 g. Slowly introduce 50 g to 75 g of
490				liquid sample into the extraction solvent/indicator solution by gradually opening the
491				cylinder valve and metering the liquid sample to maintain a controlled flow into the
492				solvent. The cylinder can be held by the analyst or clamped to a ring stand throughout
493				the procedure.
494				Note: This procedure takes practice to obtain the target mass added on the first try.

495 496 497 498 499 500 501			6) Once the sample has been added, record the post a and subtract from the starting weight, and ensure th 75 g. Observe the color change. If the color of the s is non-detected. If the solution is yellow, record 0.01 mL (designate this value as V_1) and add 0.01 until the original green color endpoint is reached. R nearest 0.01 mL (designate this value as V_2).	at the addition is between 50 g and solution is green or blue, the result the buret volume to the nearest N potassium hydroxide dropwise
502 503 504 505 506 507 508 509			7) When testing samples with high concentrations of carbon dioxide (R-744) refrigerant or blends co following the addition of the 50 g to 75 g, the titratie nitrogen for five minutes to evaporate the entrench with potassium hydroxide. Failure to do so results of the acidity value. Following titration, wait an add the next sample. If the solvent turns blue or very da increasing the nitrogen purge to ten minutes.	ntaining carbon dioxide (R-744), on solvent shall be purged with dry ed carbon dioxide prior to titrating n over-titration and over reporting itional five minutes prior to testing
510 511			The final volume, designated as V_f , of 0.01 N potassi as shown in Equation <u>1</u> .	um hydroxide added is determined
			$V_f = V_2 - V_1$	1
512			8) The calculation of total acidity expressed in ppm as	HCl is shown in Equation 2.
			$ppm \ as \ HCl = \frac{V_f \cdot normality \ KOH \cdot 36500}{refrigerant \ weight \ sampled}$	2
513			Note: The value 36 500 is the equal weight of H	Cl (36.5 x 10 ³).
514	C.2.	Determ	mination of Water in New and Reclaimed Refrigerants by Coulometric	Karl Fischer (KF) Titration
515		C.2.1.	Purpose	
516 517			This test method determines moisture in new and reclaimed refrigerant method.	s by the coulometric KF titration
518		C.2.2.	Scope	
519			This test method is for use with low, medium, and high pressure refrigera	nts.
520		C.2.3.	Definitions	
521			Definitions for this section are identical to those in <u>Section 3</u> and AHRI 7	40.
522		C.2.4.	•	
523			KF titration is based upon the redox reaction of water, iodine, and sulfur of	lioxide as shown in Equation $\underline{3}$.
			$H_2O + I_2 + SO_2 \rightarrow 2HI + SO_3$	3
524 525 526 527 528			The solvent is a mixture of methanol and a weak organic base (imidazole a to neutralize the reaction products. In coulometric KF titration, iodine i proportion to the amount of water introduced, and the end point is detect appearance of excess free iodine. The added refrigerant eventually evaporar repeatedly until either the sulfur dioxide or the base solution is consumed	s generated at the anode in direct ed bi-amperametrically as the first ates; hence, the solvent can be used
529		C.2.5.	Applicability	
530 531			This method is applicable to the routine quantitative determination of small and high pressure refrigerants.	amounts of water in low, medium,

532	C.2.6.	Limitatio	Limitations and Interferences			
533 534 535 536		Fe (III), Co such as ba	None of the refrigerants tested interfere with the titration. Oxidizing agents such as MnO_4^- , $Cr_2O_7^{-2}$, H_2O_2 , Fe (III), Cu (II), and reducing agents such as S^{-2} , thiosulphates, and Sn (II) interferes. Certain compounds such as basic oxides and salts of weak acids (NaHCO ₃ , for example) can form water with the KF reagent. None of these interferences are present in new or reclaimed refrigerants.			
537	C.2.7.	Sensitivity	Sensitivity, Precision, and Accuracy			
538		C.2.7.1.	Sensitivity			
539 540			The sensitivity of the analyzer in this method using a 10 g sample is 1 ppm. Samples shall be handled to achieve this sensitivity.			
541		C.2.7.2.	2. Precision and Accuracy			
542 543			The mean of the analysis (\overline{X}) , standard deviation (σ), and 95% confidence limits (CL) established for the single operator precision of this method are shown in Table 24.			
544 545			The data in Table 24 were calculated from seventeen replicate analyses of one sample (10 g) performed by one analyst over a period of two days.			
546 547 548 549			The samples in Table 25 are test and R-22 to 4.8 ppm and 7.1 pp known amounts of water. Both analyzing. Results are shown in 7	om, respectively, and then conta samples are mixed for a perio	aminating the refrigerants with	
550		The total percent recovery for each sample was 99.3% for R-12 and 99.7% for R-22.				
551			Table 24 Single Operat	tor Method Precision		
			$\frac{\text{Mean}}{(\overline{X})}$	Standard Deviation	95% Confidence	

	$\frac{\text{Mean}}{(\overline{X})}$	Standard Deviation (σ)	95% Confidence Limit
Water (R-12), ppm by weight	10.6	0.11	0.26
Water (R-22), ppm by weight	28.1	0.29	0.77

552

Table 25 Testing for Percent Water Recovery

	Original Value	Amount Contaminated	Calculated Total	Recovered Total	Percent Recovery
Water (R-12), ppm by weight	6.8	6.9	13.7	13.6	99.3
Water (R-22), ppm by weight	19.2	19.0	38.2	38.1	99.7

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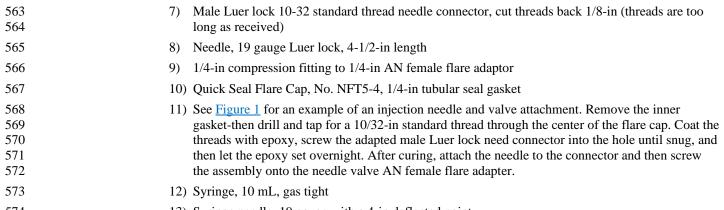
560 561

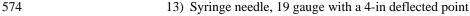
562

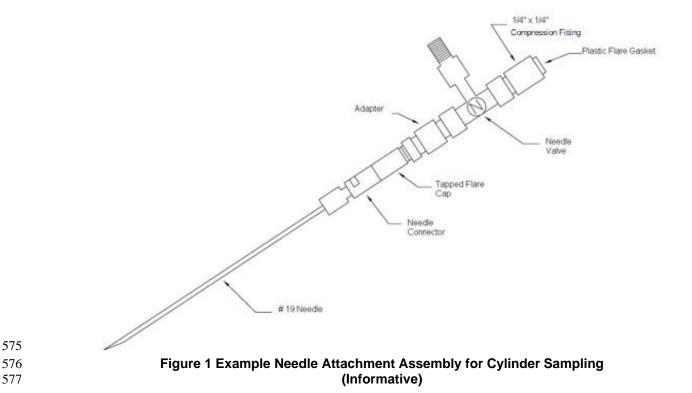
553

C.2.8. Special Apparatus and Reagents

- 1) Coulometric KF titrator system (contains a drying tube for venting refrigerant, anode and cathode solutions, septum, and water vaporizer)
- 2) Desiccant, 20-40 mesh
- 3) Desiccator, containing desiccant
- Refrigerant sample cylinder, such as 50 mL, 500 mL, or 1000 mL stainless steel double ended 1/4-in FNPT cylinder (1800 psig), steel cylinder, 2.2 lb, single 9-gauge valve, 3/8-in pipe neck, disposable can, 17 oz, or other cylinder
- 5) Stainless steel integral bonnet non-rotating stem valve, 1/4-in MNPT x 1/4-in FNPT
- 6) Brass screwed-bonnet needle valve, 1/4-in MNPT







C.2.9. Procedure

	C.2.9.1.

Verification

Verify that the instrument is operating accurately by injecting quantified moisture standard prior to sample testing.

C.2.9.2. Sample Analysis

Note: To minimize contamination from moisture, the sample should be introduced directly from the refrigerant sample cylinder into the coulometric titrator to prevent a secondary container transfer, whenever able. The effects of moisture contamination and phase distribution are minimized if the sample container is 60% to 80% liquid filled with refrigerant. If the sample is a very high pressure refrigerant, cool the cylinder to 14K less than the *critical temperature* of the refrigerant and wait thirty minutes for equilibrium to be established before starting the analysis.

590	1)	Refer to the instruction manual for moisture analyzer installation and operation.
591 592		Note: Instrument sensitivity should be set at 0.10 and a new septum should be attached.
593 594 595 596 597	2)	Turn-on the analyzer and magnetic stirrer and wait until the background current (μ g of H ₂ O per second) has reached a low, steady level. The titration vessel can be swirled to contact (wash down) any water mist on the upper inside walls with the anode solution. Optimum levels are less than 0.10 µg of H ₂ O per second, between 0.02 µg of H ₂ O to 0.05 µg of H ₂ O.
598 599 600 601 602 603 604 605		Note: If after fifteen minutes a low (< $0.1 \ \mu g$ of H ₂ O per second) background current is not obtained or if the cathode solution turns a dark reddish-brown color, turn off the moisture meter and, using a small funnel, renew both anode and cathode solutions. If a negative background reading persists (free iodine in the anode solution), introduce a drop of R-113 or methanol-water wetting solution into the vessel to eliminate the free iodine through reaction with water and produce a positive background. This wetting solution can be made by adding a small amount of water (less than 500 ppm) to methanol or R-113.
606 607 608	3)	Using a heat gun, dry-off the valve threaded end of the sample cylinder valve that contains a pressure relief valve (350 psi to 400 psi) and cylinder stem valve (1/4-in MNPT x 1/4-in FNPT).
609 610	4)	Remove the needle/needle valve attachment (see <u>Figure 1</u>) from the oven or desiccator and immediately attach to the sample cylinder valve.
611 612 613	5)	Open the refrigerant sample cylinder valve, then slowly open the needle valve and purge a small amount of sample liquid phase to flush the air from the needle (one second to two second purge). Close both valves.
614	6)	Using a heat gun (high position), dry the needle for twenty seconds to thirty seconds.
615 616	7)	Weigh the refrigerant sample cylinder plus attachment on a top loader balance (nearest 0.1 g) and record on a work sheet.
617 618 619	8)	Using a clamp (or clamps) and weighted ring stand, invert and position the sample cylinder such that the needle punctures the septum and is immersed to the hub of the needle.
620 621		Note: The needle should be submerged about one inch below the surface of the KF solution.
622 623		Note: The background current rises after the needle is inserted, then returns to the low valve.
624 625 626	9)	At this juncture, with the instrument turned on, preset for a five-minute titration start delay, and verify that the background current is at a low value such as $0.02 \ \mu g$ to $0.05 \ \mu g$.
627 628		 a) The titration shall not be initiated unless and until the background current has stabilized at a low µg value.
629 630 631 632 633 634 635 635		b) The coulometric titrator background signal, given as μg H ₂ O per second, is subtracted from the analyzed result and represents the background moisture accumulated during the time taken to introduce and to titrate the sample. The background value subtracted is the final value read just before sample addition begins. An artificially elevated background value results in an erroneously low result (meaning negatively biased). The background value shall be determined. The titration cell can be physically quirled to rinea moisture accumulated on the inper wells into the physically quirled to rinea.
636 637 638		physically swirled to rinse moisture accumulated on the inner walls into the KF solution. This operation can speed up the process of reaching a low background signal.
639	10)	The desiccant tube shall be clear of obstructions.

640 641	11) Enter the gross cylinder weight (W_1) from Section C.2.9.2(7) into the moisture meter, if applicable, or record the initial weight of the cylinder to the nearest 0.1 g.
642	12) If applicable, remove any prior number displayed for the second weight.
643 644 645 646	13) When the moisture meter is stable, initiate a run, slowly open the needle valve, and introduce sample at a moderate rate such that foaming is not observed on the KF solution surface. Add at a rate such that 15 g to 20 g of the sample is added over a ten-minute period. The sample addition count down (delay) can be used.
647 648 649 650	14) A 20-g sample is used for best accuracy. Observe the cell potential reading or microgram reading. If during the sample addition this reading climbs rapidly to a range of 200 ppm by weight to 300 ppm by weight, the sample contains high moisture, and a smaller sample size of 5 g to 10 g can be used.
651 652	15) The titration initiates after the proper sample size has been added or after the countdown (delay) period ends.
653 654 655	If the sample contains high moisture, the rate of titration can never exceed the rate of H_2O addition and the titration shall be terminated (closing off the needle valve) before too much of the sample is added.
656 657 658	Note: Conversely, if the sample added is 4 g to 5 g and the moisture level is 5 ppm to 10 ppm, the sample should be reanalyzed using a longer sample addition delay, for example, ten minutes, to achieve better accuracy.
659	16) Remove the sample cylinder/assembly and reweigh to the nearest 0.1 g (W_2).
660 661	Note: If a 4 g to 5 g sample size is used, a more accurate balance should be utilized, and weights should be recorded to the nearest 0.01 g.
662 663	17) Enter the weight from Section C.2.9.2(<u>16</u>) into the moisture meter if applicable, or record the final weight of the cylinder to the nearest 0.1 g.
664 665	18) Calculate and print a report of the ppm or microgram water result. See Figure 2 for an example of the printed results.
666	No.: 1-14 F=1 CONC: 4.02 ppm FNo1: (M-B) / (W-w) M: 83.6 µg B.G.: 0.08 µg/S TIME: 5 SENS: 0.10 VA-T: 100 VA-P: PRNT: 3 CALC: 1 IDNo: 1-14 W: 503.5 W: 482.7 W-w. 20.800000 g B: 0
	TIME: 1:43

Figure 2 Example of Moisture Analyzer Report (Informative)

669		C.2.9.3.	Calculation
670			Equation $\underline{4}$ shows moisture concentration.
			microarams of $H_{\rm c}$ 0
			$MoistureConcentration, ppm = \frac{micrograms of H_2 0}{grams of sample(W_1 - W_2)}$ 4
671			Record all results to the nearest 1 ppm. If the results are less than 2 ppm, record as "< 2 ppm."
672 673			Note: Erratic and out-of-specification moisture results can be the result of poor or improper sampling, or both.
674			Moisture contamination occurs faster when the relative humidity is high.
675 C. 676			igh Boiling Residue in New and Reclaimed Refrigerants by Volumetric or Gravimetric etermination of Particulate Residue by Visual Indication
677	C.3.1.	Purpose	
678		This test met	hod determines HBR and visible particulates in new and reclaimed refrigerants.
679	C.3.2.	Scope	
680		This test met	hod is for use with low, medium, and high pressure refrigerants.
681	C.3.3.	Definitions	
682		Definitions f	or this section are identical to those in <u>Section 3</u> and AHRI 740.
683	C.3.4.	Principle	
684 685 686 687 688 689		temperature. volume is of volume of re purity solven	mined by evaporating a known amount of refrigerant in a Goetz bulb at an ambient or elevated The remaining residue is then visually measured or weighed. If greater than specification oserved, the bulb is placed in a $60.0^{\circ}C \pm 2^{\circ}C$ oven for thirty minutes and, after cooling, the esidue is again measured. For gravimetric determination, the residue is redissolved in a high- th such as R-514A and quantitatively transferred into a small, tared aluminum pan. The solvent by evaporation and the pan reweighed to obtain the weight of residue.
690 691 692		insoluble ma	poration, the measured volume of liquid refrigerant is visually examined for the presence of aterials such as packing fibers, rust, and dirt. The residue from high pressure samples is n a clean solvent, swirled, and then visually examined for any insoluble particulates.
693	C.3.5.	Applicabilit	y
694 695 696 697		particulates in to measure <i>H</i>	I is applicable to the routine quantitative determination of <i>HBR</i> and visible evidence of n all low, medium, and high pressure new and reclaimed refrigerants. The method was developed <i>HBR</i> and particulates in compliance with the specifications for <i>HBR</i> and particulates shown in 1gh Table 23.
698	C.3.6.	Limitations	and Interferences
699 700			ne statistical parameters stated for this method, at least 100 mL of refrigerant sample is required. t any known interferences to this method.
701	C.3.7.	Sensitivity, I	Precision, and Accuracy
702		C.3.7.1.	Sensitivity
703 704 705 706 707 708			Based upon a 100 mL volume of sample, the method detects 0.01 mL of <i>HBR</i> , and that is the first mark on the Goetz bulb buret. This 0.01% value is the specification for refrigerants in <u>Table 1</u> through <u>Table 23</u> . The DL by weight is less than 0.01% due to the sensitivity of the analytical balance and because 0.01 mL of residue (can be oil) weighs less than 0.01 g. Except for very high pressure refrigerants, the weight of 100 mL of liquid refrigerant weighs greater than 100 g.

709		C.3.7.2.	Precision		
710 711					<i>HBR</i> determination at 0.03 volume percent was found to be \pm 0.005 at the ed upon an analysis of R-11 by two analysts, each of whom used silicone
712			oil as the res		. I
713		C.3.7.3.	Accuracy		
714			The relative	mean err	or at the 0.03% volume level was found to be 3.3%.
715			Note: The	ese statist	ical parameters are not applicable to visual observations of particulates.
716	C.3.8.	Special Ap	oparatus and H	Reagents	
717		1) Ge	oetz graduated	centrifug	tube: 100 mL
718		2) Bo	oiling chips, ca	rborundu	m crystal
719		3) Di	isposable alum	inum disl	h
720	C.3.9.	Procedure	9		
721		C.3.9.1.	Calibration		
722					re, a calibration solution of 0.03% by weight of silicone oil in R-11 can
723 724					ing 0.220 g of silicone oil and dissolving in 500 mL (738 g) of high purity
724 725					shly, labeling, and storing in a screw-capped glass bottle in a refrigerator. 0.187 g of oil and dissolve in 500 mL of R-514A or other solvent.
726		C.3.9.2.	Sample Ana	lysis for	HBR Volume Percent Measurement and Particulates
727			1) Me	asure 100) mL of refrigerant sample into the Goetz bulb as follows:
728			i.		w pressure refrigerants (R-11, R-113, R-123) add 100 mL of liquid
729 730				-	rant from a glass graduate into the Goetz bulb. Alternatively, add liquid ne sample container to the 100 mL mark of the Goetz bulb.
731			ii.		holding the bulb at arm's length, gently swirl the sample solution and then
732 733					n the bulb in front of a light source such as a window and visually examine presence of particulate matter. Record as "Pass" if particulates are not
734					ed. Proceed to Section C.3.9.2($\underline{2}$).
735			iii.		lium and high pressure refrigerants: Tare the sample cylinder to the nearest
736 737					vert the cylinder and, by positioning the valve opening just inside the neck foetz bulb, open the valve to let the liquid phase discharge into the bulb.
738					id refrigerant, other than very high pressure refrigerants [see
739				Section	C.3.9.2(1)(iv)], begins to accumulate in the Goetz bulb. Continue to add
740					until 60 mL to 75 mL of liquid has been collected. Turn off the sample
741 742				sample	Reweigh the sample cylinder and record the difference as the weight of added.
743				While f	irmly holding the bulb at arm's length, gently swirl the sample solution
744					n position the bulb in front of a light source such as a window and visually
745 746					e for the presence of particulate matter. Record the description of ates if observed. Proceed to Section $C.3.9.2(2)$.
747				Note:	Use isopropyl alcohol, a finger, or a paper towel to remove frost from
748 749					the outside of the bulb to create a window to facilitate the visual observation.

750 751 752 753 754 755 756 757		iv	r. For very high pressure refrigerants (R-503, R-13, R-23), the sample cylinder is precooled to 4.4°C in ice water before flashing the liquid phase into the Goetz bulb. Continue to add the liquid phase until the sample cylinder weigh-back shows that between 100 g and 130 g of refrigerant has been flashed into the bulb. At this point, little or no liquid phase refrigerant accumulates in the bulb. Record this weight as the grams of sample added. Add 100 mL of a high-purity solvent such as R-514A to the bulb, put the stopper in the bulb, swirl to dissolve any residue on the inner walls of the bulb, and remove the stopper.
758 759			Stopcock grease shall not be present on the glass stopper or on the neck of the bulb.
760		v	Repeat Section C.3.9.2(1)(\underline{ii}).
761 762 763 764 765		2)	Add one small boileezer and place the Goetz bulb in a 45.0° C constant temperature water bath, for example, 60.0° C for R-113. Immerse the bulb in the bath to about the 20 mL to 25 mL mark. The bulb shall not be removed from the bath until all the refrigerant has completely evaporated. This is determined by observing the disappearance of refrigerant condensation around the neck of the bulb.
766 767 768		3)	Remove the Goetz bulb from the bath, wipe the outside dry and visually measure the mL residue (if any) at the bottom of the buret (ignore the boileezer). Measure to the nearest 0.005 mL.
769 770		4)	If the observed residue is less than or equal to 0.01 mL, proceed to Section C.3.9.3. If the observed residue is greater than 0.01 mL, proceed to Section C.3.9.2($\underline{5}$).
771 772 773 774		5)	Place the Goetz bulb upright in a 60.0°C oven for thirty minutes, remove, cool, then measure and record the volume of residue to the nearest 0.005 mL in the buret as described in Section C.3.9.2(3). To measure weight percent, save the residue in the Goetz bulb for Section $C.3.9.4$.
775	C.3.9.3.	Calculat	ion
776		Use Equ	nation 5 to calculate <i>HBR</i> by volume.
		HBR V	$blume \% = \frac{A \cdot 100}{B}$ 5
777		Wh	ere:
778		Α	= volume of residue (mL) in buret
779		В	
7 00			= mL of sample added to bulb [Section C.3.9.2(1)]
780 781 782		Note:	= mL of sample added to bulb [Section C.3.9.2(1)] To calculate the volume of high and very high pressure refrigerant samples, in mL, divide the weight of the sample by the liquid density of the refrigerant at the ambient sample temperature (see Table 26).
781		Record	To calculate the volume of high and very high pressure refrigerant samples, in mL, divide the weight of the sample by the liquid density of the refrigerant at the ambient
781 782 783	C.3.9.4.	Record "< 0.019	To calculate the volume of high and very high pressure refrigerant samples, in mL, divide the weight of the sample by the liquid density of the refrigerant at the ambient sample temperature (see Table 26). all results to the nearest 0.01% volume. If the results are less than 0.01%, record as
781 782 783 784	C.3.9.4.	Record "< 0.019 Sample A	To calculate the volume of high and very high pressure refrigerant samples, in mL, divide the weight of the sample by the liquid density of the refrigerant at the ambient sample temperature (see Table 26). all results to the nearest 0.01% volume. If the results are less than 0.01%, record as % volume."
781 782 783 784 785 786 787	C.3.9.4.	Record "< 0.019 Sample 1)	To calculate the volume of high and very high pressure refrigerant samples, in mL, divide the weight of the sample by the liquid density of the refrigerant at the ambient sample temperature (see Table 26). all results to the nearest 0.01% volume. If the results are less than 0.01%, record as % volume." Analysis for Weight Percent Measurement Rinse an aluminum pan in acetone and place the pan in a 60.0°C oven for at least thirty minutes. Remove using tweezers and place in a desiccator until cool, fifteen minutes

794 795 796 797	4	Pour the solution from the Goetz bulb into the pan. Use 10 ml to 20 ml of solvent and repeat Section C.3.9.4(3) if necessary to complete the quantitative transfer of residue. The boiling chip shall not fall into the aluminum pan; however, if that does occur, remove the boiling chip using metal tweezers.
798 799	5	Place the aluminum pan inside a hood and let the high-purity solvent evaporate. Alternatively, the pan can be placed on the hot water bath.
800 801	6	Place the pan in the 60.0°C oven for thirty minutes, remove, and then place in the desiccator until cool, twenty minutes to thirty minutes.
802 803	7	Using tweezers, remove and reweigh the pan and record the difference in weight from Section $C.3.9.4(2)$ as the weight of residue.
804 C	.3.9.5. Calcul	ation
805	Equat	on <u>6</u> shows <i>HBR</i> by mass.
	HBR	weight $\% = \frac{A \cdot 100}{B}$ 6
806	W	/here:
807	Α	= grams of residue from Section C.3.9.4($\frac{7}{1}$)
808	В	= grams of sample taken from Section C.3.9.2($\underline{1}$)
809 810	Note:	To determine the amount of a low pressure sample refrigerant such as R-11, R-113, or R-123, multiply the volume taken times the density. See Table 26.
811 812		d the results to the nearest 0.01% weight. If the results are less than 0.01% weight, record 0.01% weight."

Refrigerant	Density (g/mL)
R-11	1.476
R-12	1.311
R-22	1.194
R-32	0.961
R-123	1.468
R-124	1.364
R-125	1.19
R-134a	1.21
R-142b	1.114
R-152a	0.899
R-290	0.492
R-404A	1.167
R-407A	1.142
R-407C	1.134
R-410A	1.031
R-438A	1.147
R-448A	1.097
R-449A	1.097
R-454B	0.985
R-500	1.168
R-502	1.217
R-507	1.17
R-513A	1.134
R-514A	1.311
R-515B	1.180
R-600	0.573
R-600a	0.551
R-744	0.711
R-1270	0.506
R-1233zd(E)	1.163
R-1234yf	1.092
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Table 26 Densities of Common Liquid Refrigerants at 25°C

- 814 C.4. Determination of Chloride in New and Reclaimed Refrigerants by Silver Chloride Precipitation
 815 C.4.1. Purpose
 816 This test method qualitatively determines the presence of chloride in new and reclaimed refrigerants.
- 817 C.4.2. Scope

 818 This test method is for use with low, medium, and high pressure refrigerants.

 819 C.4.3. Definitions

 820 Definitions for this section are identical to those in Section 3 and AHRI 740.

821 **C.4.4. Principle**

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Equation <u>7</u> shows the qualitative determination of chloride in refrigerants is based on precipitation of the chloride anion as silver chloride.

$$Ag^+ + Cl^- \rightarrow AgCl$$
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Add the same volume of methanol as the volume of refrigerant found in Section C.4.9.3(7) to a 100 mL beaker. For each 5 mL of methanol used, add three drops of saturated silver nitrate (AgNO₃) solution to the methanol. Also, add one drop of concentrated nitric acid to the solution before adding the refrigerant sample. Visual turbidity indicates the presence of chloride and the test failed. If turbidity is not observed, chloride is within limits as the test passed.

C.4.5. Applicability

This method is applicable to the routine qualitative determination of chloride in low, medium, and high pressure refrigerants.

C.4.6. Limitations and Interferences

None of the refrigerants tested interfere with the chloride determination. Anions of weak acids can be an interference in the determination, but these interferences are not present in new or reclaimed refrigerants. Samples containing insoluble lubricants and oils can show a visual haze or turbidity, however, such levels of lubricant or oil necessary to show such visual turbidity are not present in new or reclaimed refrigerants.

C.4.7. Sensitivity, Precision and Accuracy

C.4.7.1. Sensitivity

The sensitivity of the chloride turbidity test using 5 mL of sample in 5 mL of methanol containing three drops of saturated AgNO₃ is 3 ppm. Sample handling shall prevent cross contamination when performing this test.

C.4.7.2. Precision

Data is not provided.

C.4.7.3. Accuracy

Data is not provided.

846 C.4.8.	Special Apparatus and Reagents
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- 1) Stainless steel capillary tubing
- 2) Top loading balance, 1000 g with 0.1 g resolution
- 3) Methanol anhydrous reagent
- 4) $AgNO_3$
 - 5) 75 mL stainless steel double ended 1/4-in FNPT cylinder
 - 6) Two 1/4-in stainless steel valves with MNPT fittings
 - 7) Two 1/4-in FNPT x 1/4-in flare fittings
- 8) 1/16-in x 1/4-in stainless steel tube compression fitting reducing union
- 9) 1/4-in compression fitting x 1/4-in flare AN female adaptor
- 856 10) 1/4-in x 1/4-in copper flare connector
 - 11) 1/4-in inlet MNPT x 1/4-in outlet FNPT pressure relief valve

858	C.4.9.	Procedure			
859		C.4.9.1.	Stainless Steel Capillary Tubing Connector		
860 861 862 863 864			Take a 1/16-in x 0.007-in stainless steel tubing and attach a 1/16-in nut and ferrule. Connect this to a 1/16-in x 1/4-in compression fitting reducing union and then connect this combination to the 1/4-in compression fitting x 1/4-in flare adaptor. The 1/4-in flare adaptor can then be connected to the 1/4-in flare fitting on the cylinder assembly just before each chloride determination.	l ;	
865		C.4.9.2.	Cylinder Assembly		
866 867 868			The cylinder assembly is used as the sampling apparatus for chloride determination of medium and high pressure refrigerants. To complete this assembly, all pipe fittings shall be tetrafluoroethylene taped to confirm a proper seal at each joint.		
869 870 871 872 873			Attach the pressure relief valve to the 75 mL stainless steel cylinder. Attach one of the 1/4-in MNPT x 1/4-in MNPT stainless steel valves to the pressure relief valve. Connect a 1/4-in FNPT x 1/4-in fitting to the 1/4-in MNPT valve. To the other side of the 75 mL cylinder, attach another 1/4 in MNPT x 1/4 in MNPT valve. Sampling shall always occur from the side of the 75 mL cylinder that does not employ the pressure relief valve.	l	
874		C.4.9.3.	Sample Analysis		
875 876 877			 Thoroughly clean the 75 mL stainless steel cylinder, the valve, the capillary tube, the copper connector, and the 100 mL beaker before initiating testing. Heat all of the components to 110°C and pull a vacuum. 		
878			2) Weigh the cylinder assembly to the nearest 0.1 g and designate this weight as "X."		
879 880			 Attach the 1/4-in copper fitting to the gas value of the sample cylinder and to the cylinder assembly. Loosen the connector and quickly tighten the fitting. 	1	
881 882 883			4) Invert the sample cylinder with the attached cylinder assembly. Open the sample cylinder valve and then the cylinder assembly valve. Introduce the refrigerant into the cylinder assembly until 30 g to 40 g of refrigerant has been sampled.		
884 885 886			Note: For very high pressure refrigerants such as R-13, R-23, or R-503, the sample cylinder and the cylinder assembly shall be precooled to 4.0°C to provide liquid phase sample for this test.		
887 888			5) Close the cylinder assembly valve and set the sample cylinder upright. Close the sample cylinder valve, loosen the 1/4-in connector, and remove the cylinder assembly.		
889 890 891			6) Reweigh the cylinder assembly with the refrigerant and designate this value as "Y." The weight of the refrigerant is given by $Y-X = \text{grams of refrigerant sampled}$. The value for "X" is in Section C.4.9.3(2).		
892			7) Calculate the volume of refrigerant sampled with Equation $\underline{8}$.		
			$volume = \frac{grams \ sampled}{density} $ 8		
893 894 895 896 897 898			 The values of the densities for each refrigerant can be found in Table 26. 8) For medium and high pressure refrigerants, proceed to Section C.4.9.3(9). For low pressure refrigerants, pour 25 mL of the refrigerant into a 100 mL beaker and proceed as in Section C.4.9.3(8). After adding the methanol and saturated AgNO₃ solution, stir the mixture for thirty seconds. If any turbidity is present in the methanol layer, the test failed. 		

899 900 901 902				9) Add the same volume of methanol as the volume of refrigerant found in Section C.4.9.3(7) to a 100 mL beaker. For each 5 mL of methanol used, add three drops of saturated AgNO ₃ solution to the methanol. Add one drop of concentrated nitric acid to the solution before adding the refrigerant sample.
903 904 905 906				This chloride test is valid only if the sample solution being tested is acidic. This prevents the formation of silver oxide if the sample pH is greater than 7.10) Attach the cleaned capillary connector to the cylinder assembly containing the refrigerant sample and slowly introduce the entire sample into the methanolic AgNO₃.
907				11) If turbidity is present, the test failed. If turbidity does not exist, the test passed.
908	C.5.	Determ	nination of N	ICG in New and Reclaimed Refrigerants by Gas Chromatography
909		C.5.1.	Purpose	
910			This test m	ethod determines NCG levels in new and reclaimed refrigerants using gas chromatography.
911		C.5.2.	Scope	
912			This test m	ethod is for use with medium, high, and very high pressure refrigerants.
913		C.5.3.	Definition	3
914			Definitions	for this section are identical to those in <u>Section 3</u> and AHRI 740.
915		C.5.4.	Principle	
916 917 918 919 920 921 922			using a TC carbon diox in amounts R-503) do refrigerant	asured in the vapor space above the refrigerant liquid phase by isothermal gas chromatography 2D and an external standard calibration. <i>NCG</i> includes gases such as oxygen and nitrogen (air), kide, argon, and carbon monoxide. However, in the refrigerant sample, air is the only <i>NCG</i> present and the other gases are not routinely analyzed. Very high pressure refrigerants (R-13, R-23, not always contain liquid phase and these are analyzed directly. <i>NCG</i> equilibrium between the liquid phase and the vapor phase is temperature dependent and sample temperature corrections to record results at the 24.0°C specification temperature.
923		C.5.5.	Applicabil	
924 925				d is applicable to the routine quantitative analysis of <i>NCG</i> in medium, high, and very high pressure
926		C.5.6.	Limitation	s and Interferences
927 928 929 930			Methane el begins to i	e refrigerants interfere with the determination as all chromatographically elute after the air peak. utes about 0.10 minutes after the air peak and, if present in amounts greater than 0.10% by volume, nterfere. However, the amounts of methane (formed during compressor burn-out) in reclaimed s range from 0 ppm to 50 ppm by weight and does not interfere at these levels.
931		C.5.7.	Sensitivity	, Precision and Accuracy
932			C.5.7.1.	Sensitivity
933 934				The method detects 0.02% by volume <i>NCG</i> in any of the refrigerants listed as applicable in <u>Table 1</u> through <u>Table 23</u> .
935			C.5.7.2.	Precision
936 937 938				The precision was determined at 5.2% by volume concentration and was found to be \pm 0.07% by volume at the 95% CL. This is based upon twelve repetitive analyses of an R-12 sample by two technicians over a two-day period.
939			C.5.7.3.	Accuracy
940 941 942				A 5.1% by volume certified calibration standard (air in helium) was analyzed nine times following the initial calibration during a one-day period by one technician. The relative mean error was 1.63%.

943	C.5.8.	Special Apparatus and Reagents
944		1) Gas chromatograph: Equipped with a manual sample injection valve, 1 mL sample loop and a TCD
945 946		2) Gas chromatographic column: 1.8 m x 3.17 mm (6.0 ft x 0.125 in) OD stainless steel, divinylbenzene/ethylvinylbenzene crosslinked polymers, 80-100 mesh
947 948		 Chromatography data system: Capable of electronic integration and processing the chromatographic data
949		4) Calibration standard: 1.5% by volume, air in helium, 30 lb cylinder
950		5) Digital thermometer
951		6) Temperature probe
952	C.5.9.	Procedure
953		C.5.9.1. Chromatographic Operating Conditions
954		Set the GC and data integration system as shown in Table 27.

Table 27 Chromatographic Operating Conditions for the Determination of NCG in New and Reclaimed Refrigerants

Parameter	Setting		
Detector sensitivity	low sensitivity		
Carrier gas flow	30 mL helium per minute		
Attenuator	x1 ¹		
Detector temperature, °C	100		
Injector port temperature, °C	100		
Head pressure	as required ²		
Column temperature, °C	100		
Sampling valve	load position		
Integrator	External Standard method % volume		
Notes: 1. Unattenuated 2. Twenty psi can be used.			

C.5.9.2. Calibration

1)	Refer to the op	perating manua	l to gain fan	niliarity with th	he gas chroma	tograph (GC).
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- 2) Attach a 51 cm (20 in) section of 1/4-in inside diameter flex line to the GC sample inlet line and terminate the other end with a 1/4-in female flare connector.
- 3) Attach a short piece of flex line to the GC sample exit line and terminate the tubing by placing the flex line inside a small beaker of water.
- 4) Connect the sample inlet line to the valve of the 1.5% *NCG* calibration standard cylinder.
- 5) Slowly open the standard cylinder valve, and slowly purge the sample vapor through the sample loop as indicated by bubbles in the exit line beaker of water. Purge for about ten seconds to expel air from the system.
 - Note: One ten-second purge should be equal to 10 mL of vapor.

969 970 971	6) Close the cylinder valve and, when the bubbling stops, immediately rotate the sampling valve to the "Inject" position and immediately start the GC/integration system.
972 973	 After the air peak has eluted 0.4 minutes, return the sampling valve to the "Load" position and terminate the integration.
974 975	8) Repeat Section C.5.9.2(5) through Section C.5.9.2(7) until three consecutive analyses yield essentially reproducible peak areas for the air peak.
976 977	 Calculate the air peak absolute response factor (ARF) for each of the three analyses as shown in Equation <u>9</u>.
	$ARF = \frac{A_i}{\% \ by \ volume \ air \ in \ calibration \ standard} \qquad 9$
978	Where:
979	A_i = area of air peak
980	10) Average the three ARF values and assign the average value as the ARF for the method.
981 982 983	Note: The three ARF values should agree within about 1.6% relative mean error. The calibration standard should be analyzed at least daily, and the ARF updated as necessary.
984	C.5.9.3. Sample Analysis
985	Analyze the sample using the chromatographic conditions described in Section $C.5.9.1$.
986	Note: See example gas chromatograms in <u>Appendix D</u> .
987 988 989	 Record the temperature to the nearest 0.5°C of the sample source liquid phase when the vapor phase is taken for analysis. If this information is unknown (customer samples, for example), record as 24.0°C.
990 991 992 993 994	i. To reestablish equilibrium in a liquid/vapor phase sample cylinder brought into the laboratory and that has changed temperature to a degree from the original temperature (standing several hours, for example), the cylinder shall be rolled to mix the contents for two minutes before sampling the vapor phase for gas chromatography (GC) analysis.
995 996 997	Note: The outer wall temperature of the cylinder below the liquid level should be equal to that of the refrigerant contents and can be measured using a thermocouple probe.
998 999 1000 1001 1002	 ii. If the vapor phase of a storage tank, road tanker, or ton cylinder, is sampled into a small, evacuated cylinder, regardless of what temperature the small sample cylinder vapor can be when analyzed by gas chromatography, the contents represent the vapor temperature at the original sample location point.
1003 1004	 Connect the sample inlet line to the sample cylinder valve that directly accesses the sample vapor phase.
1005 1006	3) Slowly open the sample cylinder valve and slowly purge vapor (about ten seconds) to expel air from the sample loop and lines.
1007 1008 1009 1010 1011 1012	i. When analyzing cylinders containing both a liquid phase and a vapor phase, a too rapid purge shall not be used when purging air from the chromatographic system. A too rapid purge can cause liquid refrigerant to expel and such droplets can evaporate resulting in a too rich in refrigerant vapor purge. The presence of refrigerant liquid can result in incorrect <i>NCG</i> values that are lower than the true value in the sample.

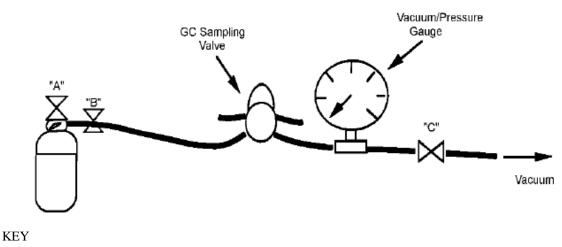
1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029	4) 5) 6)	 immediately rotate the sampling valve to the "Inject" position and immediately start the GC/integration system. Continue the chromatographic separation until the large refrigerant peak returns to the original baseline (refer to the ASHRAE <i>Handbook — Fundamentals</i>). Stop the integration. Repeat Section C.5.9.3(3) through Section C.5.9.3(5) until the air peak area is reproducible (such as until all system air has been expelled). Two or three additional consecutive determinations can be used.
1030	C.5.9.4. Calculat	tion
1031 1032	1)	The data system calculates the result for air (<i>NCG</i>) in % by volume that represents the temperature that the sample is taken for analysis as shown in Equation 10 .
		% by volume NCG = $\frac{A_i}{ARF}$ 10
1033 1034 1035	2)	Correct the result to % <i>NCG</i> at 24.0°C as in Equation <u>11</u> . Use the vapor pressure- temperature graphs in the ASHRAE <i>Handbook</i> — <i>Fundamentals</i> or calculate through REFPROP. For R-403B, use the curve for R-125.
1036 1037 1038 1039		Note: In all liquid/vapor phase refrigerants, the <i>NCG</i> concentration in the vapor phase increases with decreasing temperature of the liquid phase. This is because the vapor concentration of the refrigerant decreases more so than that of air as the temperature drops.
		$C_1 = \frac{C_2 \cdot P_2 \cdot K_i}{T_2} $ 11
1040		For K values, see <u>Table 28</u> .
1041		Where:
1042		$C_1 = NCG$, % by volume, at 24.0°C
1043		$C_2 = NCG$, % by volume, at the sampling temperature
1044		K_i = Temperature/pressure ratio for refrigerant <i>i</i> at 24.0°C, see <u>Table 28</u>
1045 1046 1047		P_2 = Vapor pressure (psia) of the refrigerant at the sampling temperature, T ₂ , in °C (°F). This value is determined from the ASHRAE <i>Handbook</i> — <i>Fundamentals</i> or calculated through REFPROP.
1048		T_2 = Sampling temperature in K (°R) such as $T_2 = °C + 273.15$
1049 1050	3)	Record results to the nearest 0.01% by volume. If results are less than 0.02% by volume, record as "< 0.02% by volume."

Refrigerant	K _i (K/MPa)	K _i (°R/psia)	
R-12	478.705	5.941	
R-114	1445.54	17.94	
R-124	797.71	9.9	
R-125	224.406	2.785	
R-22	297.086	3.687	
R-134a	439.625	5.456	
R-115	340.597	4.227	
R-142b	906.969	11.256	
R-500	402.88	5.0	
R-502	269.13	3.34	
R-152a	552.352	6.855	
R-32	180.66	2.242	
R-1234yf	447.76	5.557	
R-1234ze(E)	614.43	7.625	
Note:	ata for this table		

Table 28 K_i Values for Selected Refrigerants at 24.0°C

1. Source data for this table is the ASHRAE *Handbook* — *Fundamentals*.

2. Other refrigerant K-values can be calculated using data produced by REFPROP or other reference materials.



1054	"A"	Sample cylinder valve

1055 "B" Metering valve

- 1056 "C" Vacuum pump valve
- 1057 1058

1052 1053

Figure 3 Evacuated System Method of Introducing Vapor Sample into Gas Chromatograph

1059	C.6.	Determ	nination of	of Purity of New and Reclaimed R-11 by Gas Chromatography
1060		C.6.1.	Purpos	e
1061 1062				st method determines the purity of new and reclaimed trichlorofluoromethane (R-11) by gas tography.
1063		C.6.2.	Scope	
1064			This tes	t method is for use with R-11.
1065		C.6.3.	Definiti	ons
1066			Definiti	ons for this section are identical to those in Section 3 and AHRI 740.
1067		C.6.4.	Princip	le
1068 1069 1070			chromat	ganic purity of new and reclaimed R-11 is determined by programmed temperature gas tography using a packed column with a flame ionization detector (FID). Component peak areas are ed electronically and quantified by the area normalization response factor method.
1071		C.6.5.	Applica	bility
1072 1073				ethod is applicable to the determination of the impurities that can be present in commercially ctured R-11 and in R-11 recovered and reclaimed from operating refrigeration systems.
1074		C.6.6.	Limitat	ions and Interferences
1075 1076				ethod is calibrated for only those impurities commonly present in R-11. Other impurities that have tected on occasion are listed (with retention times) in Table 30.
1077			This me	thod does not detect any impurities that can elute within the comparatively large R-11 peak matrix.
1078		C.6.7.	Sensitiv	vity, Precision and Accuracy
1079 1080				al parameters for each impurity are listed in Table 31. The data is obtained by analyzing an R-11 ion mixture seven times during one day by one operator.
1081		C.6.8.	Special	Apparatus and Reagents
1082			1)	Gas chromatograph: Equipped with an FID and capable of oven temperature programming.
1083 1084			2)	Chromatography data system: Capable of electronic integration and processing chromatographic data.
1085 1086 1087 1088			3)	Gas chromatographic column (Packed): 1% high molecular weight compound of polyethylene glycol and a diepoxide reacted with nitroterephthalic acid on (60-80) mesh graphitized carbon with a nominal surface area of 100 square meters per gram in a 7.3 m (24 ft), 3.2 mm (1/8 in) OD stainless steel column. Prepacked columns are commercially available from multiple vendors.
1089			4)	Serum bottle: 125 mL
1090				Note: Bottle holds 160 mL when liquid full.
1091			5)	Crimp seal with 20 mm Septa.
1092			6)	Glass collecting tube: 125 mL
1093 1094				Enlarge side outlet opening to accommodate a crimp-on 2 cm septum. Apply fiberglass tape outside for protection.
1095			7)	Syringe, 10 µL, liquid.
1096				Externally cool the syringe and sample to 10°C before sampling.
1097 1098			8)	R-11 and impurities for calibration standard preparation: CCl_4 , $CHCl_3$, CH_2Cl_2 , and trichloroethylene (TCE) and all other fluorochemicals are commercially available.
1099 1100				The purity of each calibration component shall be predetermined by gas chromatography FID or TCD, or both and, if necessary, by gas chromatography/mass spectrometry (GC-MS).

C.6.9. Procedure

C.6.9.1. Chromatographic Operating Conditions

Table 29 shows chromatographic operating conditions.

Table 29 Chromatographic Operating Conditions for the Determination of Purity of New and Reclaimed R-11

Parameters	Settings
Detector	FID
Carrier gas	30 mL helium per minute
Initial column temperature, °C	125
Initial hold	Four minutes
Program, °C per minute	10
Final column temperature, °C (°F)	180
Post hold	Fourteen minutes
Detector temperature, °C	250 ¹
Injector port temperature, °C	2001
Sample	1 μL (liquid syringe)
Maximum safe column temperature, °C	225 (for conditioning purposes)
Notes: 1. Condition can be optimized for spec	ific gas chromatograph used.

C.6.9.2. Calibration Standard for Preparation and Analysis

- 1) Obtain a stock of the highest purity R-11 as evidenced by the chromatograms using the procedure in Section $\underline{C.6}$.
- 2) Determine the tare weight to the nearest 0.01 g of a 125 mL serum bottle with septum and cap loosely attached, then fill with stock R-11 to within 5/8 inch of the top. Crimp on the septum.
- 3) Reweigh and subtract the tare weight in Section C.6.9.2(2) to obtain the grams of R-11 added.
 - Note: The purest R-11 does contain impurities listed in Table 30. The amounts of impurities already in the stock R-11 are determined through the method of standards addition. Individual impurity peak areas in the stock are increased in the calibration standard by the amount of the corresponding impurity added. The amount already present is combined with the amount added to give the total component present, in ppm, in the calibration standard.
- 4) Individually and in turn add the volumes of each calibration component indicated in Table 31 through the septum and below the R-11 liquid surface in the bottle. Use a gas tight syringe with a deflected point needle for gases and a liquid μ L syringe for liquids. Shake the bottle to mix after addition of each component.

1124 1125 1126 1127 1128 1129	Note:	To preserve the stock of calibration gases, a small 125 mL gas collecting to that has been evacuated to 1 atm should be loaded from the liquid phase illustrated in Figure 4. The volume is then withdrawn and injected into serum bottle containing the R-11. For impurities that are liquids at amb temperature, inject the indicated μ L volumes of each respective comportion into the serum bottle.	e as the oient
1130 1131		the mass added column and combine this weight with that of Section C.6.9.2 In the total weight to the nearest 0.01 g of calibration sample in the bottle.	2(<u>3</u>)
1132 1133		te the amount added to the nearest 1 ppm for each component by dividing lded by the total weight of sample in the serum bottle [Section C.6.9.2(5)].	
1134 1135 1136 1137	the stor in Sect	te the amount present for each component by combining the amount present k R-11, if any, and the amount of the component added in ppm [see the r ion $C.6.9.2(3)$]. The component present values, in ppm, are those used ning the method response factors.	note
1138 1139		the serum bottle standard in an ice bath and, after the serum is ice cold, rem and immediately replace the septum with a new septum.	ove
1140 1141 1142 1143	with th sample	the amount of the present values for each component on the label in ppm, all e date of preparation, the gross weight, and the total grams of calibrar Store in a refrigerator. Discard and prepare a new standard when the sam falls below 60% of the original weight [see the note in Section C.6.9.2(4)]	tion nple
1144 C.6.9.3. Deter	mination o	f Component Response Factors	
		a the data system used, the ppm values can be converted to weight % calculations and for recording purposes.	for
1147 1148	 Set up calibrat 	the chromatography data system for an area normalization-response fa- ion.	ctor
1149 1150		e the calibration standard bulb in triplicate using the chromatograp ons described in Table 29.	phic
1151 1152 1153 1154	integrat respons	R-11 as the reference peak, perform the necessary functions to have or or the chromatography data system determine each component rela e factor (<i>RRF_i</i>) that is then stored. Response factors are calculated as show in <u>12</u> and Equation <u>13</u> .	tive
	ARF_i =	$= \frac{weight \% in calibration standard}{A_i}$	12
	ARF _{R-}	$_{11} = \frac{100.0000 - S}{A_{R-11}}$	13
1155	W	nere:	
1156	AR	F = Absolute response factor of component i	
1157	A_i	= peak area of component i (average of three determinations)	
1158	S	= weight % sum of all impurities present to four decimal places	
1159 1160		R-11 as the reference peak, the relative response factor (RRF) can be ned. See Equation 14 .	

$$RRF_i = \frac{ARF_i}{ARF_{R-11}}$$
 14

 RRF_i values are computed to the nearest 0.0001 unit.

1162C.6.9.4.Sample Analysis

Analyze the sample using the chromatographic conditions described in Section C.6.9.1. The sample and syringe are precooled (refrigerator, ice bath) to 10°C before sampling to simplify loading into the μ L syringe. To identify an unknown peak, use component spiking, GC-MS (if provided), or both.

Note: See example gas chromatograms in <u>Appendix D</u>.

1168 **C.6.9.5.** Calculations

The weight percentage of each component is calculated as shown in Equation 15.

$$W_i = \frac{RRF_i \cdot A_i \cdot 100}{\sum(A_i \cdot RRF_i)}$$
15

Where:

1171	A_i	=	peak area of component i
1172	RRF_i	=	Relative response factor (RFF) for component i
1173	W_i	=	weight percent of component i
1174	$\sum (A_i \cdot RRF_i)$	=	sum of all component peak areas times their respective relative
1175			response factors
1176	Record sample cor	npor	nent concentrations to the nearest 0.0001% (or to the nearest 1 ppm).

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Table 30 Retention Time Data for Identified Impurities Not Observed

Table 30 shows retention time data for identified impurities not observed.

	Impurity	Retention Time, min	
	R-32 ¹	2.37	
R-114		4.1	
R-290		8.0	
Note:			
1.	1	rate, attach a 0.30-m section of a porous polymer T column umn and reanalyze the chromatograph (R-23 elutes first).	

1180 1181 Table 31 shows component statistical parameters for the determination of purity of R-11.

Component	Detection Limit, ppm	Range Investigated, ppm	Precision at 95% CL, ppm	Relative Mean Error, %
R-23	2	15	0.37	-2.8
R-13	3	20	0.53	-3.1
R-152a	1	30	0.47	1.7
R-22	2	50	0.98	-0.8
R-115	2	30	0.8	0.7
R-12	2	60	1.1	1.1
R-133a	1	25	0.33	-2.5
R-21	2	30	0.67	1.2
R-30	2	25	0.33	-2.5
R-114	2	40	1.91	-2.7
R-123a	3	25	2.7	-4.8
R-123	2	50	1.33	3.3
R-20	2	25	0.73	0.7
R-113	2	60	2.31	2.2
R-10	2	25	1.7	-3.3
R-1120	2	25	1.77	1.8

Table 31 Component Statistical Parameters for the Determination of Purity of New and Reclaimed R-11

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Table 32 shows primary calibration standard components.

Component	Molecular Weight	Volume Added	Mass Added ¹ , µg	Added Concentration ² , ppm	Total Concentration Present ³ , ppm
R-23 ⁴	70	1.2 mL	3436	15	
R-13 ⁴	105	1.0 mL	4274	19	
R-152a ⁴	66	2.5 mL	6748	30	
R-22 ⁴	86	3.2 mL	11 321	50	
R-115 ⁴	136	1.2 mL	6650	29	
R-12 ⁴	121	2.8 mL	13 845	61	
R-133a ⁴	118	1.1 mL	5332	24	
R-21 ⁴	103	1.6 mL	6740	30	
R-30	85	5.0 µL	6680	29	
R-114 ⁴	170	1.3 mL	9061	40	
R-123a	153	5.0 µL	7490	33	
R-123	153	10.0 µL	14 750	64	
R-20	120	5.0 µL	7445	33	
R-113	188	10.0 µL	15 650	68	
R-10	154	10.0 µL	15 950	70	
R-1120	132	5.0 μL	7278	32	

Table 32 Primary Calibration Standard Components for the Determination of Purity of New and Reclaimed R-11

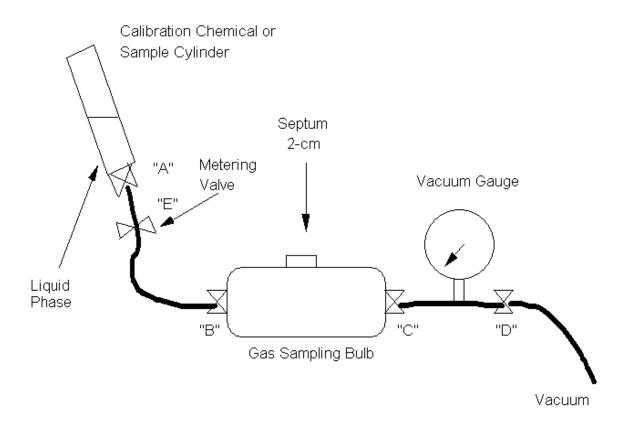
Notes:

1. The mass added for the purity of the calibration component previously established can be corrected.

2. Values shown are for illustration; exact values are determined in Section C.6.9.2(6).

3. Fill in column [see Section C.6.9.2(7)] after determining amount present, in ppm, in stock R-11. See the note in Section C.6.9.2(3). Intentionally left blank to enter data.

4. These impurities are gases at ambient room temperature. The others are liquids with low *boiling points*.



1185			
1186			Figure 4 Apparatus Used for Calibration Standard Preparation
1187 1188	C.7.		ination of Purity of New and Reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R-152a, R-218, R-290, R-600, and R-600a by Packed Column Gas Chromatography
1189		C.7.1.	Purpose
1190 1191			This test method determines the purity of new and reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R-143a, R-152a, R-218, R-290, R-600, and R-600a by gas chromatography.
1192		C.7.2.	Scope
1193 1194			This test method is for use with new and reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R-143a, R-152a, R-218, R-290, R-600, and R-600a.
1195			Note: R-290, R-600, and R-600a are components of fluorocarbon blends.
1196		C.7.3.	Definitions
1197			Definitions for this section are identical to those in <u>Section 3</u> and AHRI 740.
1198		C.7.4.	Principle
1199 1200 1201 1202			The purity of refrigerants is determined by gas chromatography using a packed column with a liquid phase coated onto a solid support. Separated components are detected using an FID or a TCD. The peak areas from the detector are measured with a data system capable of electronic integration, and component concentrations are quantified by the area normalization response factor method.
1203		C.7.5.	Applicability
1204 1205			This method is applicable to the routine gas chromatographic determination of new and reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R-143a, R-152a, R-218, R-290, R-600, and R-600a.

1206	C.7.6.	Limitations and Interferences
1207 1208		This method is calibrated only for impurities found in new and reclaimed refrigerant. Any impurity that elutes within the matrix of the major component interferes if present in concentration.
1209	C.7.7.	Sensitivity, Precision, and Accuracy
1210 1211 1212 1213		The DL, 95% CLs (95% CL), and accuracy (relative mean error, RME) were established for single operator. Statistical parameters for each impurity are listed in <u>Table 34</u> . The data is calculated from seven replicate analyses from one sample of an R-12 calibration standard performed by one technician over a period of one day.
1214	C.7.8.	Special Apparatus and Reagents
1215 1216		1) Gas chromatograph: Equipped with a packed column injector with either an FID or TCD, or both, and capable of oven temperature programming.
1217 1218 1219 1220		2) Chromatography data system: Capable of electronic integration and processing the chromatographic data. The data system shall be configured to capture peak areas enabling measurement of peaks greater than or equal to 0.001% by weight. If the peak is identified, then the peak shall be quantified using its measured response factor.
1221 1222		Note: Peaks that are not identified by the data system should be given a default response factor that is the greater of the average response factors for the calibrated components or R-22.
1223 1224 1225 1226		3) Gas chromatographic column (packed): 1% high molecular weight compounds of polyethylene glycol and a diepoxide reacted with nitroterephthalic acid on 60-80 mesh graphitized carbon with a nominal surface area of 100 m ² /g in a 7.3 m, 3.20 mm OD stainless steel column. Prepacked columns are commercially available.
1227 1228		 Glass collecting tubes: 125 mL and 500 mL. (Enlarge side outlet opening to accommodate a crimp- on 2-cm septum. Apply fiberglass tape to the outside for protection.)
1229		5) Syringe, 1 mL, gas tight
1230		6) Deflected point needle: Standard hub 22 gauge x 1-1/2-in stainless steel
1231		7) Impurities for calibration standard preparation: These impurities are commercially available.

1232 C.7.9. Procedure 1233 C.7.9.1.

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- 1255
- 1236 1237

. Chromatographic Operating Conditions

<u>Table 33</u> shows chromatographic operating conditions for R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R-143a, R-152a, R-218, R-290, R-600, and R-600a.

Table 33 GC Operating Conditions for R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R 143a, R-152a, R-218, R-290, R-600, and R-600a

Condition	R-12, R-22, R-114, R-115, R-116, R-124, R-125, R-143a, R-152a, R-218, R-290, R-600, and R-600a	R-13	R-23			
Detector	FID	TCD	TCD			
Detector temperature, °C ¹	200	200	200			
Injection port temperature, °C1	200	200	200			
Carrier gas, mL helium per minute	20	20	20			
Sample size, mL (gas syringe) ¹	0.5	0.5	0.5			
Initial column temperature, °C	50	40	35			
Initial hold, min	6	6	4			
Program, °C/min	10	10	10			
Final column temperature, °C	175	160	125			
Post hold, min	15	6	4			
Maximum column temperature, °C	225 (conditioning purposes only)					
Note:						

1. Condition can be optimized for specific GC used.

1238 C.7.9.2.	Example	e - Primary Calibration Standard, Preparation and Analysis for R-12	
1239	Note:	Modify procedure for other refrigerants as necessary.	
1240 1241 1242 1243	1)	Determine the internal volume of a 500 mL gas bulb by weighing the bulb empty, then fill the bulb to maximum capacity with water. Record the grams of water as mL volume capacity on the outside of the bulb (to the nearest 1.0 mL). Thoroughly dry the nside of the gas bulb then crimp-on the septum.	
1244	2)	Assemble the apparatus as illustrated in Figure 5.	
1245	3)	Attach a cylinder of high purity stock refrigerant to the gas sampling bulb.	
1246 1247 1248 1249 1250 1251 1252		Note: The purest stock refrigerant contains the impurities found in the method. The ppm amounts of impurities already in the stock refrigerant are determined through the method of standards addition. Individual impurity peak areas in the stock refrigerant are increased in the calibration standard by the ppm amount of the corresponding impurity added. The ppm already present is combined with the ppm added to give the total ppm component present in the calibration standard.	
1253 1254	4)	With valve "A" closed, open all other valves, and evacuate to less than 100 microns of Hg pressure (0.013 kPa).	
1255	5)	Close valve "D" and monitor the gauge to confirm the system is not leaking.	

1256 6 1257 1258 6) Close metering valve "E," open valve "A," and then slowly open valve "E" and flash liquid phase stock refrigerant to bring the system to one atmosphere pressure. Close valve "A."
1259 7	Repeat Section C.7.9.2($\underline{4}$) through Section C.7.9.2($\underline{6}$).
1260 8) Close valves "B" and "C" and remove the bulb from the vacuum/sampling apparatus.
1261 9) Calculate the grams of the stock refrigerant added to the bulb as shown in Equation 16 .
	grams added = $\frac{MW_{ref} \cdot internal \ volumen \ of \ bulb(ml)}{24\ 450}$ 16
1262	Where:
1263	MW_{ref} = molecular weight of the stock refrigerant in g/mole
1264	24 450 = volume (mL) occupied by 1 mole of refrigerant at 25°C and 1 atm
1265 1 1266 1267	0) Individually, and in turn, add the volumes of each calibration impurity component of interest indicated in Table 35 to the calibration bulb. Use a μ L or mL gas tight syringe with a deflected point needle.
1268 1269 1270 1271	Note: To preserve the stock of calibration component, a small 125 mL gas collecting tube that has been evacuated to 1 atm should be loaded from the liquid phase as illustrated in Figure 5. The volume is then withdrawn and injected into the 500 mL calibration bulb.
1272 1 1273 1	1) Preparing a vapor phase standard by weighing the components into the gas bulb can be used as an alternate for Section C.7.9.2($\underline{10}$).
1274 1 1275 1276 1277	2) Into a 30 mL (37 mL filled) serum bottle, capped and crimped with a septum, add the exact volumes of the liquid impurities from Table 35 in the order given. Add by syringe injection through the septum using a 22-gauge or smaller needle as a vent. After addition, shake bottle vigorously to mix. Label, date, and store in a refrigerator.
1278 1279	Note: For calibration components that have <i>boiling points</i> above ambient temperature, cool the material and syringe to 10°C before transferring.
1280 1 1281 1	3) Refer to Figure 5. Evacuate a 125 mL bulb (internal volume premeasured) and fill to 1 atm with refrigerant stock.
1282 1 1283 1	 Accurately withdraw and inject exactly 5.0 µL of solution from the 30 mL serum bottle into the 125 mL bulb. Equilibrate for thirty minutes.
1284 1 1285 1286 1287	5) Using a 5 mL gas tight syringe, withdraw vapor from the 125 mL bulb and inject exactly 5.0 mL into the 500 mL calibration bulb. The mass of each component thus added is calculated as follows and is added to column four of Table 35. See Equation 17 .
	$m = \frac{V_W \cdot 25\ 000}{V \cdot A} $ 17
1288	Where:
1289	25 000 = dilution ratio
1290	A = internal mL of 125 mL bulb
1291	$m = \text{mass added}, \mu g$

1292 1293	V = total mL of solution from Section C.7.9.2(12) $V_w = \text{volume added, mL, from Table 35}$	
1294	C.7.9.3. Determination of Component Response Factors	
1295 1296	Note: Depending upon the data integration system used, the ppm values can be converted weight % for response factor calculations and for recording purposes.	1 to
1297 1298	 Set up the chromatography data system for an area normalization response fac calibration. 	tor
1299 1300	 Analyze the calibration standard gas bulb in triplicate using the chromatograph conditions described in Section C.7.9.3(1). 	hic
1301 1302	 Perform the necessary functions to have the data system determine each component response factor that is then stored. 	ent
1303 1304	 Response factors for each component are calculated as shown in Equation <u>18</u> a Equation <u>19</u>. 	and

$$ARF_i = \frac{weight\%_i \text{ in calibration standard}}{A_i}$$
18

$$ARF_i = \frac{100.0000 - S}{A_r}$$
 19

1306	A_i	=	peak area of component <i>i</i>
1307	A_r	=	peak area of major refrigerant
1308	ARF_i	=	Absolute response factor of component <i>i</i>
1309	ARF_r	=	Absolute response factor of the major refrigerant
1310	S	=	weight % sum of all impurities present

Where:

Then using the major refrigerant, r, as the reference peak, the RRF can now be determined as shown in Equation 20 and Equation 21.

$$RRF_i = \frac{ARF_i}{ARF_r}$$
 20

The weight percentage of each component is calculated as follows:

$$W_i = \frac{RRF_i \cdot A_i \cdot 100}{\sum(A_i \cdot RRF_i)}$$
21

Where:	
WINCIC.	

A_i	=	peak area of component <i>i</i>
RRFi	=	Relative response factor for component <i>i</i>
Wi	=	weight percent of component <i>i</i>
$\sum (A_i \cdot RRF_i)$	=	sum of all component peak areas times their respective
		relative response factors

1320	C.7.9.4.	Sampling			
1321		Submitted sample cylinders shall contain liquid phase for analysis.			
1322		Note: Eighty percent liquid full should be used for analysis.			
1323 1324 1325 1326 1327		Special handling for low <i>critical temperature</i> refrigerants R-13, R-23, and R-116: A vapor phase sample shall be used to determine non-condensables and volatile impurities, including other refrigerants. The vapor phase sample is obtained by regulating the sample container temperature to 5°C or more above the refrigerant <i>critical temperature</i> . <i>Critical temperatures</i> : $R-13 = 28.8$ °C, $R-23 = 25.9$ °C, and $R-116 = 19.7$ °C.			
1328	C.7.9.5.	Sample Analysis			
1329 1330 1331 1332 1333		Analyze the sample using the chromatographic conditions described in Section C.7.9.1. Load the sample injection device by slowly and completely vaporizing the liquid phase, for example, by bubbling the vapor into water through flexible polymer tubing and then puncturing the tubing with the syringe needle. An alternative apparatus for vaporizing a liquid sample into a glass gas sample bulb allowing repeat injections of the same sample is shown in Figure 5.			
1334		Note: See example gas chromatograms in <u>Appendix D</u> .			
1335	C.7.9.6.	Calculations			
1336		1) The weight percentage of each component is calculated as shown in Equation 22 .			
		$W_i = \frac{RRF_i \cdot A_i \cdot 100}{\sum(A_i \cdot RRF_i)}$ 22			
1337		Where:			
1338		A_i = peak area of component <i>i</i>			
1339		RRF_i = Relative response factor for component <i>i</i>			
1340		W_i = weight percent of component <i>i</i>			
1341 1342		$\sum (A_i \cdot RRF_i)$ = sum of all component peak areas times their respective relative response factors			
1343		2) Record the sample component concentrations to the nearest 0.01%.			
1344					

1347

Table 34 Component Statistical Parameters for the Determination of Purity of New and Reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R 143a, R-152a, R-218, R-290, R-600, and R-600a

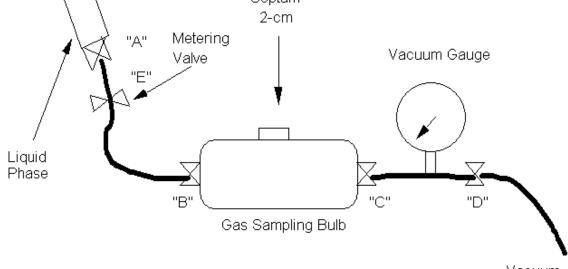
Component	Detection Limit, ppm	Concentration Range Investigated, ppm	Concentration Precision at 95% Confidence Limit, ppm	Relative Mean Error, %	
Methane	1	5	0.07	4	
R-23	2	25	0.54	-2.3	
R-1150 (C ₂ H ₄)	1	5	0.13	-5.6	
R-170 (C ₂ H ₆)	1	5	0.1	-4.1	
R-13	3	30	0.47	-3.8	
R-143a	1	25	0.3	3.3	
R-152a	1	30	0.63	1.7	
R-40	1	20	0.37	2.3	
R-134a	1	45	0.27	-3.3	
R-22	2	65	1.75	2.7	
R-1170 (C ₃ H ₆)	1	5	0.1	3.4	
R-115	2	115	1.67	1.8	
R-142b	1	20	0.23	-1.3	
R-124	1	25	0.37	1.8	
R-133a	1	35	0.23	1.8	
R-21	2	50	0.83	1.8	
R-600a	1	20	0.23	-2.8	
R-114	2	50	0.83	2	
R-600	1	20	0.18	-3.3	
2-butene-T	1	5	0.06	-3.8	
R-11	4	40	0.87	1.1	
R-123	2	35	1.05	-4.7	
2-butanol	2	20	0.33	1.6	
MEK	2	25	0.47	-2.3	
R-113	2	30	0.87	-4	
n-pentane	1	5	0.25	-3.7	

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Table 35 Primary Calibration Standard Components for the Determination of Purity of New and Reclaimed R-12, R-13, R-22, R-23, R-114, R-115, R-116, R-124, R-125, R 143a, R-152a, R-218, R-290, R-600, and R-600a

Component	Molecular Weight	Volume Added, µL	Mass Added ¹ , µg	Added ² Concentration, ppm	Total Concentration Present ³ , ppm
Methane	16	20	13.1	5	
R-23	70	22	63	23	
C_2H_4	28	12	13.7	5	
C ₂ H ₆	30	11	13.5	5	
R-13	104	20	85.4	31	
R-143a	84	20	68.8	25	
R-152a	66	30	81	30	
R-40	50	28	57.8	21	
R-134a	102	30	125.1	46	
R-22	86	50	176.9	64	
C ₃ H ₆	42	8	13.7	5	
R-115	154	50	315.9	115	
R-142b	100	15	61.7	22	
R-124	136	12	67	24	
R-133a	118	20	97	35	
R-21	103	32	134.7	49	
isobutane	58	25	59.3	22	
R-114	170	20	139.8	51	
n-butane	58	25	59.3	22	
2-butene-T	56	6	13.7	5	
R-11⁴	137		5	57	
R-123 ⁴	153		5	38	
MEK ⁴	72		5	17	
R-113 ⁴	188		5	27	
2-butanol ⁴	74		5	21	

Component	Molecular Weight	Volume Added, µL	Mass Added ¹ , µg	Added ² Concentration, ppm	Total Concentration Present ³ , ppm		
n-pentane4	72		5	5			
Notes:							
	ecessary, correct blished.	the mass adde	ed for the purity of	the calibration co	omponent previously		
2. Valu	es shown are for	illustration; exa	ct values are determin	ned in Section C.7.9	0.2(<u>10</u>).		
			the amount prese blank to enter data.	nt in stock R-12	l [see the note in		
	-	1	ient laboratory tempe rough Section C.7.9.2		d to the 500 mL bulb		
5. See S	Section C.7.9.2(1	5) to determine	mass added.				
— = Inter	ntionally left blan	k					
Calibration Chemical or Sample Cylinder							
Septum 2-cm							



٧a	cuum	

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1353	Figure 5 Apparatus Used for Calibration Standard Preparation and for
1354	Cylinder Sampling

1356	C.8.	Detern	nination of Purity of New and Reclaimed R-123 by Capillary and Packed Column Gas Chromatography	
1357		C.8.1.	Purpose	
1358 1359			This test method determines the purity of new and reclaimed 1,1-dichloro-2,2,2-trifluoroethane (R-123) by gas chromatography.	
1360		C.8.2.	Scope	
1361			This test method is for use with R-123.	
1362		C.8.3.	Definitions	
1363			Definitions for this section are identical to those in <u>Section 3</u> and AHRI 740.	
1364		C.8.4.	Principle	
1365 1366 1367 1368			The organic purity of new and reclaimed R-123 is determined by programmed temperature subambient capillary column gas chromatography, and the R-123 and R-113 isomers determined isothermally using a packed column. Component peak areas are integrated electronically and quantified by the area normalization response factor method.	
1369		C.8.5.	Applicability	
1370 1371			This method is applicable to the determination of the impurities present in commercially manufactured R-123. The impurities profile in reclaimed R-123 is expected (more or less) to be the same as the new product.	
1372		C.8.6.	Limitations and Interferences	
1373 1374 1375 1376			This method is calibrated for only those impurities commonly present in R-123 from commercial sources. Other impurities that have been detected on occasion are listed (with retention times) in Table 39. The method does not detect any impurity that can elute within the comparatively large R-123 peak matrix on either column.	
1377		C.8.7.	Sensitivity, Precision and Accuracy	
1378 1379			Statistical parameters for each impurity are listed in Table 38. The data was obtained by analyzing an R-123 calibration mixture seven times during one day by one operator.	
1380		C.8.8.	Special Apparatus and Reagents	
1381			The following is a list of special apparatus and reagents unique to this analysis:	
1382 1383			1) Gas chromatograph: Equipped with an FID, capillary column split injector, subambient (liquid nitrogen) cooling valve, and packed column capability.	
1384 1385			2) Chromatography data system: Capable of electronic integration and processing chromatographic data.	
1386 1387 1388 1389			3) Gas chromatographic column (packed): One percent high molecular weight compounds of polyethylene glycol and a diepoxide reacted with nitroterephthalic acid on 60-80 mesh graphitized carbon with a nominal surface area of 100 m ² /g in a 7.3 m, 3.20 mm OD stainless steel column. Prepacked columns are commercially available.	
1390 1391			4) Gas chromatographic column (capillary): 210 m (connect the following two columns together with the first column end attached to the injection port):	
1392			a) 105 m 14 % cyanopropylphenyl-86% methylpolysiloxane, 0.25 mm, 1µm.	
1393			b) 105 m 5 % diphenyl-95% dimethyl polysiloxane, 0.32 mm, 1µm.	
1394 1395			5) Glass collecting tube: 125 mL. Enlarge side outlet opening to accommodate a crimp-on 2 cm septum. Apply fiberglass tape outside for protection.	
1396			6) Syringe, 10 μL, liquid	
1397			7) Serum bottle: 125 mL	
1398			Note: The bottle holds 160 mL of liquid when full.	
1399			8) R-123 and most impurities for calibration standard preparation are commercially available.	

The purity of each calibration component shall be predetermined by gas chromatography FID or TCD, or both, and, if necessary, by gas chromatography/mass spectroscopy (GC-MS).

C.8.9. Procedure

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C.8.9.1. Chromatographic Operating Conditions, Packed Column

Table 36 shows chromatographic operating conditions for R-123 packed columns.

Table 36 Chromatographic Operating Conditions for R-123 Packed Column

Parameters	Settings
Detector	FID
Carrier gas	40 mL helium per minute
Column temperature, °C	125 isothermal
Detector temperature, °C	250 ¹
Injector port temperature, °C	150 ¹
Sample	2 µL ²
Maximum safe column temperature, °C	225 (for conditioning purposes)
Notes:	·

1. Condition can be optimized for specific GC used.

2. Externally cool the syringe and sample to 10°C before sampling.

C.8.9.2. **Chromatographic Operating Conditions, Capillary Column**

Table 37 shows chromatographic operating conditions for R-123 capillary columns.

Parameters	Settings
Detector	FID
Carrier gas	1.4 mL helium per minute
Split flow	40:1
Injector port temperature, °C	200 ¹
Detector temperature	200 ¹
Sample	2 μL ²
Initial column temperature, °C	0 (subambient, liquid N ₂)
Initial hold	twenty-one minutes
Program, °C per minute	15
Final temperature, °C	165
Post hold	eighteen minutes

Table 37 Chromatographic Operating Conditions for R-123 Capillary

2. Externally cool the syringe and sample to 10°C before sampling.

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C.8.9.3. **Calibration Standard, Preparation and Analysis**

- 1) Obtain a stock of the highest purity R-123 as evidenced by the chromatograms using the procedures described in Section C.8.9.
 - Note: To accurately calibrate for R-1112a, select a stock R-123 that does not contain any detectable R-114aB1. The purest R-123, however, contains the impurities listed in Table 38 in low concentrations. Individual impurity peak areas in the stock R-123 are increased in the calibration standard by the amount of the corresponding impurity added in ppm. The amounts in the stock are thereby determined by the method of standards addition. The amount present, if any, is combined with the amount added to give the total of the component present, in ppm, in the calibration standard.
- 2) Determine the tare weight to the nearest 0.0001 g with a 125 mL serum bottle with septum and cap loosely attached; then fill with stock R-123 to within 5/8 in of the top. Crimp-on the septum.
- 3) Reweigh and subtract the tare weight determined in Section C.8.9.3(2) to obtain the grams of R-123 added.
- 4) Individually and in turn add the volumes of each calibration component indicated in Table 40 through the septum and below the R-123 liquid surface in the bottle. Use a µL or mL gas tight syringe with a deflected point needle. Shake the bottle to mix after addition of each component.

1430 1431 1432 1433		Note: To preserve the stock of calibration component that are gases, a small 125 m gas collecting tube that has been evacuated to 1 atm should be loaded from the liquid phase of the gas as illustrated in <u>Figure 6</u> . The volume is the withdrawn and injected into the serum bottle containing the R-123.	om
1434 1435 1436	5)	Total the mass added to the bottle and combine this weight with that Section C.8.9.3($\underline{3}$) to obtain the total weight to the nearest 0.0001 g of calibrat sample in the bottle.	
1437 1438	6)	Calculate the amount added to the nearest 1 ppm for each component by dividing mass added by the total weight of sample in the serum bottle, see Section C.8.9.3(
1439 1440 1441 1442	7)	Calculate the amount present for each component by combining the amount present the stock R-123 (if any) to the amount of the component added [see the note Section C.8.9.3(1) and the following note]. The component present values, in ppm, those used for determining the method response factors.	e in
1443 1444 1445 1446 1447 1448		Note: The concentration of R-123a in the stock is determined separately by method of standards addition (adding percent amounts of R-123a to the sto R-123 and chromatographing as in Section C.8.9.1). The calculated RRF _R -value is assigned to the R-123b isomer, as R-123b is not commercial available for separate calibration. The amounts present are added to Table the R-123a isomer shown as percent present.	ock -123a ally
1449 1450 1451 1452	8)	Write the present values for each component on the label in ppm, as well as the d of preparation, the gross weight, and the total grams of the calibration sample. St in a refrigerator. Discard and prepare a new standard when the sample weight fa below 60% of the original weight.	tore
1453	C.8.9.4. Determ	ination of Component Response Factors	
1454 1455	1)	Set up the chromatography data system for an external standard area normalizat calibration.	ion
1456 1457	2)	Analyze the calibration standard solution in triplicate using the chromatograp conditions described in Section $\underline{C.8.9.1}$ and Section $\underline{C.8.9.2}$.	hic
1458 1459 1460	3)	Using R-123 as the reference peak, perform the necessary functions to have integrator determine each component relative response factor (RRF_i) that is th stored. Response factors are calculated as shown in Equation 23 and Equation 24.	
		$ARF_i = \frac{weight\% \text{ in calibration standard}}{A_i}$	23
		$ARF_{R-123} = \frac{100.0000 - S}{A_{R-123}}$	24
1461		Where:	

1462	A_i	= peak area of component i (average of three determinations)
1463	ARF_i	Absolute response factor of component <i>i</i>
1464	S	= weight % sum of all impurities present to ppm levels
1465 1466	Then, using R-123 as the reference peak, the RRF can be calculated as shown in Equation 25 .	

	$RRF_i = \frac{ARF_i}{ARF_{R-123}}$ 25			
1467	RRF_i values are computed to the nearest 0.0001 unit.			
1468	Samples shall be submitted in either metal cylinders or in glass bottles, containing at least 60%			
1469	liquid but not more than 80% full.			
1470	C.8.9.5. Sample Analysis			
1471 1472 1473 1474 1475	Analyze the sample using the chromatographic conditions described in Section C.8.9.1 and Section C.8.9.2. The sample and syringe are precooled in a refrigerator to 10°C before sampling to simplify loading liquid sample into the μ L syringe. By spiking components or doing GC-MS, or both, unidentified peaks can be identified. Use the <i>ECN method</i> wherever applicable to estimate the concentration of any identified components not in the calibration table (see Table 20)			
1476 1477	Table 39).Note:See example gas chromatograms in Appendix D.			
1478	C.8.9.5.1. Check for Presence of R-114aB1			
1478 1479 1480 1481 1482 1483 1484 1485 1486 1487	The capillary column procedure does not resolve R-1112a and (if present) R-114aB1. If the R-114B1 peak is small or absent, then R-114aB1 is not present. To resolve R-1112a and R-114aB1, the sample is reanalyzed exactly as in Section <u>C.8.9.2</u> except the column initial temperature is 40°C. The higher starting temperature resolves the R-114B1, R-114aB1 and R-1112a into a triplet in the order given with 0.12 minutes separation between the three peaks. In the absence of R-114aB1, the peak separation between R 114B1 and R-1112a remains at 0.25 minutes. Use the <i>ECN method</i> (Table 39) to estimate the amount of R-114aB1 present.			
1488	C.8.9.5.2. Check for R-122 Isomers			
1489 1490	If R-122 isomers are suspected to be present, extend the capillary column procedure post hold for an additional fifteen minutes (see Table 39).			
1491	C.8.9.6. Calculation			
1492	1) The weight percentage of each component is calculated as shown in Equation 26 .			
	$W_i = \frac{RRF_i \cdot A_i \cdot 100}{\sum (A_i \cdot RRF_i)}$ 26			
1493	Where:			
1494	$A_i = \text{peak area of component } i$			
1495	RRF_i = relative response factor for component <i>i</i>			
1496	W_i = weight percent of component <i>i</i>			
1497 1498	$\sum (A_i \cdot RRF_i) =$ sum of all component peak areas times their respective relative response factors			
1499	2) Record the sample component concentrations to either the nearest 0.0001% or to the			
1500	nearest 1 ppm.			
1501				

Component	ECN ¹	Detection Limit, ppm	Range Investigated, ppm	Precision at 95% CL ² , ppm	Relative Mean Error, %
R-1113	1.69	1	25	0.37	0.95
R-12	0.35	3	25	0.37	-1.1
R-22	0.4	2	25	0.24	1.4
R-114	1.04	2	50	1.2	-2.1
R-1317mx	3.63	1	30	0.88	4.3 ³
R-31	0.92	1	10	0.52	2.2
R-216ba	2.16	1	20	0.67	-1.8
R-1326mxz	3.65	1	15	0.33	0.7
R-133a	1.93	1	40	0.67	1.9
R-114B1	0.95	2	50	0.8	2.4
R-1112a	1.64	1	25	0.3	-0.7
R-1112	1.64	1	15	0.27	-0.5
R-123a	1.84	2	50 000	1300	0.3
R-123b	1.8	2	400	12.7	
R-11	0.43	3	60	2.2	1.8
R-30	0.63	2	50	1.1	0.3
R-113	1.6	3	300	7.3	-0.2
R-113a	1.68	3	250	7	-0.15
R-1111	1.9	2	15	0.67	0.8

Table 38 Component Statistical Parameters for the Determination of Purity of New and Reclaimed R-123

Notes:

1. *ECN* determined experimentally or estimated. Refer to scientific literature on *ECN*.

2. Intra-lab, multiple operator

3. Combining both isomers

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	Method	
Impurity	Capillary Column Retention Time, min	ECN^1
R-1132	9.18	2
R-125	9.46	0.79
R-134a	9.8	1.67
R-114a	11.22	1.17
R-124a	11.56	1.27
R-1122	11.57	1.76
R-124	11.77	1.33
R-E328lcc ether ²	14.59	3.9
R-114aB1	15	0.8
R-141b	19.9	2
R-1121	23	1.75
R-132b	25.35	1.9
R-1130-Е	25.64	2.25
R-123B1	28.72	1.7
R-122b	36.28	1.75
R-122a	37.24	1.75
R-122	38	1.76
R-112a	43.55	1.48
as shown in Secti	experimentally or estimated. Refer to sci on $C.8.9.7$ and Equation 27 .	
2. Structure tentativ	ely identified as: CHClF-CF ₂ -O-CF ₂ -CF	3.
Select a nearb	by ECN Method y peak in the chromatogram whose iden ed (the internal standard). See Equation	
$\frac{RF_i}{RF_r} = \frac{ECN_r}{ECN_i}$	$=rac{MW_i}{MW_r}$	

Table 39 Additional Impurities Observed in R-123, Quantitation by ECN Method

Where:

1513 RF either absolute or relative response factor = molecular weight of the component to be determined 1514 MW_i = molecular weight of the internal standard reference peak 1515 MW_r =

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Component	Molecular Weight	Volume Added, µL	Mass Added ¹ , µg	Added Concentration ² , ppm	Total Concentration Present ³ , ppm
R-1113	116	1	4765	22	
R-12	121	1	4946	23	
R-22	86	1.5	5307	24	
R-114	170	1.5	10 454	48	
R-1317mx ⁴	216	6	9289	416	
R-31	68	0.75	2101	10	
R-216ba ⁵	221	0.5	4517	21	
R-1326mxz	198	0.4	3270	15	
R-133a	118	1.8	8720	40	
R-114B1 ⁶	215	6	11 109	49	
R-1112a	133	1	5450	25	
R-1112	133	0.5	2725	13	
R-123a	153	7	7	1000 - 70 000	
R-123b	153	7	7	200 - 700	
R-11 ⁶	137	10	14 869	65	
R-30 ⁶	85	10	13 360	59	
R-113 ⁶	188	50	78 795	361	
R-113a ⁶	188	50	78 986	362	
R-1111 ⁶	149	6	9279	41	

Table 40 Primary Calibration Standard Components for the Determination of of Purity of New and Reclaimed R-123

Notes:

- 1. If necessary, correct the mass added for the purity of the calibration component previously established.
- 2. Values shown are for illustration; exact values are determined at Section C.8.9.3(<u>6</u>).
- 3. Fill in column after determining the amount present in stock R-123, see Section C.8.9.3(1) and Section C.8.9.3(7). Intentionally left blank to enter data.
- 4. The R-1317mx resolves into the cis and trans isomer peaks with a ratio of 1:2, respectively.
- 5. Although other R-216 isomers comprise the usual R-216 peak multiple, the R-216ba isomer is used for calibration purposes.
- 6. Add by syringe injection of the liquid.
- 7. Refer to Section C.8.9.3(7) for mass and volume added.

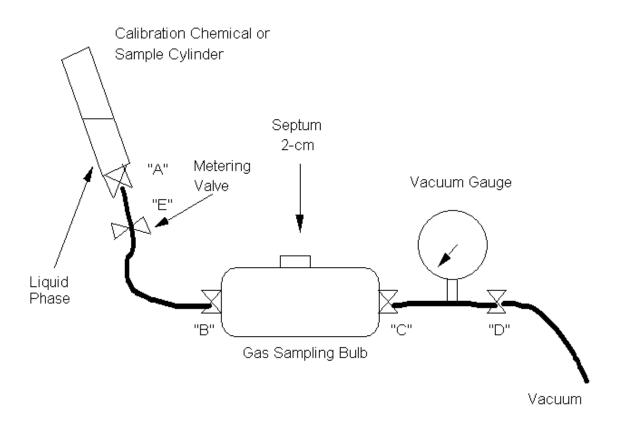


Figure 6 Apparatus Used for Calibration Standard Preparation

1524C.9.Determination of Purity of New and Reclaimed R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf,1525R-1234ze(E), R-236fa, and R-1233zd(E) by Capillary Column Gas Chromatography

C.9.1. Purpose

This test method determines the purity of new and reclaimed R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf, R-1234ze (E), R-236fa, and R-1233zd(E) by gas chromatography.

C.9.2. Scope

This test method is for use with R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf, R-1234ze(E), R-236fa, and R-1233zd(E).

C.9.3. Definitions

Definitions for this section are identical to those in <u>Section 3</u> and AHRI 740.

C.9.4. Principle

The organic purity of new and reclaimed R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf, R-1234ze(E), R-236fa, and R-1233zd(E) is determined by programmed temperature gas chromatography using capillary columns with an FID. A capillary column procedure is used because the impurities are not resolved by the packed column method. Because R-22 obscures R-31 on the packed column method (Section C.7), R-31 is determined separately by this capillary method. Component peak areas are integrated electronically and quantified by the area normalization response factor method.

C.9.5. Applicability

This method can be applicable to the determination of the impurities that can be present in commercially manufactured and reclaimed R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf, R-1234ze(E), R-236fa, and R-1233zd(E).

C.9.6. Limitations and Interferences

This method is calibrated for only those impurities commonly present in R-22, R-32, R-113, R-134a, R-141b, R-142b, R-245fa, R-1234yf, R-1234ze(E), R-236fa, and R-1233zd(E). Any impurity that elutes within the matrix of the major component interferes if present in concentration. Other impurities that have been detected are listed (with retention times) in Table 42.

C.9.7. Sensitivity, Precision, and Accuracy

Statistical parameters for each impurity are listed in <u>Table 43</u>. The data was obtained by analyzing an R-134a calibration standard mixture seven times during one day by one operator.

C.9.8. Special Apparatus and Reagents

- 1) Gas chromatograph: Equipped with an FID, capillary column split injector, subambient cooling valve (liquid nitrogen), and packed column capability
- 2) Chromatography data system: Capable of electronic integration and processing chromatographic data
- Gas chromatographic column (capillary): 135 m x 0.25 mm, 1 μm DF, 6% cyanopropylphenyl-94% dimethyl polysiloxane
 - 4) Glass collecting tubes: 125 mL and 500 mL. (Enlarge the side outlet opening to accommodate a crimp-on 2-cm septum. Apply fiberglass tape outside for protection.)
 - 5) Steel cylinder: 1 L, with a single 9-gauge valve
 - 6) Syringe, 1 mL, gas tight
 - 7) Deflected point needle: Standard hub 22 gauge x 1-1/2-in stainless steel
- 8) Swivel union: 1/4 in female flare x 1/4-in female flare
- 15669)R-134a and impurities for calibration standard preparation. The identified impurities R-1336mzz1567and R-1234yf are not commercially available. The purity of each calibration component shall be1568predetermined by gas chromatography FID or TCD, or both, and, if necessary, by GC-MS.

C.9.9. Procedure

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C.9.9.1. Chromatographic Operating Conditions, Capillary Column Gas Chromatography

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			ng Condition	-		1
Condition	R-22	R-113/ R-1233zd(E)/ R-514A	R-134a/ R-32/ R-1234yf/ R-1234ze(E)/ R-236fa	R-141b	R-142b	R-245fa
Detector	FID	FID	FID	FID	FID	FID
Carrier gas, mL helium per minute	1.3	1	1	1	1	1
Injection port temperature ¹ , °C	200	200	200	200	200	200
Detector temperature ¹ , °C	200	200	200	200	200	200
Sample, mL	1	1	1	1	1	1
Initial column temperature, °C	-20	35	-20	10	10	-20
Initial hold, min	14	10	20	12	12	20
Program 1						
Ramp, °C/min	20	10	20	10	10	20
Column temperature, °C	175	160	190	100	100	125
Hold, min	6.25	11.5	4.5	5	6	10
Program 2						
Ramp, °C/min				15		20
Column temperature, °C		_		150		190
Hold, min				6.67		19.5
Total run time, min	30	34	35	36	27	60
Split ratio			40:0	1:00		•
Subambient cooling			Liqui	id N ₂		
Maximum safe column temperature, °C	280					

Note:

1. Condition can be optimized for specific GC used.

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1572	C.9.9.2.	Example	e - Primary Calibration Standard, Preparation and Analysis for R-134a
1573		Note:	Modify procedure for other refrigerants as necessary.
1574 1575 1576 1577		1)	Crimp-on the septum, then determine the internal volume of the 500 mL gas bulb by weighing the bulb empty, then fill to maximum capacity with water. Record the grams of water as mL volume capacity on the outside of the bulb to the nearest 1.0 mL. Thoroughly dry the inside of the glass bulb.
1578		2)	Assemble the apparatus as illustrated in Figure 7.

1579	3)	Attach a cylinder of high purity refrigerant stock to the gas sampling bulb.
1580 1581 1582 1583 1584 1585 1586		Note: The purest stock refrigerant can contain the impurities found in the method. The ppm amounts of impurities already in the stock refrigerant are determined via the method of standards addition. Individual impurity peak areas in the stock refrigerant are increased in the calibration standard by the ppm amount of the corresponding impurity added. The ppm already present is combined with the ppm added to give the total ppm component present in the calibration standard.
1587	4)	With valve "A" closed, open all other valves, and evacuate cylinder.
1588 1589		Note: The cylinder should be evacuated to less than 100μ of Hg pressure (0.013 kPa) to prevent cross-contamination.
1590 1591	5)	Close valve "D" and monitor the gauge for several minutes to confirm that the system is not leaking.
1592 1593	6)	Close metering valve "E," open valve "A," and then slowly open valve "E" and flash <i>liquid phase</i> stock refrigerant to bring the system to 1 atm. Close valve "A."
1594	7)	Repeat Section C.9.9.2($\underline{4}$) through Section C.9.9.2($\underline{6}$).
1595	8)	Close valves "B" and "C" and remove the bulb from the vacuum/sampling apparatus.
1596	9)	Calculate the grams of stock refrigerant added to the bulb as shown in Equation 28 .
		$grams \ added = \frac{MW_{ref} \cdot internal \ volume \ of \ bulb \ (ml)}{24 \ 450} $ 28
1597		Where:
1598		MW_{ref} = molecular weight of the stock refrigerant, g/mole
1599 1600		24 450 = volume (mL) occupied by 1 mole of R-134a at 25°C and 1 atm
1601 1602 1603 1604 1605 1606	10)	Individually and in turn, add the volumes of each gaseous calibration component indicated in Table 39 to the calibration bulb. Use a μ L or mL gas tight syringe with a deflected point needle. To preserve the stock of calibration component, a small, evacuated 125 mL gas collecting tube shall be loaded to 1 atm from the <i>liquid phase</i> as illustrated in Figure 7. The volume is then withdrawn and injected into the 500 mL calibration bulb.
1607 1608 1609 1610 1611	11)	Into a 30 mL (37 mL filled) serum bottle, capped and crimped with a septum, add the exact volumes of the liquid impurities from Table 45 in the order given. Add by syringe injection through the septum using a 22-gauge or smaller needle as a vent. After addition, shake bottle vigorously to mix. Label, date, and store the filled serum bottle in a refrigerator.
1612		Note: Cool the syringe and R-1112a to 10°C before transferring.
1613 1614	12)	Refer to <u>Figure 7</u> . Evacuate a 125 mL bulb (internal volume premeasured) and fill to 1 atm with refrigerant stock.
1615 1616	13)	Accurately withdraw and inject exactly 5.0μ L of solution from the 30 mL serum bottle into the 125 mL bulb. Equilibrate for thirty minutes.
1617 1618 1619 1620	14)	Using a 5 mL gas tight syringe, withdraw vapor from the 125 mL bulb and inject exactly 5.0 mL into the 500 mL calibration bulb. The mass added (μ g) of each component thus added is calculated as follows and is added to column four of Table 41. See Equation 29.

$$\mu g_i = \frac{g_i \cdot 25\,000}{V \cdot A} \tag{29}$$

1652 1653

1621	Where:
1622	A = internal mL of 125 mL bulb
1623	g_i = grams from Table 44
1624	V = total mL of solution, see Section C.9.9.2(<u>11</u>)
1625	$25\ 000$ = dilution ratio
1626 1627	15) Total the mass added column and combine this weight with that of Section C.9.9.2(9) to obtain the total weight of sample to the nearest 0.0001 g in the bulb.
1628 1629	16) Calculate the amount added, to the nearest 1 ppm, for each component by dividing the mass added by the total weight of sample in the gas bulb. See Section C.9.9.2(<u>15</u>).
1630 1631 1632 1633	17) Calculate the amount present for each component, in pm, by combining the amount present in the stock refrigerant, if any, and the amount of component added [see the note in Section C.9.9.2(3)]. The component present values, in ppm, are those used for determining the method response factors.
1634 1635	 Let the gas calibration bulb stand for twenty minutes to thirty minutes to equilibrate. The standard is stable for three days to four days.
1636	C.9.9.3. Determination of Component Response Factors
1637 1638	Note: Depending upon the data integration system used, the ppm values to weight % can be converted for response factor calculations and for recording purposes.
1639 1640	1) Set up the chromatography data system for an area normalization-response factor calibration.
1641 1642	 Analyze the calibration standard bulb in triplicate using the chromatographic conditions described in Section <u>C.9.9.1</u>.
1643 1644 1645	3) Perform the necessary functions to have the data system determine each component's relative response factor (<i>RRF_i</i>) that is stored. Response factors are calculated as shown in Equation $\underline{30}$ and Equation $\underline{31}$.
	$ARF_i = \frac{weight\% \text{ in calibration standard}}{A_i}$ 30
	$ARF_r = \frac{100.0000 - S}{A_r}$ 31
1646	Where:
1647	A_i = peak area of component <i>i</i> (average of three determinations)
1648	A_r = peak area of major refrigerant
1649	ARF_i = Absolute response factor of component <i>i</i>
1650	ARF_r = Absolute response factor of component r

S = weight % sum of all impurities present

Then, using the major refrigerant r as the reference peak, the RRF can now be determined as shown in Equation <u>32</u>.

$$RRF_i = \frac{ARF_i}{ARF_r}$$
32

1654			RRF_i values are computed to the nearest 0.0001 unit.
1655	C.9.9.4 .	Example	e - Secondary Calibration Standard Preparation for R-134a
1656 1657 1658 1659 1660 1661		Note:	A secondary calibration standard is prepared in much larger quantity due to the comparatively short lifetime of the primary bulb standard. The primary bulb standard is necessary initially because of the inherent phase distribution of added components if simply preparing and calibrating a standard such as described here. The secondary standard is analyzed as a sample against the primary standard and then used subsequently as the daily calibration standard.
1662		Note:	Modify procedure for other refrigerants as necessary.
1663 1664		1)	Evacuate a one-liter steel cylinder and determine the cylinder's tare weight to the nearest 0.1 g.
1665 1666		2)	Attach a septum nut and septum to the valve and then cool the cylinder in ice water. Open the cylinder valve.
1667 1668 1669 1670		3)	While keeping cold in ice water, individually and in turn add 500 times the volume of each gaseous component given in calibration Table 44 to the cylinder by syringe injection through the septum. Add 0.10 mL of the liquid refrigerant mixture from Section C.9.9.2(<u>11</u>). Close the cylinder valve and remove the septum nut and septum.
1671 1672		4)	Evacuate a second clean, dry one-liter steel cylinder and determine the tare weight to the nearest 0.1 g.
1673 1674 1675 1676		5)	Cool the cylinder in ice water and attach a section flex line that is not longer than 61 cm from the stock cylinder supply. Purge a small amount of the stock refrigerant through the flex line before immediately attaching the flex line to the one-liter cylinder.
1677 1678 1679 1680		6)	Open the one-liter cylinder valve, then open the stock cylinder valve and, while keeping cold in the ice water, fill the one-liter cylinder with 950 g of liquid refrigerant. The flex line can be reconnected and more R-134a added until a total of 950 g has been added. If more than 950 g is added, vent the cylinder to 950 g.
1681 1682 1683			During the refrigerant addition to the one-liter cylinder (secondary standard preparation), the cylinder shall be brought to ambient temperature between each weight measurement.
1684 1685 1686		7)	Place the secondary one-liter standard cylinder, the cylinder mentioned in Section C.9.9.4(1), Section C.9.9.4(2), and Section C.9.9.4(3), in the ice bath and cool for thirty minutes.
1687 1688 1689 1690 1691		8)	Using a short double female swivel coupler, invert the 1 L cylinder containing the 950 g of refrigerant and connect to the secondary standard cylinder. Open the valve and purge the refrigerant vapor to sweep the coupler before immediately connecting to the secondary standard cylinder. Warm without overheating the cylinder containing the refrigerant with a heat gun.
1692 1693		9)	Open the valves on both cylinders so that all the refrigerant transfers into the calibration standard cylinder. Close the cylinder valves.
1694 1695 1696		10)	Remove the calibration cylinder from the ice bath and allow the cylinder to reach ambient laboratory temperature before the final weighing. Dry off and then reweigh to the nearest 0.1 g.
1697 1698 1699		11)	Subtract the tare weight from the total weight to obtain the total grams of standard in the cylinder [see Section C.9.9.4(1)]. Record this weight together with the cylinder tare weight and date of preparation on the cylinder label.

1700		12)	Roll the cylind	er for one h	our to	o thoroughly mix.	
1701 1702		13)	• •			triplicate as described in Section <u>C.9.9.1</u> loading first nown in <u>Figure 7</u> .	
1703 1704 1705 1706 1707		14)	nearest 1 ppm. each. This cyl standard weigh	List each c inder is use nt indicates t	compo ed hen that th	electronically (see Section <u>C.9.9.7</u>) and tabulate to the onent on the cylinder label with the ppm amount for neeforth as the calibration standard until the loss of the internal volume of liquid phase is less than 60% of cylinder. For liquid densities, see Table 26.	
1708	C.9.9.5.	Sampling					
1709		Submitt	Submitted sample cylinders shall contain liquid phase for analysis.				
1710		Note:	Eighty percent	liquid full s	should	d be used for analysis.	
1711	C.9.9.6.	Sample A	Analysis				
1712 1713 1714 1715 1716		Analyze the samp bringing question	the sample using the as illustrated to 1 atm pressu table peaks. Use	in <u>Figure 7</u> ire. Use com the <i>ECN me</i>	by fla by fla bonen bonen bod t	graphic conditions described in Section <u>C.9.9.1</u> . Loa ashing the liquid phase into an evacuated gas bulb an nt spiking or GC-MS (if provided), or both, to identif to estimate the concentration of identified component -1140, see Section C.9.9.6(2).	
1717 1718		1)				phase can be flashed into a gas sampling bag and th analysis withdrawn from the bag.	
1719 1720 1721 1722 1723 1724 1725 1726 1727		2)	R-134a peak n within the large R-31, and the F shoulder of the column), repeat except that the	natrix on eit e R-134a pea R-152a/R-12 e R-134 pea at the capill column tem re resolved a	ther co eak may 243zf p ak. To llary co nperatu at abou	impurity that can elute within the comparatively larg column. For example, R-134, R-31, and R-152a elut atrix. The capillary column resolves R-134, R-1234yt pair (elute together). R-12, if present, elutes on the fa o separate R-31 and R-1140 (coelute on the capillar column analysis exactly as given in Section C.9.9. ure is held at 50.0°C (isothermal) throughout. The two but fifteen minutes retention time with the R-31 pear R-1140 peak.	
1728		3)	See example g	as chromato	ograms	s in <u>Appendix D</u> .	
1729	C.9.9.7.	Calculat	ions				
1730		1)	The weight per $W_i = \frac{RRF_i}{\sum (A_i)}$	-	each c	component is calculated as shown in Equation <u>33</u> . 33	
1731			Where				
1732			A_i	=	pe	eak area of component <i>i</i>	
1733			RRF_i	=	Re	elative response factor for component <i>i</i>	
1734			W_i	=	W	eight percent of component <i>i</i>	
1735 1736			$\sum (A_i)$	RRF_i) =		um of all component peak areas times their respectiv elative response factors	
1737 1738 1739		2)		If results a	re less	ncentrations to either the nearest 0.0001% or to the s than the individual DLs (see Table 42), then record	

1740	
1741	

Impurity	Column Retention Time Capillary, min	ECN^1
R-1243zf	14.98	2.84
R-1336mzz	—	2.9
R-1234yf	13.75	2.65
R-22	16.4	0.4
R-123a	_	1.84
R-124a	—	1.27
R-245cb		2.6
R-1225ye		2.42
R-1113	—	1.69
R-263fb	—	2.95
R-1140	21.5	2.08
R-132b		1.9
R-13	—	0.23
R-1318my-T	—	2.95
R-1318my-C	—	2.95
	nined experimentally or estimated. Refe tion <u>C.9.9.8</u> and Equation <u>34</u> .	r to scientific literature

C.9.9.8. Quantitation by ECN Method

Select a nearby peak in the chromatogram whose identification and response factor (RF) have been established (the internal standard). See Equation <u>34</u>.

34
response factor
omponent to be determined
nternal standard reference

Table 42 Additional Impurities Observed in R-134a, Quantitation by ECN Method

Chromatography					
Component	ECN ¹	DL, ppm	Range Investigated, ppm	Precision at 95% Confidence Level, ppm	Relative Mean Error, %
R-23	0.16	4	15	0.7	1.8
R-32	0.62	2	15	0.3	1.2
R-1123	1.93	1	20	0.2	-0.8
R-143a	2.12	1	20	0.2	1.5
R-125	0.79	2	30	0.25	3.2
R-115	0.76	5	60	0.65	-1.3
R-1243zf	2.84	1	10	0.2	-3.6
R-12	0.35	2	40	0.3	1.8
R-1122	1.76	1	15	0.2	2.2
R-124	1.33	1	40	0.45	2
R-31	0.92	1	15	0.8	1.7
R-133a	1.93	1	25	0.5	1.7
R-1336mzz	2.9	1	—	0.5 ²	
R-114	1.04	2	30	1.1	-3.3
R-114a	1.1	2	50	1.2	4.3
R-11	0.43	4	50	2.6	2.6
R-1112a	1.64	1	15	0.3	-0.2
R-1121-C	1.75	1	10	0.3	-6.7
R-123	1.76	2	20	0.9	-3.3
R-1121-T	1.75	1	30	1	4.3
R-113	1.6	2	20	1.3	1.7
R-134	1.61	2	30	0.2	1.4
R-152a	1.08	1	30	0.2	0.8
R-1234yf	2.65	1	_	0.5 ²	_

Table 43 Component Statistical Parameters for Capillary Column Gas Chromatography

Notes:

1. *ECN* were determined experimentally. Refer to scientific literature on *ECN*.

2. Precision estimated at 10 ppm based upon sample reproducibility.

— = Intentionally left blank

Component	Molecular Weight	Volume Added, µL	Mass Added ¹ , µg	Added ² Concentration, ppm	Total Concentration Present ³ , ppm
R-23	70	12	34.73	15	
R-32	52	16	34.03	15	
R-1123	82	14	46.98	20	
R-143a	84	14	48.1	20	
R-125	120	14	68.72	30	
R-115	154	22	139.05	60	
R-134	102	28	116.81	50	
R-152a	66	25	67.49	30	
R-12	121	20	98.89	43	
R-1122	98	8	32.23	15	
R-124	136	16	89.32	39	
R-31	68	12	33.61	14.5	
R-133a	118	12	58.17	25	
R-114	170	10	69.46	30	
R-114a	170	20	138.92	60	
R-11 ⁴	137	_	6	30	
R-1112a ⁴	133	_	6	18	
R-1121-C ⁴	115	_	5, 6	5	
R-123 ⁴	153	_	6	19	
R-1121-T ⁴	115		5, 6	23.5	
R-113 ⁴	188		6	24	

Table 44 Primary Calibration Standard Components for Capillary ColumnGas Chromatography

Notes:

1. If necessary, correct the mass added for the purity of the calibration component previously established.

2. Values shown are for illustration; exact values are determined at Section C.9.9.2(<u>16</u>).

3. Fill in column in accordance with Section C.9.9.2(<u>17</u>) after determining the amount present in stock R-134a. Intentionally left blank to enter data.

4. These components are liquids at ambient temperature and are added to the 500 mL bulb as described in Section C.9.9.2(11) through Section C.9.9.2(14).

5. R-1121 contains 17.5% of the cis isomer. The mass of R-1121 added times 0.175 is assigned to the cis isomer, the balance to the trans isomer.

6. See Section C.9.9.2($\underline{14}$) to determine mass added.

— = Intentionally left blank

Component	Volume Added, mL	Density at 20°C	Mass, g				
R-113	6	1.565	9.39				
R-1121	8	1.403	11.224				
R-123	5	1.47	7.35				
R-11	8	1.487	11.896				
R-1112a	5	1.439 (at 10°C)	7.195				



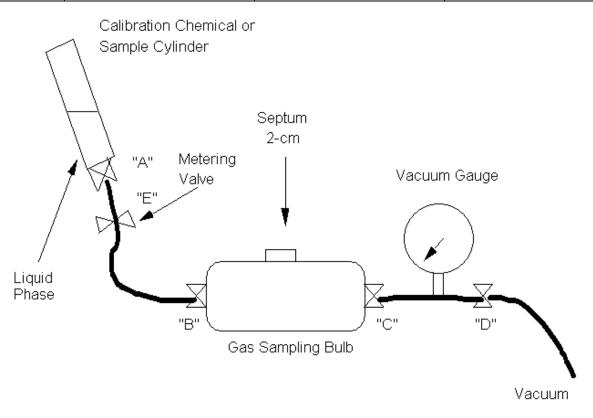


Figure 7 Apparatus Used for Calibration Standard Preparation and for Cylinder Sampling

1762 1763	C.10.	Determination of Composition of New and Reclaimed 400 Series and 500 Series Refrigerant Blends by Gas Chromatography								
1764		C.10.1. Purpose								
1765 1766			This test method determines the composition of all new and reclaimed 400 series and 500 series refrigerablends by gas chromatography.							
1767		C.10.2.	Scope							
1768			This test method is for use with all 400 series and 500 series refrigerant blends as listed in ASHRAE 34.							
1769		C.10.3.	Definiti	ons						
1770			Definition	Definitions for this section are identical to those in <u>Section 3</u> and AHRI 740.						
1771		C.10.4.	Princip	le						
1772 1773 1774 1775			400 series and 500 series refrigerant blend compositions are separated by gas chromatography using a packed column with a liquid phase coated onto a solid support. Separated components are detected using a TCD. The peak areas from the detector are measured with a data system capable of electronic integration, and component concentrations are quantified by the area normalization response factor method.							
1776		C.10.5.	Applica	bility						
1777 1778 1779 1780			This method is applicable to the routine gas chromatographic determination of all new and reclaimed blends of 400 series and 500 series refrigerant blends mixture compositions. At laboratory ambient temperature, R-13/R-23 mixtures of R-503 and R-116/R-23 mixtures of R-508 are all in gas phase, as their <i>critical temperatures</i> are low.							
1781		C.10.6.	10.6. Limitations and Interferences							
1782 1783 1784 1785		This method does not address components other than those found as the major components in the 400 series and 500 series refrigerant blends. R-115 and R-290 elute at the same retention time and interfere with each other if both compounds are present. Any impurity that elutes within the matrix of any of the major components interferes if present.								
1786		C.10.7.	C.10.7. Sensitivity, Precision, and Accuracy							
1787			C.10.7.1	l. Precision						
1788				C.10.7.1.1.	Single Operator					
1789 1790 1791								s), and 95% CLs (95% CL) test method are shown in		
1792 1793			Tab	le 46 Standard	Deviation and M Analysis for Si		certainty of R-	404A		
				Component	$\overline{\mathrm{X}}$, Weight %	σ	95% CL			
				R-143a	51.35	0.02	± 0.047			
				R-125	44.52	0.012	± 0.028	_		
			l	R-134a	4.13	0.017	± 0.040			
1794 1795					The data in <u>Table</u> sample performed			ate analyses of one standard eriod.		
1796				C.10.7.1.2.	Multiple Operato	ors				
1797 1798 1799								s), and 95% CLs (95% CL) e test method are shown in		

		[Component	$\overline{\mathrm{X}}$, Weight %	σ	95% CL	
		-	R-143a	51.59	0.04	± 0.084	-
		-	R-125	44.01	0.016	± 0.034	
		-	R-134a	4.4	0.032	± 0.068	
802		L		The data in Table 47	vas calculated	l from sixteen renlic	cate analyses of a standa
803				sample performed by		1	2
804		C.10.7.2	2. Accuracy		-		
805 806			·	racy of this method was	tested by an	alyzing a known I	R-401 blend as shown
807 808		Tal	ble 48 Standa	rd Deviation and Mea Analysi		ncertainty of R-4	ł01
			Component	Standard Concentrat Weight %	ion, Rel	ative Mean Error, Weight %	
		R-	-22	34.86		0.17	
		R-	-152a	25.65		0.16	
		R-	-124	39.49		0.05	
					-	te analyses of a stan	dard sample performed l
810 811 812	C.10.8.	Special 1)	multiple a Apparatus and Gas chromato	nalysts over a single-day d Reagents graph: Equipped with a	period.	·	
810 811 812 813 814 815 816	C.10.8.	-	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or	nalysts over a single-day d Reagents graph: Equipped with a	period. packed colu f electronic in red to capture	umn injector and ntegration and proce e peak areas enablis	a TCD capable of over ssing the chromatograph ng measurement of pea
 810 811 812 813 814 815 816 817 818 	C.10.8.	1)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks	nalysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of a system shall be configu equal to 0.001% by weig	period. packed colu- f electronic in red to capture nt. If the peak	umn injector and ntegration and proce e peak areas enablin is identified, then the tem should be giver	a TCD capable of over ssing the chromatograph ng measurement of pea he peak shall be quantifient n a default response fact
 810 811 812 813 814 815 816 817 818 819 820 821 822 	C.10.8.	1)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by the greater of the average graphic column (Packed): iepoxide reacted with nitr re area of 100 m ² /g in a 7.3	period. packed colu- f electronic in red to capture nt. If the peak the data syst e response fac 1 percent high percent high	umn injector and ntegration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrat n molecular weight of acid on 60-80 mesh	a TCD capable of over ssing the chromatograph ng measurement of peat he peak shall be quantified n a default response fact ted components or R-22 compound of polyethyles graphitized carbon with
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 	C.10.8.	1) 2)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by the greater of the average graphic column (Packed): iepoxide reacted with nitr re area of 100 m ² /g in a 7.3	period. packed colu- f electronic in red to capture nt. If the peak the data syst e response fac 1 percent high percent high percent high percent halic m, 3.20 mm (ge side outlet	umn injector and ntegration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrat n molecular weight of acid on 60-80 mesh OD stainless steel con-	a TCD capable of over ssing the chromatograph ng measurement of peal he peak shall be quantified in a default response fact ted components or R-22. compound of polyethyles graphitized carbon with olumn. Prepacked column
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 	C.10.8.	1) 2) 3) 4)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by s the greater of the average graphic column (Packed): iepoxide reacted with nitr re area of 100 m ² /g in a 7.3 fully available. ng tube: 500 mL. (Enlar fiberglass tape to the out	period. packed colu- f electronic in red to capture nt. If the peak the data syst e response fac 1 percent high percent high percent high percent halic m, 3.20 mm (ge side outlet	umn injector and ntegration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrat n molecular weight of acid on 60-80 mesh OD stainless steel con-	a TCD capable of over ssing the chromatograph ng measurement of peal he peak shall be quantified in a default response fact ted components or R-22. compound of polyethyles graphitized carbon with olumn. Prepacked column
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 	C.10.8.	1) 2) 3) 4)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin septum. Apply	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by s the greater of the averag graphic column (Packed): tepoxide reacted with nitr e area of 100 m ² /g in a 7.3 illy available. ng tube: 500 mL. (Enlar fiberglass tape to the out der	period. packed colu- f electronic in red to capture nt. If the peak the data syst e response fac 1 percent high percent high percent high percent halic m, 3.20 mm (ge side outlet	umn injector and ntegration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrat n molecular weight of acid on 60-80 mesh OD stainless steel con-	a TCD capable of over ssing the chromatograph ng measurement of peal he peak shall be quantified in a default response fact ted components or R-22. compound of polyethyles graphitized carbon with olumn. Prepacked column
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 	C.10.8.	1) 2) 3) 4) 5)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin septum. Apply 2 L steel cyline Syringe, 1 mL	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by s the greater of the averag graphic column (Packed): tepoxide reacted with nitr e area of 100 m ² /g in a 7.3 illy available. ng tube: 500 mL. (Enlar fiberglass tape to the out der	period. packed colu- f electronic in red to capture nt. If the peak the data syste response fac 1 percent high percent h	umn injector and netgration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrate n molecular weight of acid on 60-80 mesh OD stainless steel con- t opening to accom- ction.)	a TCD capable of over ssing the chromatograph ng measurement of peal he peak shall be quantified in a default response fact ted components or R-22. compound of polyethyles graphitized carbon with olumn. Prepacked column
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 	С.10.8. С.10.9.	1) 2) 3) 4) 5) 6) 7)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin septum. Apply 2 L steel cylind Syringe, 1 mL Deflected poin	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by s the greater of the average graphic column (Packed): iepoxide reacted with nitr re area of 100 m ² /g in a 7.3 fully available. Ing tube: 500 mL. (Enlar of fiberglass tape to the out der , gas tight	period. packed colu- f electronic in red to capture nt. If the peak the data syste response fac 1 percent high percent h	umn injector and netgration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrate n molecular weight of acid on 60-80 mesh OD stainless steel con- t opening to accom- ction.)	a TCD capable of over ssing the chromatograph ng measurement of pea- he peak shall be quantified in a default response fact ted components or R-22 compound of polyethyles graphitized carbon with olumn. Prepacked colum
 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 	С.10.9.	1) 2) 3) 4) 5) 6) 7) Procedu	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin septum. Apply 2 L steel cyline Syringe, 1 mL Deflected poin	A Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. is that are not identified by sthe greater of the averag graphic column (Packed): tepoxide reacted with nitr re area of 100 m ² /g in a 7.3 illy available. ing tube: 500 mL. (Enlar of fiberglass tape to the out der , gas tight at needle: Standard hub 22	period. packed colu- f electronic in red to capture at. If the peak the data syst e response fac 1 percent high oterephthalic m, 3.20 mm (ge side outlet side for protect	umn injector and netgration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrate n molecular weight of acid on 60-80 mesh OD stainless steel con- t opening to accom- ction.)	ssing the chromatograph ng measurement of peal he peak shall be quantified n a default response fact ted components or R-22. compound of polyethyler graphitized carbon with olumn. Prepacked column
1809 1810 1811 1812 1813 1814 1815 1816 1817 1818 1819 1820 1821 1822 1823 1824 1825 1826 1827 1828 1829 1830 1831	С.10.9.	1) 2) 3) 4) 5) 6) 7)	multiple a Apparatus and Gas chromato temperature pr Chromatograp data. The data greater than or using its measu Note: Peaks that is Gas chromatog glycol and a di nominal surfac are commercia Glass collectin septum. Apply 2 L steel cyline Syringe, 1 mL Deflected poin are 1. Chromato	analysts over a single-day d Reagents ograph: Equipped with a ogramming. hy data system: Capable of system shall be configu equal to 0.001% by weig ured response factor. Is that are not identified by s the greater of the average graphic column (Packed): iepoxide reacted with nitr re area of 100 m ² /g in a 7.3 fully available. Ing tube: 500 mL. (Enlar of fiberglass tape to the out der , gas tight	period. packed colu- f electronic in red to capture nt. If the peak the data syst e response fac 1 percent high oterephthalic m, 3.20 mm (ge side outlet side for protect gauge x 1-1/ litions	umn injector and netgration and proce e peak areas enablin is identified, then the tem should be giver ctors for the calibrate n molecular weight of acid on 60-80 mesh OD stainless steel cont t opening to accomt ction.)	a TCD capable of over ssing the chromatograph ng measurement of peal he peak shall be quantified in a default response fact ted components or R-22. compound of polyethyler graphitized carbon with olumn. Prepacked column modate a crimp-on 2 c

Table 49 Chromatographic Operating Conditions for 400 and 500 Series Refrigerant Blends

Parameters	Settings
Detector current	Low ¹
Detector temperature, °C	200 ¹
Injection port temperature, °C	200 ¹
Carrier gas	20 mL helium per minute
Reference flow	As required by the GC ¹
Sample size	0.5 mL (gas syringe) ¹
Initial column temperature, °C	40
Initial hold, minutes	12
Program, °C (°F) per minute	15
Final column temperature, °C	175
Post hold, minutes	11
Maximum column temperature, °C	225 (conditioning purposes only)
Note: 1. Condition can be optimized for spec	ific GC used.

C.10.9.2. Example - Primary Calibration Standard, Preparation, and Analysis for R-401

Note: Modify this procedure for other refrigerants as necessary.

- 1) Determine the tare weight of a dry, evacuated empty steel cylinder with a nominal volume of 2 L to the nearest 0.1 g (cylinder size can vary, but size is compensated for in the following procedure).
- Calculate the weight of each component to be added to the standard. Fill the empty 2 L steel cylinder to 90% of its loading capacity. See Equation <u>35</u>.

$$g \ component_i = \frac{desired \ weight\% \ component_i}{100} \cdot safe \ load \qquad 35$$

safe load = liquid density $\cdot 0.9 \cdot 2088$ mL (allowing for 10% loading factor)

For liquid densities, refer to Table 26.

Where:

- Note: The calculations used in this procedure should be corrected for any impurities found in the component refrigerants.
- 3) Purge the connecting line using the component with the highest *boiling point* first (such as R-124, the higher boiling component) to sweep out air; connect the line to the cylinder.
- 4) Add the component with the highest *boiling point* to the cylinder and reweigh the cylinder to the nearest 0.1 g.

1853 1854 1855		ac	the amount added is less than selected, more can be added. If the amount lded is more than selected, the cylinder can be vented until the selected eight is obtained.
1856 1857 1858 1859 1860 1861 1862		This weigh with the hi) Cool the c <i>point</i> in	weight of the cylinder plus the component with the highest <i>boiling point</i> . t minus the tare weight of the cylinder equals the weight of the component ghest <i>boiling point</i> . ylinder in wet ice and then add the component at the next highest <i>boiling</i> the same manner. This weight minus the weight recorded in 10.9.2(5) equals the weight of the component with the next highest <i>boiling</i>
1863 1864 1865 1866 1867		th co co	the component should be added with the next highest <i>boiling point</i> so that e weight is less than that selected. By adding small additions, the proponent can be brought up to the selected weight. The cylinder and ontents should reach ambient laboratory temperature before making the final eighing.
1868 1869 1870 1871 1872 1873 1874 1875 1876		 with the new with the new this step un After the l one hour to be calculat percent of 	tion C.10.9.2(5) except that the refrigerant added here is the component ext highest <i>boiling point</i> and the tare weight for calculating the component ext highest <i>boiling point</i> added is the weight in Section C.10.9.2(5). Repeat til all selected components are added to the steel cylinder. ast component is added, agitate the cylinder by rolling for a minimum of o mix the contents thoroughly. The weight percent of each component can ed from the measured weights of the components added. Record the weight each component and date of preparation on the cylinder label. Record the t of refrigerant in the calibration standard cylinder.
1877 1878 1879 1880 1881 1882		in de di va	he blend calibration standard can continue in service until the liquid phase the cylinder decreases to 60% of the loading capacity ($0.6 \cdot$ liquid ensity \cdot cylinder volume in mL) when the remaining liquid phase is scarded and a new standard prepared. This is done to prevent the upor/liquid equilibrium changing, thereby changing the composition of the quid phase. Record the minimum cylinder weight on the cylinder tag.
1883 1884 1885 1886	9	using the id phase and	a vapor phase standard by either adding a known volume of vapor phase and leal gas law to calculate the weight of each component or by adding a liquid using the liquid density to calculate each component weight can be used as for Section C.10.9.2(1) through Section C.10.9.2(7).
1887	C.10.9.3. Deter	nination of C	omponent Response Factors
1888 1889			chromatography data system for an area normalization response factor
1890 1891 1892 1893 1894	2	described completely through fle	e calibration standard in triplicate using the chromatographic conditions in Section <u>C.10.9.1</u> . Load the sample injection device by slowly and vaporizing the liquid phase. For example, by bubbling the vapor into water xible polymer tubing and then puncturing the tubing with the syringe needle e apparatus as in Figure 8.
1895 1896	2		e necessary functions to have the data system determine each component actor that is then stored.
1897 1898	2) Response f Equation <u>3</u>	actors for each component are calculated as shown in Equation 36 through 8 .
		ARF _{compo}	$u_{\text{nent}_A} = \frac{\text{weight}\% \text{ of component}_A \text{ in calibration standard}}{36}$

$$RF_{component_A} = \frac{weight\% of \ component_A \ in \ calibration \ standard}{A_{component_A}} \qquad 36$$

$$ARF_{component_B} = \frac{weight\% of \ component_B \ in \ calibration \ standard}{A_{component_B}}$$
37

$$ARF_{component_{i}} = \frac{weight\% of \ component_{i} \ in \ calibration \ standard}{A_{component_{i}}}$$
38

 Where:

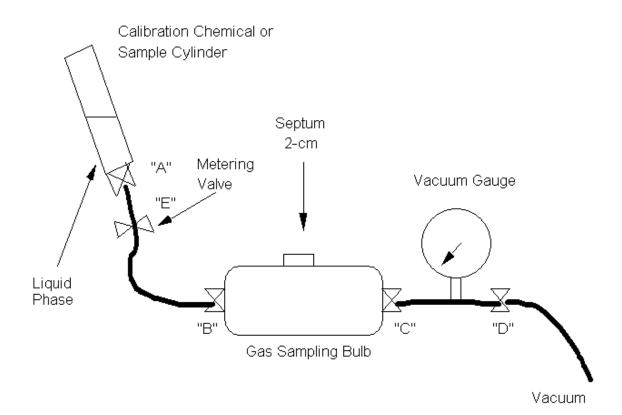
Α	=	peak area of component (average of three determinations)
ARF	=	absolute response factor
<i>component</i> _i	=	third component or greater

Then, using component *i* as the reference peak, the RRF can be determined using Equation $\underline{39}$ and Equation $\underline{40}$.

$$RRF_{component_B} = \frac{ARF_{component_B}}{ARF_{component_i}}$$
39

$$RRF_{component_A} = \frac{ARF_{component_A}}{ARF_{component_i}}$$
40

1905		RRF values are computed to the nearest 0.0001 unit.
1906 1907		Note: The largest peak in the calibration standard chromatogram is selected as the reference peak ($RRF = 1.0$).
1908	C.10.9.4.	Sampling
1909		Submitted sample cylinders shall contain liquid phase for analysis.
1910		Note: Eighty percent liquid full should be used for analysis.
1911 1912 1913 1914 1915		Special handling for low <i>critical temperature</i> refrigerants R-503 and R-508: A vapor phase sample shall be used to determine non-condensables and volatile impurities, including othe refrigerants. The vapor phase sample is obtained by regulating the sample container temperature to 5K or more above the refrigerant <i>critical temperature</i> . <i>Critical temperatures</i> R-503 = 19.5° C; R-508A = 13.5° C; and R-508B = 14.0° C.
-/		
1916	C.10.9.5.	Sample Analysis
	C.10.9.5.	
1916	C.10.9.5.	Sample Analysis
1916 1917 1918 1919 1920 1921 1922	C.10.9.5.	 Sample Analysis Analyze the sample using the chromatographic conditions described in Section <u>C.10.9.1</u>. 1) The sample taken into the syringe for injection into the gas chromatograph is vaporized liquid phase from the sample cylinder. The vapor can be obtained by completely vaporizing the liquid through soft plastic tubing into water and taking the vapor sample by piercing the tubing wall with the syringe needle. An alternative apparatus for vaporizing liquid sample into a glass gas sample bulb allowing repeat injections of the



1927 Figure 8 Apparatus Used for Calibration Standard Preparation and for **Cylinder Sampling** 1928 1929 C.10.9.6. Calculations 1930 1) The weight percentage of each component is calculated as shown in Equation 41. $W_i = \frac{RRF_i \cdot A_i \cdot 100}{\sum(A_i \cdot RRF_i)}$ 41 1931 Where: 1932 A_i peak area of component i = 1933 RRF_i Relative response factor for component *i* = 1934 W_i = weight percent of component *i* 1935 sum of all component peak areas times their respective $\sum (A_i \cdot RRF_i)$ = 1936 relative response factors 1937 Note: The largest peak in the calibration standard chromatogram is selected as the reference peak (RRF= 1.0). 1938 1939 2) Record the sample component concentrations to the nearest 0.01%. 1940

1941APPENDIX D. GAS CHROMATOGRAM FIGURES –
INFORMATIVE1942INFORMATIVE

1943 **D.1**. Purpose 1944 This appendix provides figures for the gas chromatograms used with Appendix C. For all figures: 1945 1946 Ret. Time **Retention Time** = 1947 Comp. Component = 1948 D.2. Gas Chromatogram of NCG

1949Figure 9 shows the gas chromatogram of NCG.

1950

6.0 5.5 5.0-4.5-4.0-Response - MilliVolts 3.5-3.0-2.5-Þ.0-80 1.5-C=0.04 .75 C=0.0 C=0.0 C=0.0 1.0-0.87 ŝ 2.05 0.5 0.0 3.0 0.0 1.0 2.0 4.0 5.0 6.0 7.0 8.0 Time - Minutes Data Sampling Rate = 5.001601 points/sec Run Time = 5.791479 minutes Ret Time Component

	Ket. Thile	Component	
	0.44	Air	
	0.67	CO2	
	1.33		
	1.75		
	2.05		
_			

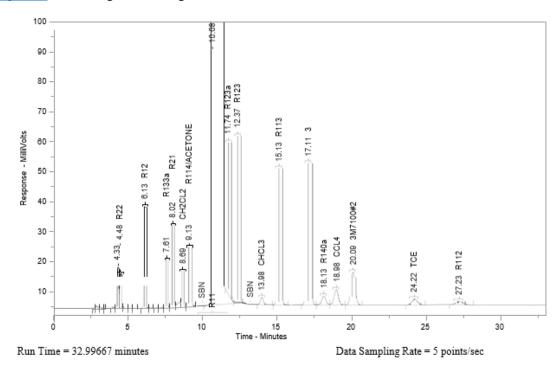
1951 1952

Figure 9 Gas Chromatogram of NCG

1954 D.3. Gas Chromatogram of R-11

1955

Figure 10 shows the gas chromatogram of R-11.



Ret. Time	Component
4.33	
4.48	R22
6.13	R12
7.61	R133a
8.02	R21
8.69	CH2CL2
9.13	R114/ACETONE
10.68	R11
11.74	R123a
12.37	R123
13.98	CHCL3
15.13	R113
17.11	3M7100#1
18.13	R140a
18.98	CCL4
20.09	3M7100#2
24.22	TCE
27.23	R112

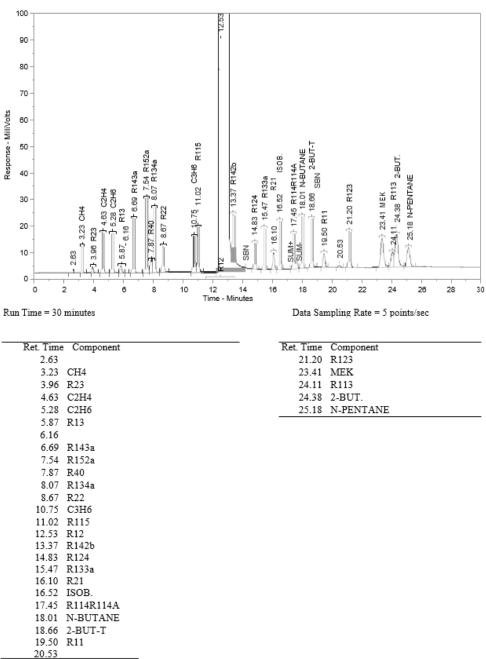
1956 1957

Figure 10 Gas Chromatogram of R-11

1959 D.4. Gas Chromatogram of R-12

1960

Figure 11 shows the gas chromatogram of R-12.



1961 1962

Figure 11 Gas Chromatogram of R-12

1964 D.5. Gas Chromatogram of R-13

1965Figure 12 shows the gas chromatogram of R-13.

1966

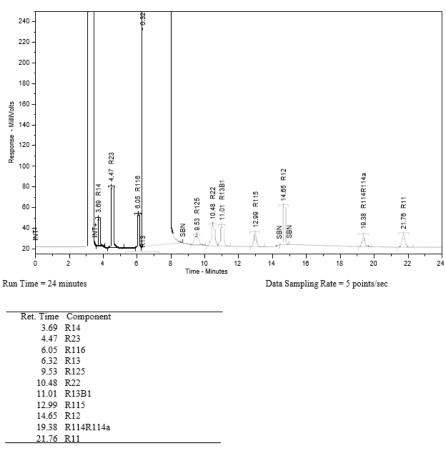
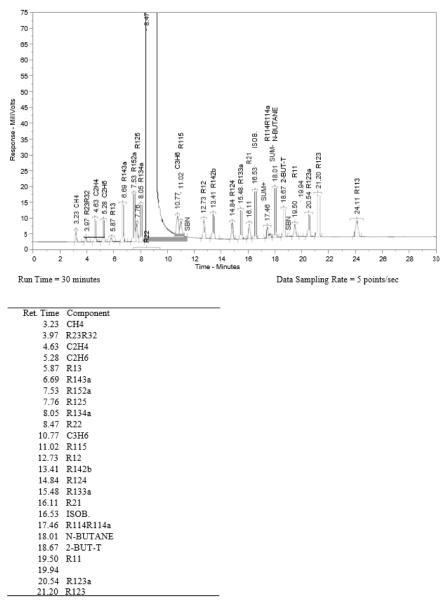


Figure 12 Gas Chromatogram of R-13

1969 D.6. Gas Chromatogram of R-22 (Packed)

1970 Figure 13 shows the gas chromatogram of R-22 (Packed).

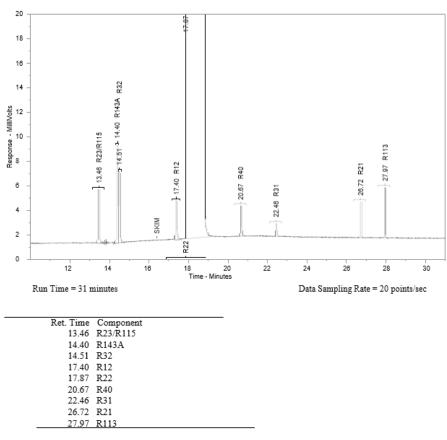


1971 1972

Figure 13 Gas Chromatogram of R-22 (Packed)

1974 D.7. Gas Chromatogram of R-22 (Capillary)

1975 <u>Figure 14</u> shows the gas chromatogram of R-22 (Capillary).

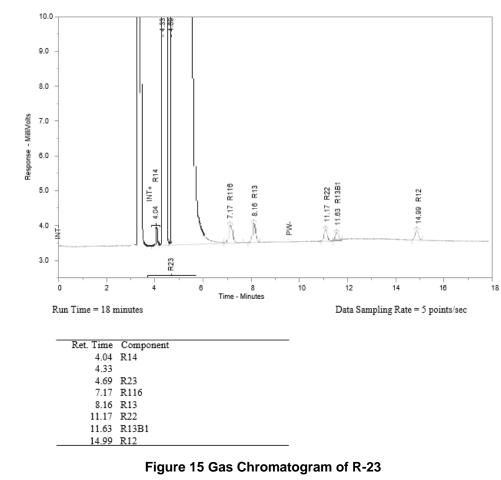


1976 1977

Figure 14 Gas Chromatogram of R-22 (Capillary)

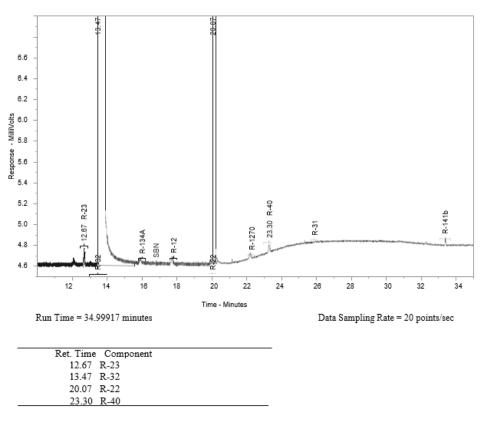
1979 D.8. Gas Chromatogram of R-23

1980 Figure 15 shows the gas chromatogram of R-23.



1986 D.9. Gas Chromatogram of R-32

1987Figure 16 shows the gas chromatogram of R-32.



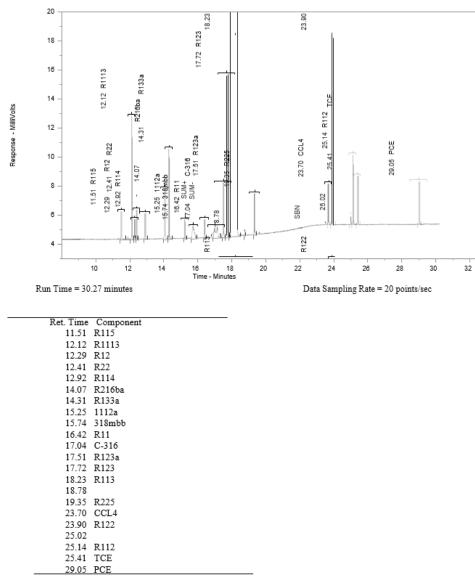
1988 1989

Figure 16 Gas Chromatogram of R-32

1990

1992 D.10. Gas Chromatogram of R-113

1993 Figure 17 shows the gas chromatogram of R-113.

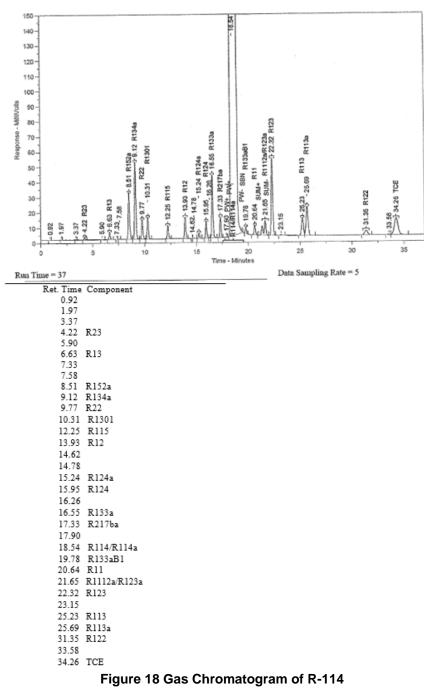


1994 1995

Figure 17 Gas Chromatogram of R-113

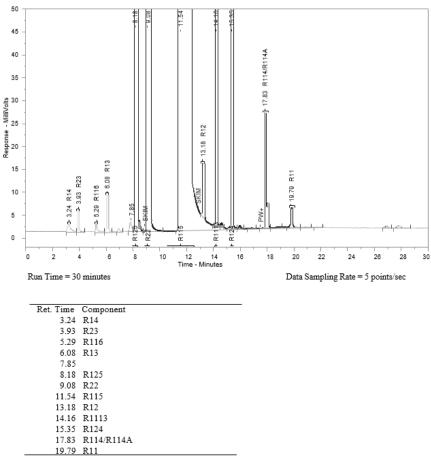
1998 D.11. Gas Chromatogram of R-114

1999 <u>Figure 18</u> shows the gas chromatogram of R-114.



2004 D.12. Gas Chromatogram of R-115

2005 <u>Figure 19</u> shows the gas chromatogram of R-115.



2006 2007

Figure 19 Gas Chromatogram of R-115

2010 D.13. Gas Chromatogram of R-116

2011 Figure 20 shows the gas chromatogram of R-116.

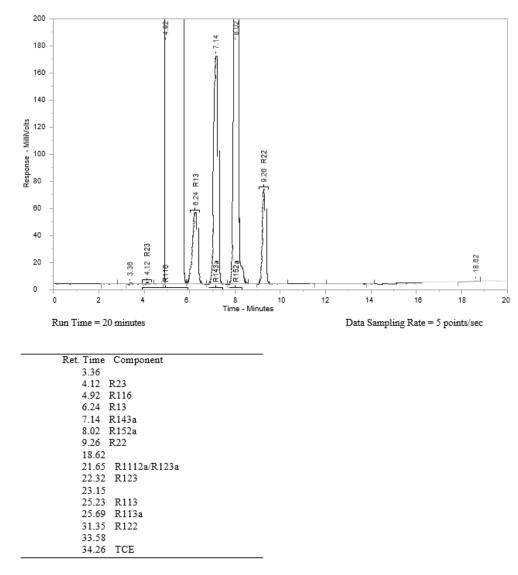


Figure 20 Gas Chromatogram of R-116

2015 D.14. Gas Chromatogram of R-123 (Packed)

2016 Figure 21 shows the gas chromatogram of R-123 (Packed).

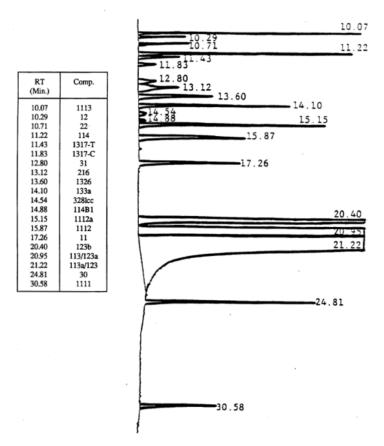
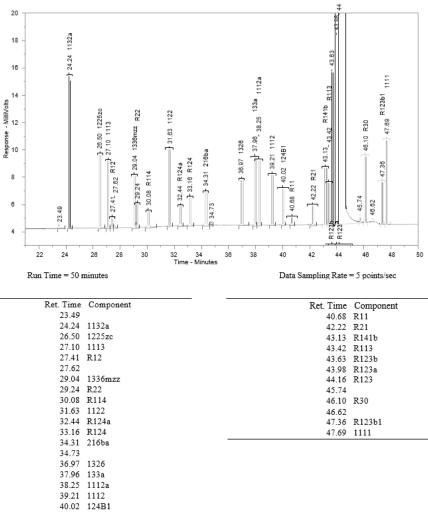




Figure 21 Gas Chromatogram of R-123 (Packed)

2021 D.15. Gas Chromatogram of R-123 (Capillary)

2022 Figure 22 shows the gas chromatogram of R-123 (capillary).

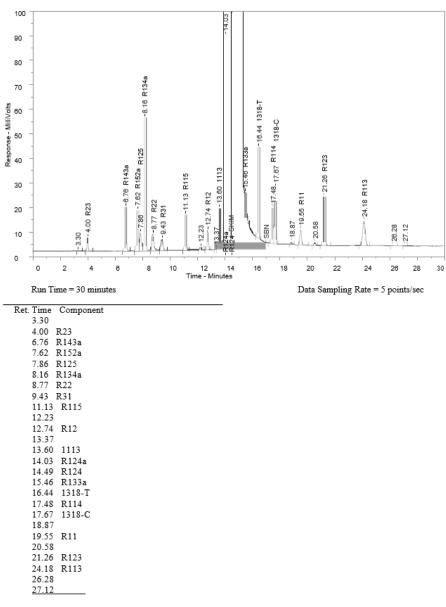


2023 2024

Figure 22 Gas Chromatogram of R-123 (Capillary)

2026 D.16. Gas Chromatogram of R-124

2027 Figure 23 shows the gas chromatogram of R-124.

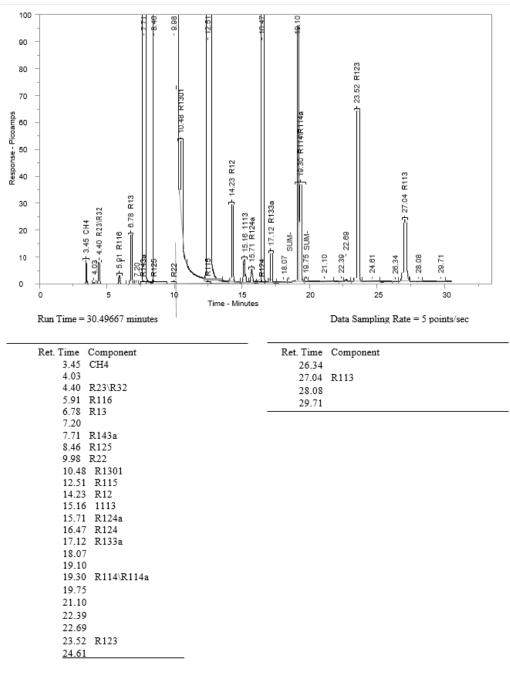


2028 2029

Figure 23 Gas Chromatogram of R-124

2031 D.17. Gas Chromatogram of R-125

2032 Figure 24 shows the gas chromatogram of R-125.



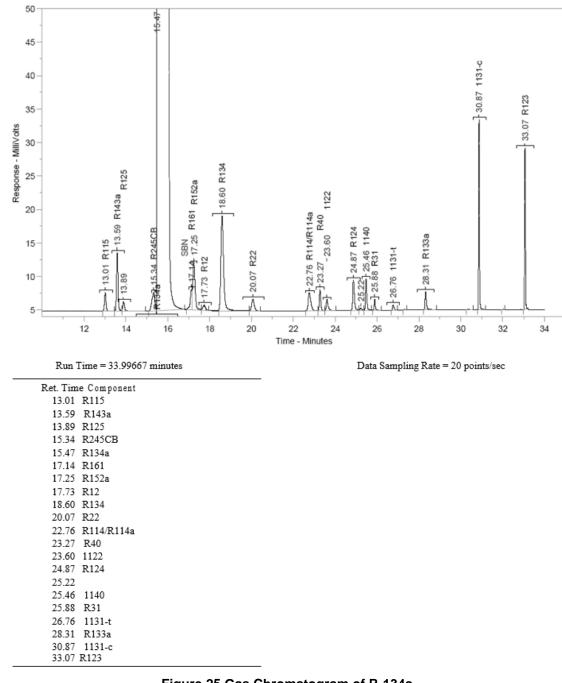
2033 2034

Figure 24 Gas Chromatogram of R-125

2036 D.18. Gas Chromatogram of R-134a

2037

Figure 25 shows the gas chromatogram of R-134a.

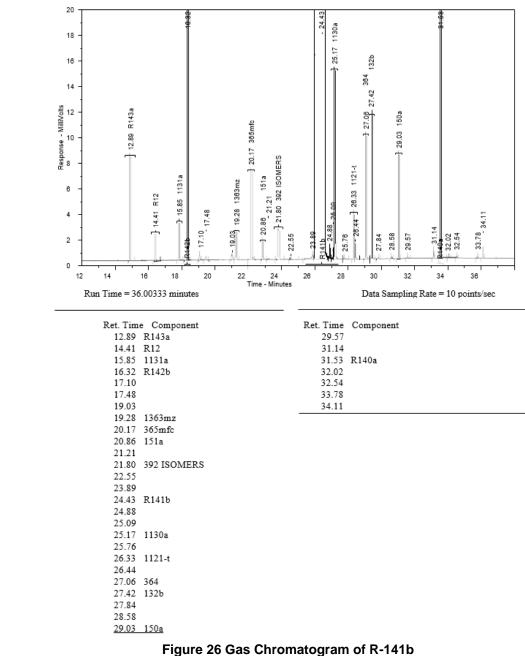


2039 2040

Figure 25 Gas Chromatogram of R-134a

2041 D.19. Gas Chromatogram of R-141b

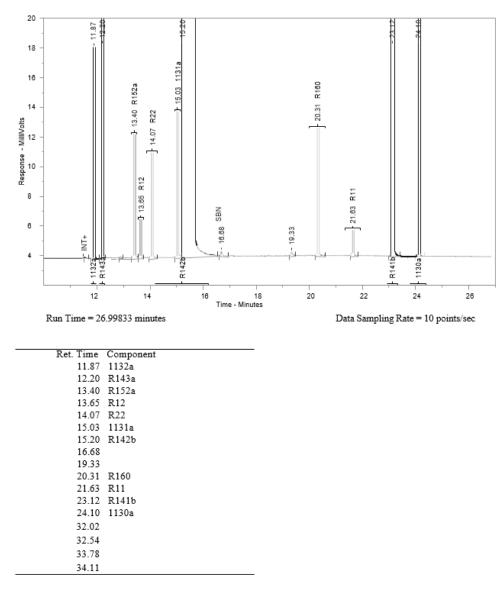
2042 Figure 26 shows the gas chromatogram of R-141b.



2043 2044

2046 D.20. Gas Chromatogram of R-142b

2047 Figure 26 shows the gas chromatogram of R-142b.



2048 2049

Figure 27 Gas Chromatogram of R-142b

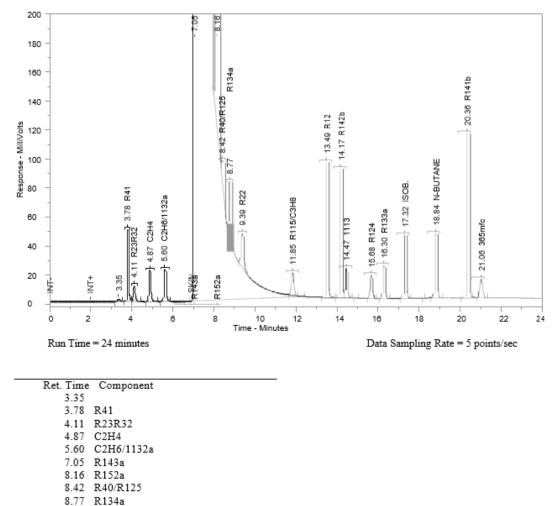
2051 D.21. Gas Chromatogram of R-143a

2052

Figure 28 shows the gas chromatogram of R-143a.

9.39 R22 11.85 R115/C3H8 13.49 R12 14.17 R142b 14.47 1113

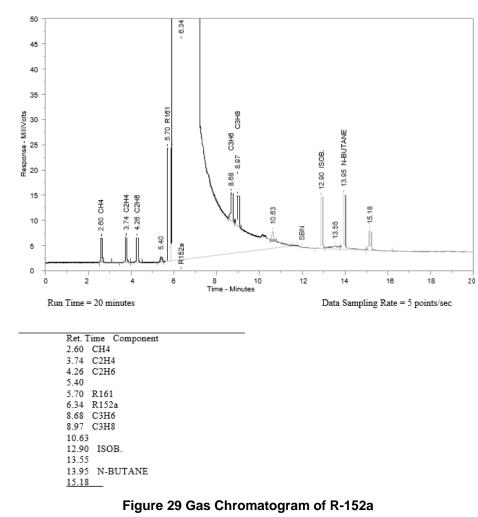
14.47 1113 15.68 R124 16.30 R133a 17.32 ISOB. 18.84 N-BUTANE 20.36 R141b 21.06 365mfc



2053 2054

2056 D.22. Gas Chromatogram of R-152a

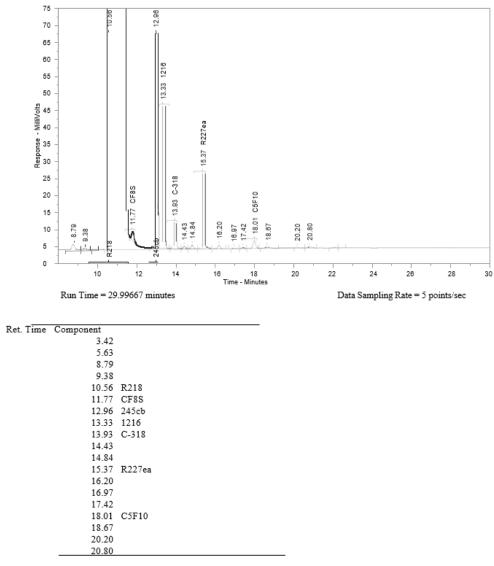
2057 Figure 29 shows the gas chromatogram of R-152a.



2058 2059

2061 D.23. Gas Chromatogram of R-218

2062 <u>Figure 30</u> shows the gas chromatogram of R-218.

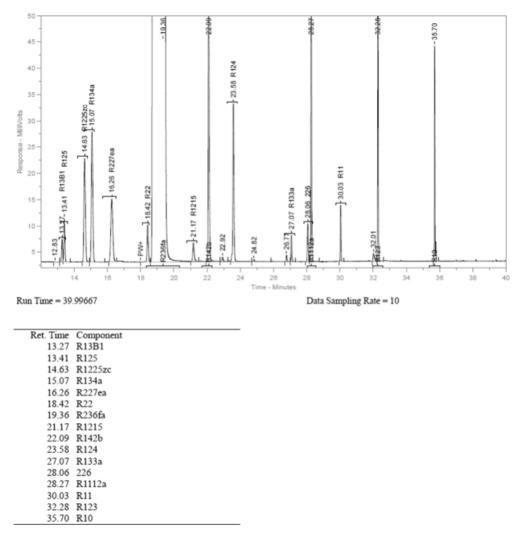


2063 2064

Figure 30 Gas Chromatogram of R-218

2066 D.24. Gas Chromatogram of R-236fa

2067 <u>Figure 31</u> shows the gas chromatogram of R-236fa.

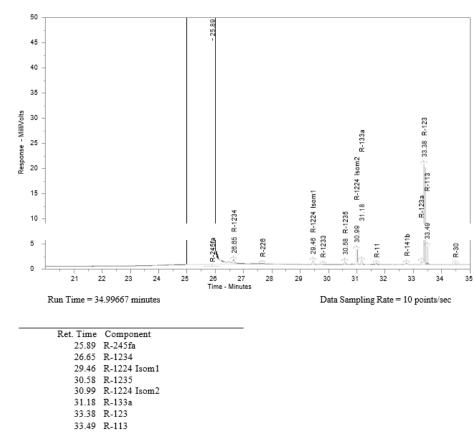


2068 2069

Figure 31 Gas Chromatogram of R-236fa

2071 D.25. Gas Chromatogram of R-245fa

2072 Figure 32 shows the gas chromatogram of R-245fa.

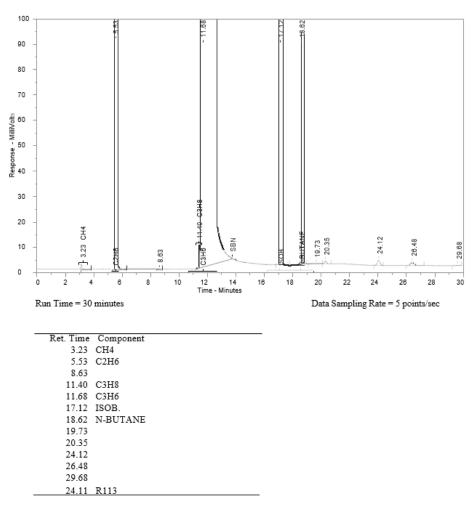


2073 2074

Figure 32 Gas Chromatogram of R-245fa

2076 D.26. Gas Chromatogram of R-290

2077 <u>Figure 33</u> shows the gas chromatogram of R-290.

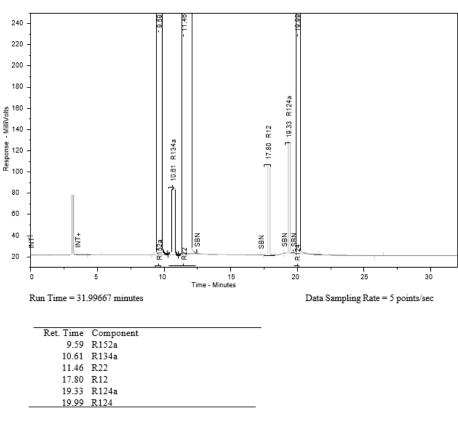


2078 2079

Figure 33 Gas Chromatogram of R-290

2081 D.27. Gas Chromatogram of R-401

2082 <u>Figure 34</u> shows the gas chromatogram of R-401.

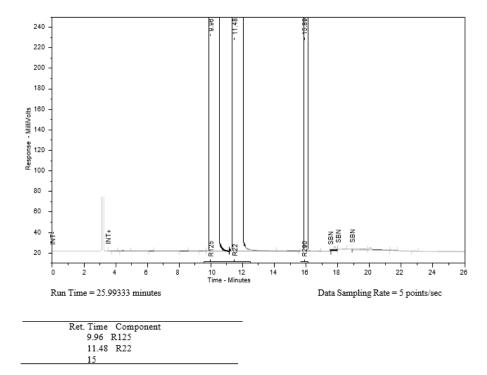


2083 2084

Figure 34 Gas Chromatogram of R-401

2086 D.28. Gas Chromatogram of R-402

2087 <u>Figure 35</u> shows the gas chromatogram of R-402.



2088 2089

Figure 35 Gas Chromatogram of R-402

2091 **D.29**. Gas Chromatogram of R-403

2092 Figure 36 shows the gas chromatogram of R-403.

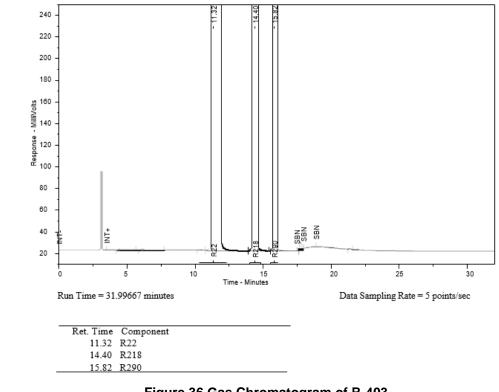


Figure 36 Gas Chromatogram of R-403

2094

2093

2096 D.30. Gas Chromatogram of R-404

2097 <u>Figure 37</u> shows the gas chromatogram of R-404.

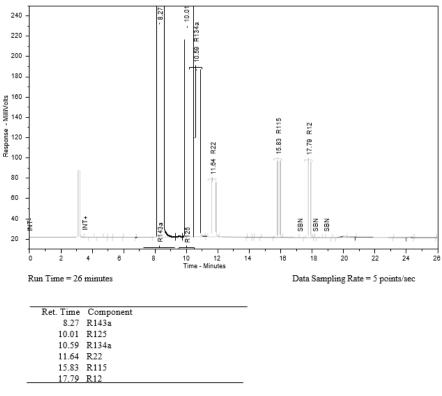
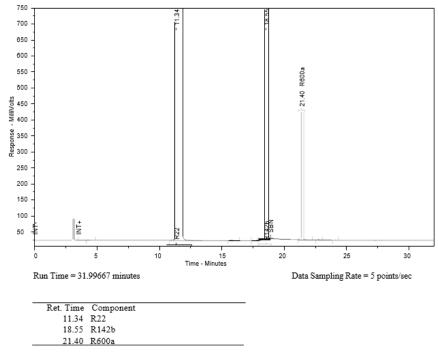


Figure 37 Gas Chromatogram of R-404

2098 2099

2101 D.31. Gas Chromatogram of R-406

2102 Figure 38 shows the gas chromatogram of R-406.

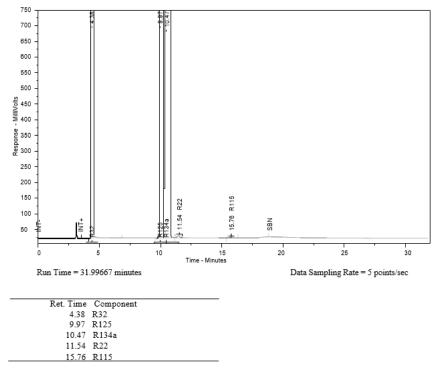


2103 2104

Figure 38 Gas Chromatogram of R-406

2106 D.32. Gas Chromatogram of R-407

2107 <u>Figure 39</u> shows the gas chromatogram of R-407.

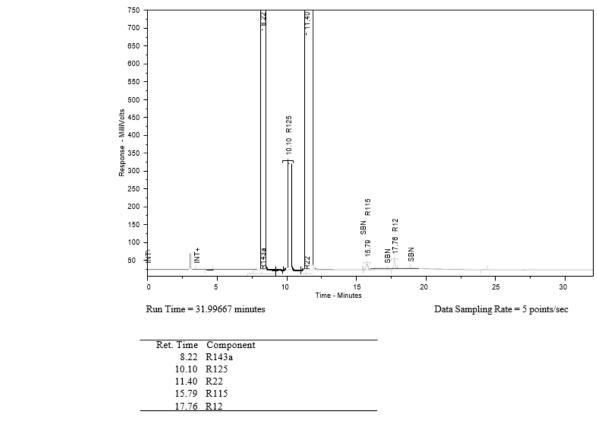


2108 2109

Figure 39 Gas Chromatogram of R-407

2111 D.33. Gas Chromatogram of R-408

2112 Figure 40 shows the gas chromatogram of R-408.

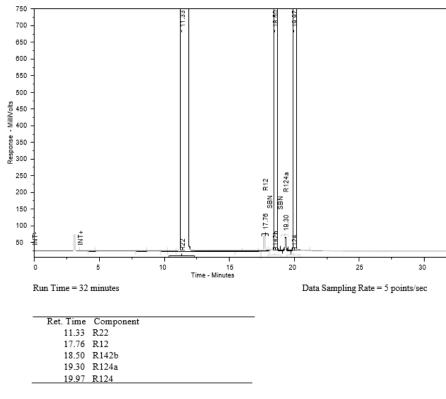


2113 2114

Figure 40 Gas Chromatogram of R-408

2116 D.34. Gas Chromatogram of R-409

2117 Figure 41 shows the gas chromatogram of R-409.





2119

Figure 41 Gas Chromatogram of R-409

2121 D.35. Gas Chromatogram of R-410

2122 Figure 42 shows the gas chromatogram of R-410.

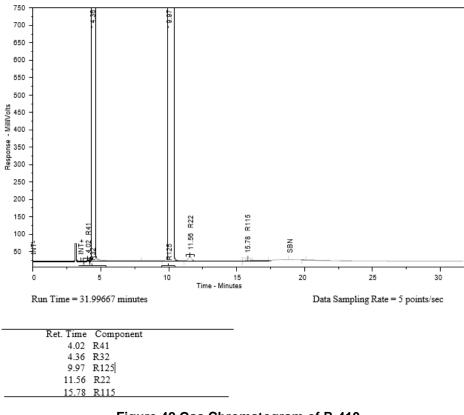


Figure 42 Gas Chromatogram of R-410

2125

2126 D.36. Gas Chromatogram of R-411

2127 Figure 43 shows the gas chromatogram of R-411.

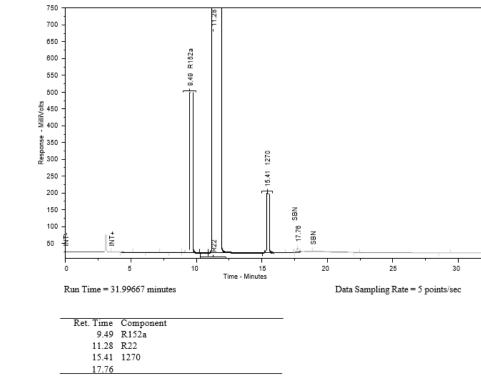


Figure 43 Gas Chromatogram of R-411

2129 2130

2131 D.37. Gas Chromatogram of R-412

2132 <u>Figure 44</u> shows the gas chromatogram of R-412.

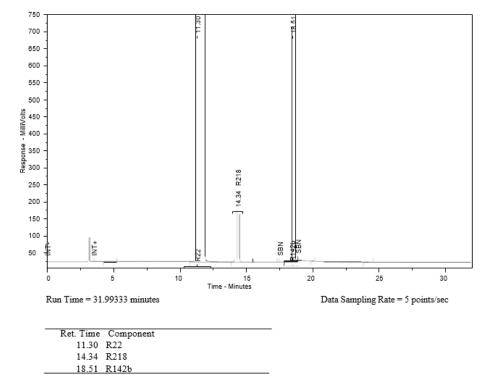


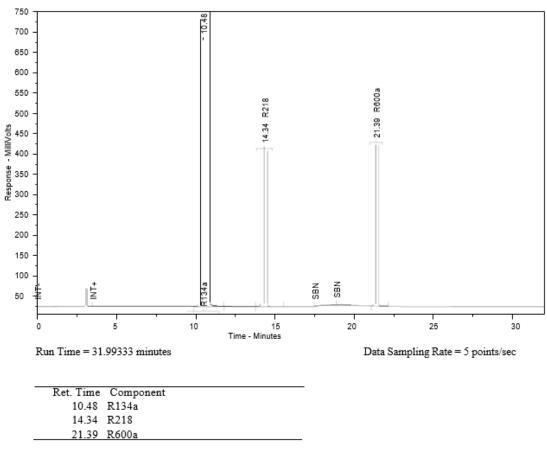
Figure 44 Gas Chromatogram of R-412

2133

2135

2136 D.38. Gas Chromatogram of R-413

2137 <u>Figure 45</u> shows the gas chromatogram of R-413.

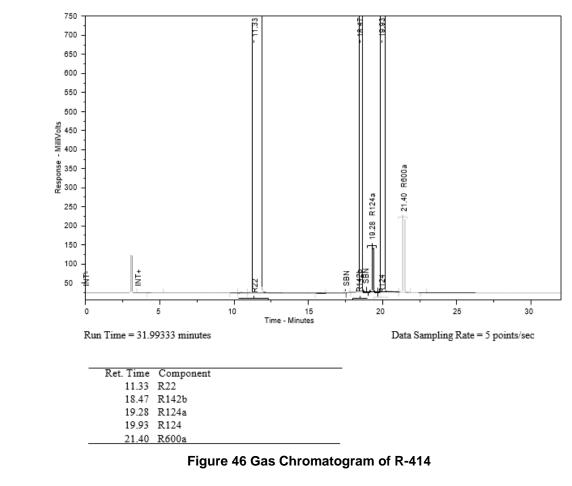


2138 2139

Figure 45 Gas Chromatogram of R-413

2141 D.39. Gas Chromatogram of R-414

2142 Figure 46 shows the gas chromatogram of R-414.



2145

2146 D.40. Gas Chromatogram of R-416

2147 Figure 47 shows the gas chromatogram of R-416.

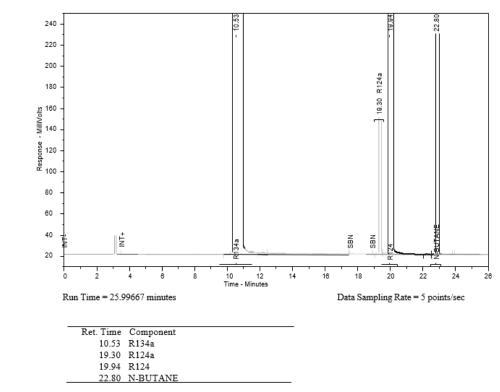
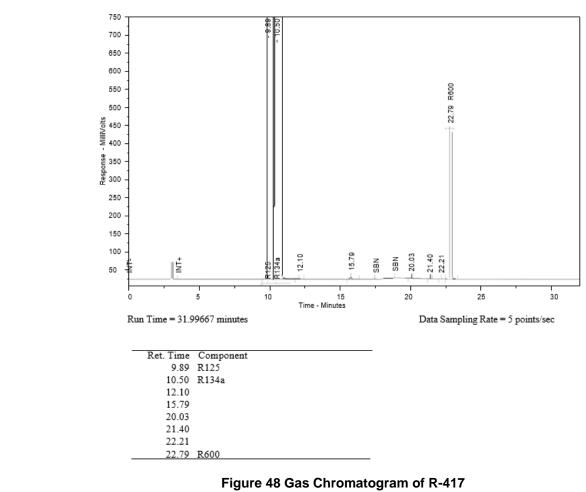


Figure 47 Gas Chromatogram of R-416

2150

2151 D.41. Gas Chromatogram of R-417

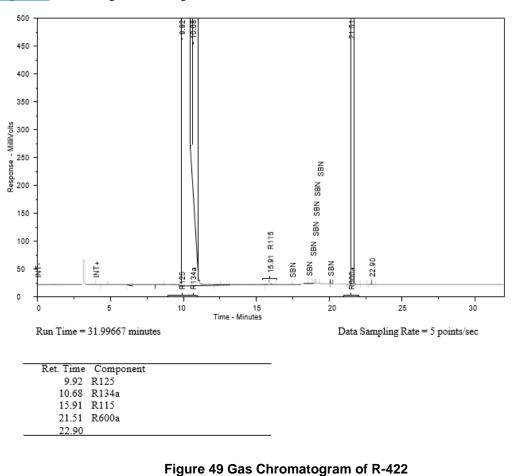
2152 Figure 48 shows the gas chromatogram of R-417.



2153 2154

2156 D.42. Gas Chromatogram of R-422

2157 Figure 49 shows the gas chromatogram of R-422.

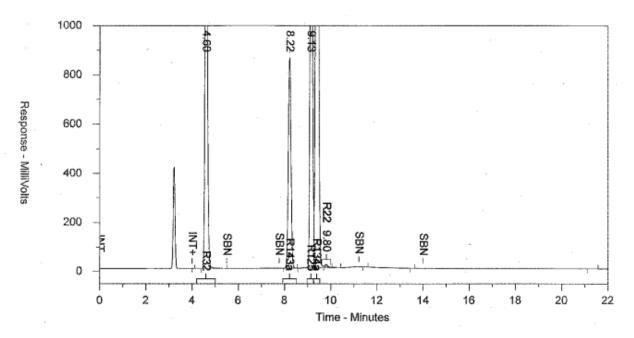


2158

2159

2161 D.43. Gas Chromatogram of R-427

2162 Figure 50 shows the gas chromatogram of R-427.



Run Time = 21.99667

Ret. Time	Component
4.60	R32
8.22	R143a
9.13	R125
9.38	R134a
9.80	R22

2163

2164

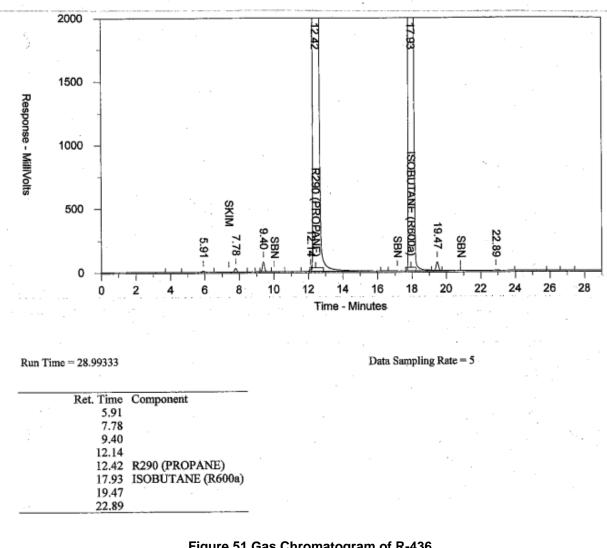
Figure 50 Gas Chromatogram of R-427

Data Sampling Rate = 5

2166 **D.44**. Gas Chromatogram of R-436

2167

Figure 51 shows the gas chromatogram of R-436.



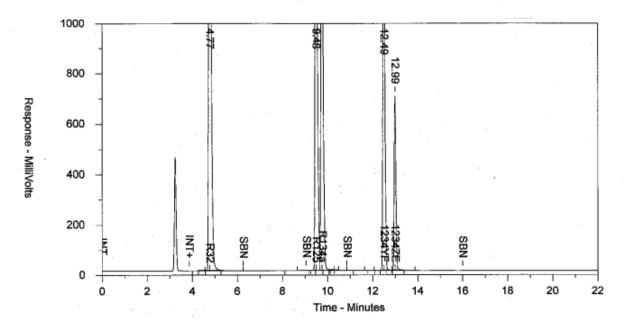
2169 2170

2168

Figure 51 Gas Chromatogram of R-436

2171 D.45. Gas Chromatogram of R-448

2172 Figure 52 shows the gas chromatogram of R-448.



Run Time = 21.99667

Ret. Time	Component
4.77	R32
9.48	R125
9.75	R134a
12.49	1234YF
12.99	1234ZE

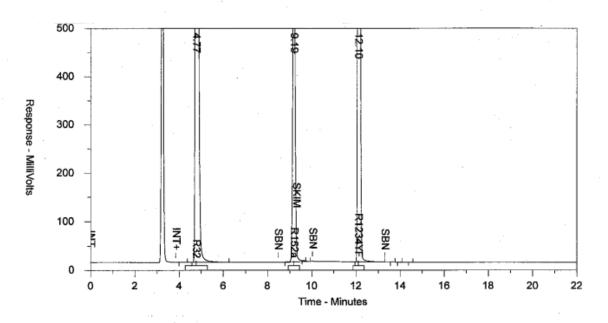
2173

Figure 52 Gas Chromatogram of R-448

Data Sampling Rate = 5

2176 D.46. Gas Chromatogram of R-457

2177 <u>Figure 53</u> shows the gas chromatogram of R-457.



Run Time = 21,99333

Component	
R32	
R152a	
R1234YF	
	R32 R152a

2178

2179

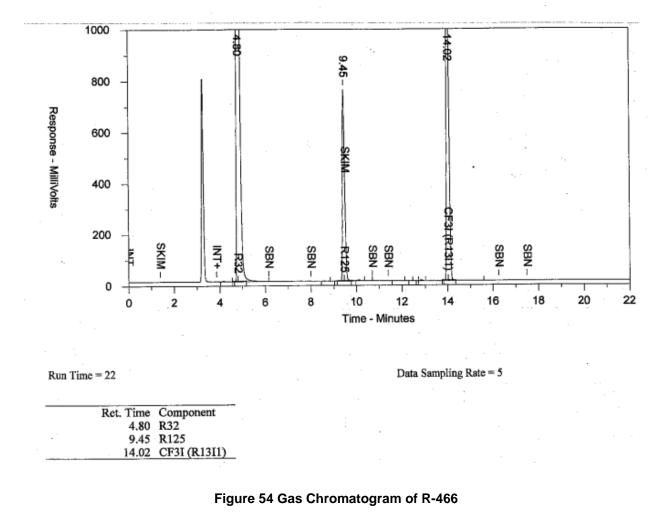
2180

Figure 53 Gas Chromatogram of R-457

Data Sampling Rate = 5

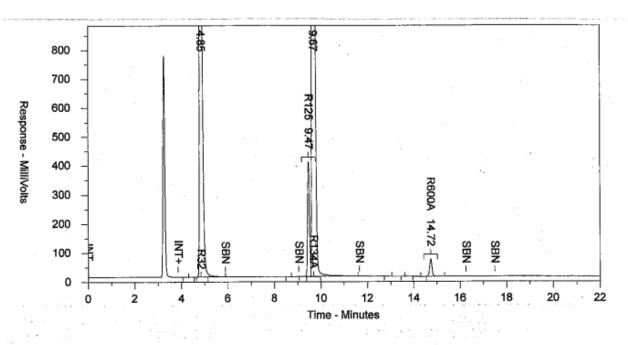
2181 D.47. Gas Chromatogram of R-466

2182 Figure 54 shows the gas chromatogram of R-466.



2186 D.48. Gas Chromatogram of R-467

2187 <u>Figure 55</u> shows the gas chromatogram of R-467.



Run Time = 21.99333

Ret: Time	Component
	R32
	R125
	R134A
14.72	R600A

2188

2189

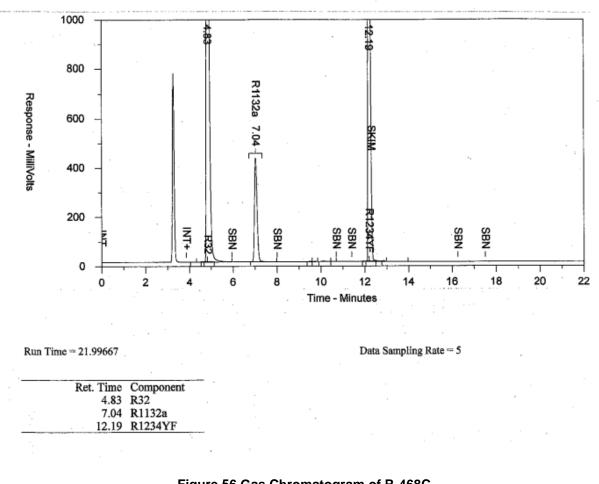
2190

Figure 55 Gas Chromatogram of R-467

Data Sampling Rate = 5

2191 **D.49**. Gas Chromatogram of R-468C

2192 Figure 56 shows the gas chromatogram of R-468C.



2193

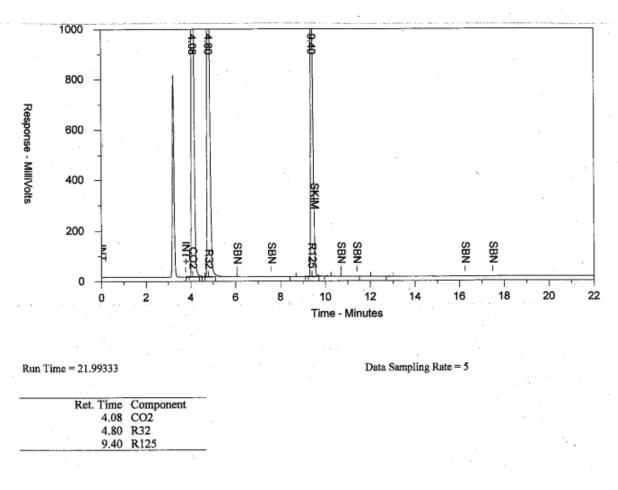
2194

2195

Figure 56 Gas Chromatogram of R-468C

2196 D.50. Gas Chromatogram of R-469

2197 <u>Figure 57</u> shows the gas chromatogram of R-469.



2198

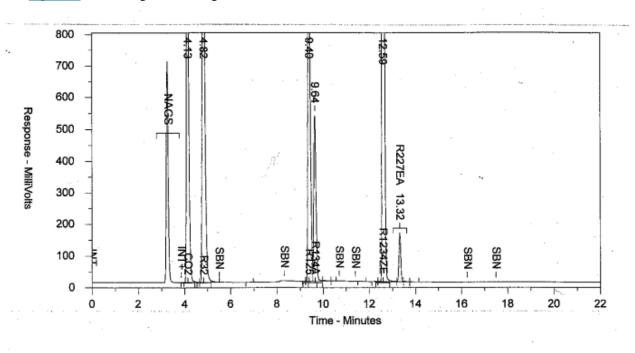
2199

Figure 57 Gas Chromatogram of R-469

2201 D.51. Gas Chromatogram of R-470A

2202

Figure 58 shows the gas chromatogram of R-470A.



Run Time = 21.99333	Data Sampling Rate = 5

	Ret. Time	Component
	4.13	CO2
· · · ·	4.82	R32
	9.40	R125
	9.64	R134A
	12.59	R1234ZE
	13.32	R227EA

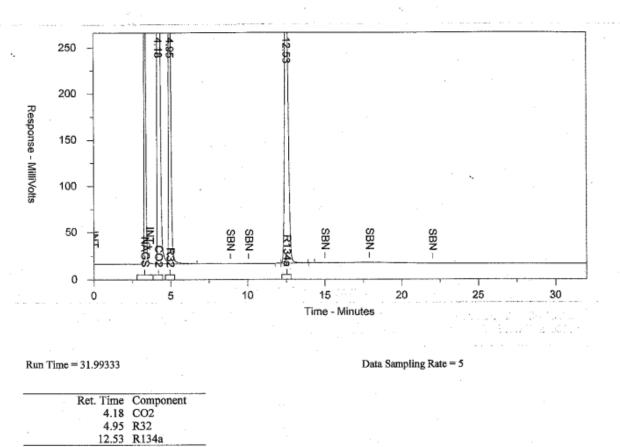
2203

2204

Figure 58 Gas Chromatogram of R-470A

2206 D.52. Gas Chromatogram of R-472A

2207 <u>Figure 59</u> shows the gas chromatogram of R-472A.

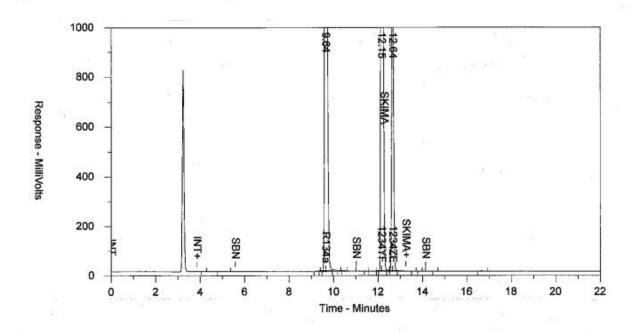


2208

2209 2210 Figure 59 Gas Chromatogram of R-472A

2211 D.53. Gas Chromatogram of R-475

2212 Figure 60 shows the gas chromatogram of R-475.



Run Time = 21.99333

	Ret. Time	Component	4
	9.64	R134a	
	12.15	1234YF	
l(t	12.64	1234ZE	-03

2213

2214

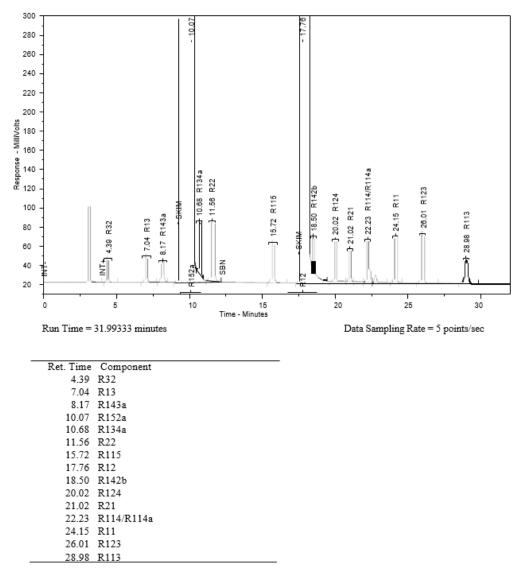
2215

Figure 60 Gas Chromatogram of R-475

Data Sampling Rate = 5

2216 D.54. Gas Chromatogram of R-500

2217 Figure 61 shows the gas chromatogram of R-500.



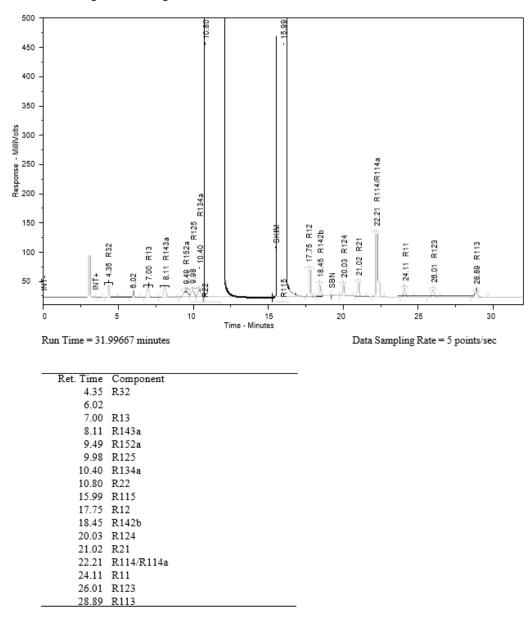
2218

2219

Figure 61 Gas Chromatogram of R-500

2221 D.55. Gas Chromatogram of R-502

Figure 62 shows the gas chromatogram of R-502.

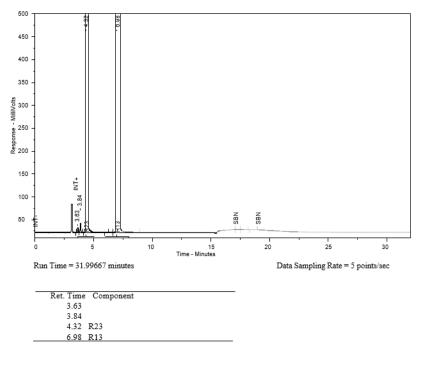


2223 2224

Figure 62 Gas Chromatogram of R-502

2226 D.56. Gas Chromatogram of R-503

Figure 63 shows the gas chromatogram of R-503.



2228

2229

Figure 63 Gas Chromatogram of R-503

2231 D.57. Gas Chromatogram of R-507

Figure 64 shows the gas chromatogram of R-507.

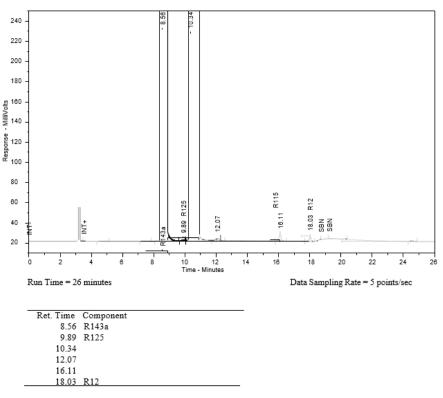


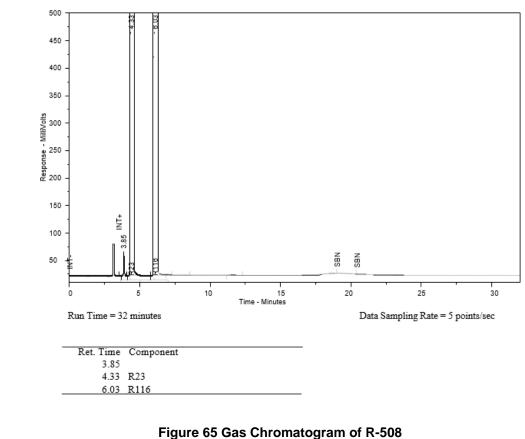
Figure 64 Gas Chromatogram of R-507

2234

2233

2236 D.58. Gas Chromatogram of R-508

Figure 65 shows the gas chromatogram of R-508.

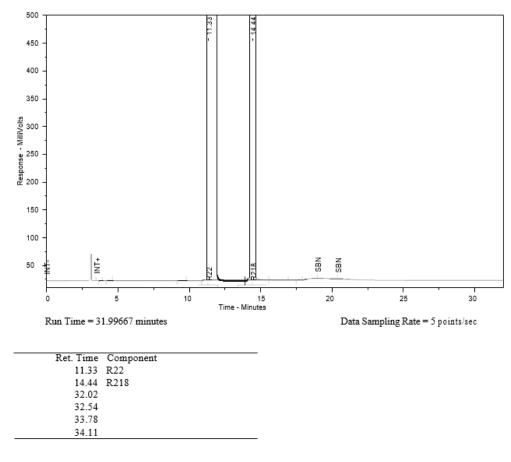


2238

2239

2241 D.59. Gas Chromatogram of R-509

Figure 66 shows the gas chromatogram of R-509.



2243

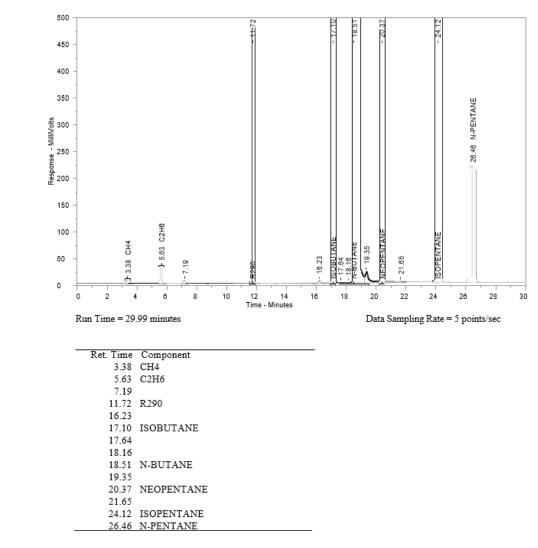
2244

2245

Figure 66 Gas Chromatogram of R-509

2246 D.60. Gas Chromatogram of R-600

Figure 67 shows the gas chromatogram of R-600.



2248

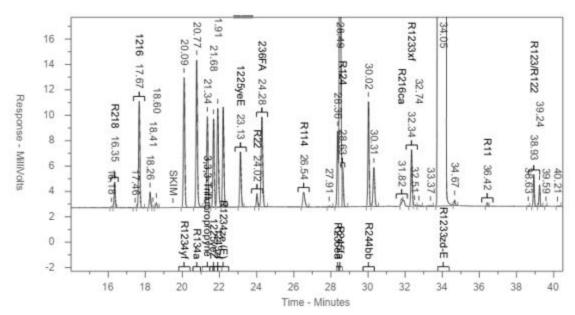
2249

Figure 67 Gas Chromatogram of R-600

Data Sampling Rate = 5 points/sec

2251 D.61. Gas Chromatogram of R-1233zd

Figure 68 shows the gas chromatogram of R-1233zd.



Run Time = 40.49667 minutes

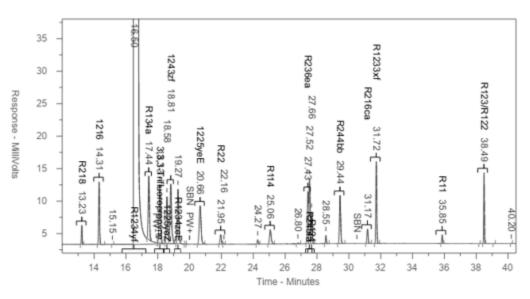
Component	Ret. Time
	16.18
R218	16.35
	17.46
1216	17.67
	18.26
	18.41
	18.60
R1234yf	20.09
R134a	20.77
3,3,3-Trifluoropropyne	21.34
1225yeZ	21.68
1243zf	21.91
R1234ze (E)	22.20
1225yeE	23.13
R22	24.02
236FA	24.28
R114	26.54
	27.91
R236ea	28.36
R245fa	28.49

2253 2254

Figure 68 Gas Chromatogram of R-1233zd

2256 D.62. Gas Chromatogram of R-1234yf

Figure 69 shows the gas chromatogram of R-1234yf.



Run Time = 40.5 minutes

Data Sampling Rate = 10 points/sec

Component	Ret. Time
R218	13.23
1216	14.31
	15.15
R1234yf	16.50
R134a	17.44
3,3,3-Trifluoropropyne	18.13
1225yeZ	18.58
1243zf	18.81
R1234zeE	19.27
1225yeE	20.66
Ř22	21.95
	22.16
	24.27
R114	25.06
	26.80
R236ea	27.43
R245fa	27.52
R124	27.66
	28.55
R244bb	29.44

2258

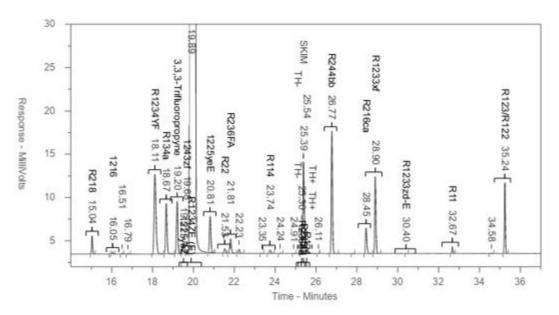
2259

2260

Figure 69 Gas Chromatogram of R-1234yf

2261 D.63. Gas Chromatogram of R-1234ze

Figure 70 shows the gas chromatogram of R-1234ze.



Run Time = 40.49667

Data Sampling Rate = 5 points/sec

Component	Wt. %	Resp. F	Area	Ret. Time
R218	0.0096	9.375916E-07	7593	15.04
1216	0.0005	3.322259E-07	1091	16.05
	0.0000	1.415021E-07	242	16.51
	0.0000	1.415021E-07	180	16.79
R1234YF	0.0174	2.184536E-07	58685	18.11
R134a	0.0090	2.313106E-07	28786	18.67
3,3,3-Trifluoropropyne	0.0057	1.495269E-07	28136	19.20
1225yeZ	0.0036	3.793551E-07	6939	19.51
1243zf	0.0003	1.040583E-07	1954	19.68
R1234ZE (E)	99.8424	1.415021E-07	520800300	19.89
1225yeE	0.0052	1.867106E-07	20534	20.81
Ř22	0.0033	9.932808E-07	2488	21.53
R236FA	0.0013	1.024832E-07	9441	21.81
	0.0004	1.415021E-07	2287	22.23
	0.0000	1.415021E-07	253	23.35
R114	0.0047	1.354606E-06	2541	23.74
	0.0001	1.415021E-07	356	24.24
	0.0000	1.415021E-07	149	24.91
R236ea	0.0101	6.028471E-07	12313	25.30
R245fa	0.0187	2.614092E-07	52881	25.39

2263 2264

Figure 70 Gas Chromatogram of R-1234ze

2266 D.64. Gas Chromatogram of R-13I1

 Figure 71 shows the gas chromatogram of R-13I1.

